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Low-Frequency Noise in Modern Bipolar Transistors: Impact of Intrinsic Transistor and Parasitic Series Resistances

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Abstract—In modern submicrometer transistors, the influence of the internal base and emitter series resistances, on both the I-V characteristics and the LF noise at higher bias currents, becomes important. In this paper expressions are presented for the LF noise in transistors, where the influence of the series resistances has been taken into account. The expressions have been compared with recent experimental results from the literature obtained from modern submicrometer (heterojunction) bipolar transistors. At low forward currents the LF noise in such transistors is determined by spontaneous fluctuations in the base and collector currents. In most transistors at higher forward currents, the parasitic series resistances and their noise become important.

I. INTRODUCTION

It is well known that low-frequency (LF) noise in bipolar transistors and FET's can limit the bandwidth and stability of circuit operation at high speed [1].

Bipolar transistors featuring very low noise are of considerable interest for high-frequency applications. Low LF noise transistors will not only improve the performance but also significantly reduce the size of microwave and millimeter-wave radio communication equipment, since such devices eliminate the need for a dielectric resonator to stabilize frequency oscillations [2]. Low-frequency noise also causes phase noise in oscillators and therefore has to be as low as possible. In general, we can state that LF noise restricts the sensitivity of a system and sets a limit in small signal processing. Consequently, it is necessary to have an understanding of the LF noise sources in transistors in order to improve techniques for device modeling and design.

Up to the present a number of papers have been published on low-frequency noise, especially 1/f noise, in bipolar transistors. In the most recent papers, the 1/f noise in bipolar transistors has mainly been discussed in terms of fluctuations in the mobility or diffusivity of free charge carriers. A survey of the interpretation of 1/f noise in bipolar transistors until 1986 has been given by Van der Ziel [3]. A review of the literature over the period 1985–1989 has been given by Kleinpenning at the 10th International Conference on Noise in Physical Systems in 1989 [4]. Until 1990 the low-frequency noise sources in bipolar transistors were generally accepted as being located between emitter and collector and between emitter and base. In principle, there is also a noise source between base and collector. In practical cases the base-collector junction is reverse-biased, so that the base-collector current is slight and its noise can be neglected.

Recent developments in transistor technology have led to a significant lateral down-scaling of bipolar devices. In such down-scaled transistors, deviations from the expected current dependence of the low-frequency noise in the collector current and in the base current are observed. Kleinpenning [4] suggested that these deviations may be ascribed to resistance fluctuations in the internal parasitic series resistances. It is well known that in submicrometer bipolar transistors the influence of the internal base and emitter series resistances on the characteristics at higher currents becomes important [5]. Recently, papers on low-frequency noise in bipolar transistors have been published taking the influence of the internal series resistances into account [6], [7].

The purpose of this paper is to present a survey of the state-of-the-art of low-frequency noise in modern transistors, like polysilicon emitter bipolar transistors and heterojunction bipolar transistors.

The organization of the paper is as follows. In Section II, we describe the measuring methods of LF noise in transistors. In Section III general formulas for the LF noise in transistors are presented, taking the contributions from the parasitic series resistances into account. In Section IV we discuss the noise sources in transistors, and in Section V we compare experimental data from literature with the general noise formulas. In Section VI the conclusions are presented.

II. CIRCUITS FOR NOISE MEASUREMENTS

Usually the low-frequency noise of a bipolar transistor is measured with the transistor in circuits as shown in Fig. 1. The internal series resistances are given by \( r_e \), \( r_b \), and \( r_c \), respectively. In Fig. 1(a) three external wire-wound or metal-film resistors \( R_C \), \( R_B \) and \( R_E \) are inserted. Such resistors only have Nyquist noise \((4kT\beta)\). Here, we consider a p-n-p transistor with the emitter-base junction to be forward-biased and the base-collector junction to be reverse biased.
DC biasing is performed with the help of batteries. The spectral noise densities of the voltage fluctuations across the resistors $R_E$, $R_B$, and $R_C$ can be measured with the help of a low-noise voltage amplifier and a Fast Fourier Transform digital spectrum analyzer. In the common-emitter configuration ($R_E = 0$) the voltage noise across the resistor $R_C$ is often measured as a function of both $R_B$ and the current $I_E$. In the common-collector configuration ($R_C = 0$), the voltage noise across the resistor $R_E$ is often measured as a function of both the current $I_E$ and the value of the external resistance $R_B$.

In the circuit of Fig. 1(b) the spectral noise densities of the current fluctuations $\Delta I_C$, $\Delta I_B$, and $\Delta I_E$ can be measured with the help of a low-noise current amplifier and an FFT spectrum analyzer. Both the currents and its noise are measured by inserting the measuring apparatus in the external lead. In the next section we shall present general noise formulas for both the voltage spectral noise densities across the external resistors and the current spectral noise densities in $I_C$, $I_B$, and $I_E$.

III. GENERAL FORMULAS

We consider a p-n-p transistor with the emitter-base junction to be forward biased ($V_{eb} \gg kT/q$) and the base-collector junction to be reverse-biased ($V_{bc} \gg kT/q$). For the fluctuations in the base, collector, and emitter currents we have

$$\Delta I_B = \Delta I_b + \Delta V_{eb}/r_e$$

(1)

$$\Delta I_C = \Delta I_c + g_m \Delta V_{eb}$$

(2)

$$\Delta I_E = \Delta I_B + \Delta I_C$$

(3)

Here $g_m = dI_e/dV_{eb}$ is the collector transconductance, $r_e = dV_{eb}/dI_e$ the input resistance, $\Delta I_b$ and $\Delta I_c$ the spontaneous fluctuations in the base and collector currents at constant $V_{eb}$, with $V_{eb}$ the voltage drop across the emitter-base junction, excluding the voltage drops across the series resistances $r_b$ and $r_c$. The fluctuations in $V_{eb}$ are given by

$$\Delta V_{eb} = -(R_B + r_b)\Delta I_B - I_B \Delta r_b - (R_E + r_e)\Delta I_E - I_E \Delta r_e + \Delta V_{eb}^N$$

(4)

with $\Delta V_{eb}^N$ the fluctuations in $V_{eb}$ due to the Nyquist noise in $R_B$, $r_b$, $R_E$, and $r_e$. The spontaneous fluctuations in the base and emitter series resistances are given by $\Delta r_b$ and $\Delta r_e$. In (1)–(3) we have assumed $I_B$ and $I_C$ to be independent of $V_{eb}$, so the Early effect has been neglected.

Combining (1)–(4), the fluctuations in the currents $\Delta I_E$, $\Delta I_C$, and $\Delta I_B$ can be expressed in terms of the spontaneous noise sources $\Delta I_b$, $\Delta I_c$, $\Delta r_b$, and $\Delta V_{eb}^N$. For the fluctuations across the external resistors in Fig 1(a), we have

$$\Delta V_b = \Delta V_{eb}^N + R_E \Delta I_E$$

$$\Delta V_c = \Delta V_{eb}^N + R_C \Delta I_C$$

$$\Delta V_E = \Delta V_{eb}^N + R_B \Delta I_B$$

(5)

Here, $\Delta V_{eb}^N$, $\Delta V_{eb}^N$, and $\Delta V_{eb}^N$ are the open-circuit Nyquist voltage fluctuations in the external resistance of $R_E$, $R_C$, and $R_B$, respectively.

Using (1)–(5), taking the spontaneous noise sources to be uncorrelated, and going over to the spectra, the voltage noise spectral densities across the external resistors can be written as [6], [8]

$$(Z/R_E)^2 S_{V_b} = [r_e - \beta(r_b + R_B)]^2 S_{I_b} + [r_e + r_b + R_B]^2 S_{I_b} + (\beta + 1)^2 S_{V_c} + 4kT[\beta + 1]^2(R_B + R_E) - 2[\beta + 1]Z + Z^2/R_E]$$

(6)

$$(Z/R_C)^2 S_{V_c} = \beta^2 r_b + R_B + r_e + R_E]^2 S_{I_b} + [r_e + r_b + R_B + r_e + R_E]^2 S_{I_b} + \beta^2 S_{V_c} + 4kT[\beta^2(R_B + R_E) + Z^2/R_C]$$

(7)

$$(Z/R_B)^2 S_{V_E} = [r_e + [r_e + R_E] S_{I_b} + [r_e + R_E]^2 S_{I_b} + S_{V_c} + 4kT[E_B + R_E - 2Z + Z^2/R_B]$$

(8)

with

$$S_{V_c} = I_B^2 S_{I_b} + I_E^2 S_{I_e} + 4kT[r_b + r_e]$$

(9)

and

$$Z = r_e + r_b + R_B + (\beta + 1)(r_e + R_E).$$

(10)

Here, $S_{I_b}$, $S_{I_e}$, $S_{R_b}$, and $S_{R_c}$ are the spectral noise densities of the spontaneous fluctuations $\Delta I_b$, $\Delta I_e$, $\Delta r_b$, and $\Delta r_e$ respectively. Considering (6)–(10), the importance of the internal series resistances can be seen. The influence of these resistances is twofold. They can produce LF noise and, they can influence the magnitude of the noise originating from the sources $S_{I_b}$ and $S_{I_e}$ by means of feedback.

For the circuit in Fig. 1(b) the fluctuations $\Delta I_E$, $\Delta I_B$, and $\Delta I_C$ can be expressed in terms of the spontaneous noise sources. With the help of (1)–(4), taking $R_B = R_C = R_E = 0$, and going over to the spectra, Kleinpenning found [8]

$$Z_0^2 \cdot S_{I_b} = [r_e - \beta r_b]^2 S_{I_b} + (r_e + r_b)^2 S_{I_b} + (\beta + 1)^2 S_{V_c}$$

(11)
\[ Z_0^2 \cdot S_{1C} = \beta^2 (r_x + r_b)^2 S_{1b} + (r_x + r_b + r_e)^2 S_{1r} + \beta^2 S_{1v} \tag{12} \]

\[ Z_0^2 \cdot S_{1B} = (r_x + \beta r_e)^2 S_{1b} + r_e^2 S_{1r} + S_{1v} \tag{13} \]

with

\[ Z_0 = r_x + r_b + (\beta + 1)r_e. \tag{14} \]

Note that for \( r_b = r_e = 0 \), we obtain \( S_{1C} = S_{1k}, S_{1B} = S_{1b}, \) and \( S_{1E} = S_{1e} + S_{1b} \).

Several remarks should be made with respect to the derivation of the noise formulas given by (6)-(8) and (11)-(13).

First, the Early effect has been neglected. Taking into account this effect one has to rewrite (2) as

\[ \Delta I_C = \Delta I_e + g_{mc} \Delta V_{eb} + h_{22} \Delta V_{be} \tag{15} \]

with

\[ \Delta V_{be} = -(R_C + r_x) \Delta I_C - I_C \Delta r_x - (R_B + r_b) \Delta I_B - I_B \Delta r_b + \Delta V_{be}^N. \tag{16} \]

Here, \( \Delta V_{be}^N \) is the fluctuation in \( V_{be} \) due to the Nyquist noise in \( R_C, r_x, R_B \) and \( r_b \). In modern transistors the output conductance \( h_{22} \) is very low, so that the term \( h_{22} \Delta V_{be} \) can be neglected.

Second, we neglect current crowding, leakage currents, and injection of electrons from the collector into the base.

Third, the base series resistance \( r_b \) consists of a part \( r_{b1} \) for the region outside the emitter and a part \( r_{b2} \) for the base region under the emitter. Consequently, we have a distributed base current. Hence, the base series resistance \( r_b \) and its fluctuations \( \Delta r_b \) have to be considered as effective quantities (see also Section IV-C). Current crowding in the base can be neglected on condition that \( I_B r_{b2} < kT/q \).

Fourth, with respect to the voltage-noise spectral densities \( S_{VC}, S_{VC}, \) and \( S_{VB} \), we find that till 1990 only expressions can be found where \( S_{1b} = S_{1e} = 0 \) in the literature. These expressions can be derived from (6)-(10) making the appropriate approximations. In the common-emitter configuration the voltage noise \( S_{VC} \) is mostly measured. With \( S_{1b} = S_{1e} = 0 \) and \( r_e = R_e = 0 \), (7) leads to the well known relation

\[ S_{VC}/R_C^2 = S_{1b} + \frac{\beta (r_b + R_b)^2}{r_x + r_b + r_e} \left[ S_{1r} + \frac{4kT}{r_b + R_b} \right]. \tag{17} \]

Fifth, with the help of the general formulas (6)-(10), one can determine the LF noise sources in bipolar transistors, as well as the magnitude of the series resistances \( r_b \) and \( r_e \). For that the transistor has to be set in a circuit with variable external base, emitter, and collector resistances. By measuring the LF noise at the emitter, base, and collector contact at different values of the external resistances and at different currents, the LF noise sources can be located. Some examples are presented in [8] and in Section V.

In the next section we shall present expressions for the spontaneous LF noise sources.

IV. LOW-FREQUENCY NOISE SOURCES

A. Base Current Noise

The current-noise spectral density of the spontaneous fluctuations in the base current \( S_{IB} \) can consist of several contributions. There always is shot noise and \( 1/f \) noise and, occasionally, there is generation-recombination (GR) noise and burst noise, or so-called random telegraph signal (RTS) noise. The shot noise contribution is given by the well known relation

\[ S_{IB} = 2qI_B/3f \tau_j. \tag{19} \]

Currently, the \( 1/f \) noise in bipolar devices is often discussed in terms of mobility fluctuations [3], [4]. According to the mobility fluctuation model, we have three expressions for the \( 1/f \) noise in the base current. If the base current and its noise is determined by carriers recombining in the space-charge region between emitter and base we have [9], [10]

\[ S_{IB} = 2qI_B/3f \tau_n. \tag{21} \]

where \( \tau_j \) is the carrier lifetime in the space-charge region, \( f \) the frequency, \( \alpha \) the Hooge parameter, \( W \) the effective width of the junction, \( n_i \) the intrinsic concentration, and \( A \) the emitter area. If the base current and its noise are determined by carriers injected from the base into the emitter, we have two expressions both for \( S_{IB} \) and for \( I_B \). If the width of the emitter \( W_E \) is thicker than the minority carrier diffusion length, \( L_n = (D_n \tau_n)^{1/2} \), then we have [9], [11]

\[ S_{IB} = 4qI_B/4f \tau_n. \tag{22} \]

and

\[ I_B = (qAD_n^{1/2}n_i^2NE^{1/2} \exp(qV_{eb}/kT) \tag{24} \]

where \( \tau_n \) is the minority carrier lifetime in the emitter, \( D_n \) its diffusivity, and \( N_E \) the dope concentration in the emitter. For \( W_E < L_n \) we obtain [4], [12]

\[ S_{IB} = \frac{4qI_B D_n}{fW_E^2(1 + D_n/n_i^2W_E)^2} \ln[1 + s_nW_E/D_n] \tag{25} \]

and

\[ I_B = qAD_n^{1/2}n_i^2NE(1 + D_n/n_i^2W_E) \exp(qV_{eb}/kT) \tag{26} \]

with \( s_n \) the recombination velocity of minority carriers at the emitter contact.

Sometimes GR noise or RTS noise in the base current is observed in bipolar transistors. The experimental results are discussed with the help of fitting formulas like \( S_{IB} = AI_B^k/(1 + 2\pi f \tau_j^2) \) with \( A \) and \( k \) parameters [14]. Burst noise and GR noise in bipolar transistors are often associated with traps or \( g-r \) centers near the emitter-base space-charge region.

GR noise in the base current can be attributed to fluctuations in the recombination (trapping) rate \( R_i \) of the excess carriers either in the space-charge region between emitter and base, or in the emitter, or at the emitter contact. These fluctuations
\[ S_{R_t}/R_t^2 = S_{N_t}/(Z_t - N_t)^2 \]

and

\[ S_{N_t} = 4\pi t_1(\Delta N_t^2)/[1 + (2\pi f t_1)^2] \]

with \( \Delta N_t^2 \) the variance of the fluctuations in \( N_t \), and \( t_1 \) the relaxation time of carriers in the trap. The quantities \( \tau_j \), \( \tau_n \) and \( s_n \) in (20), (22), and (24) are related to the trapping rate as \( \tau_j \sim 1/R_t \), \( \tau_n \sim 1/R_t \), and \( s_n \sim R_t \). If the base current is given by (20), (22), and (24) we have successively

\[ S_{I_e}/I_e^2 = S_{R_t}/R_t^2, \]
\[ S_{I_e}/I_e^2 = (1/4)S_{R_t}/R_t^2 \]

and

\[ S_{I_e}/I_e^2 = (1 + s_n W_E/D_n)^{-2}S_{R_t}/R_t^2. \]

Sometimes the \( 1/f \) noise in \( I_B \) is interpreted as a sum of GR spectra with a particular distribution of relaxation times. In that case the noise has a \( I_B^2 \) dependence. Since \( 1/f \) noise is observed over a broad frequency range, the \( \tau_j \)-distribution has to meet very specific requirements.

**B. Collector Current Noise**

Usually, the noise in the collector current is the sum of shot noise and \( 1/f \) noise. The shot noise is given by

\[ S_{I_c} = 2qI_C \]

and the \( 1/f \) noise, according to the mobility fluctuation model, by a similar expression as (23)

\[ S_{I_c} = \frac{\alpha q I_C D_p}{f W_B^2(1 + D_p/v_p W_B)^2} \ln [1 + v_p W_B/D_p]. \]

The collector current is given by

\[ I_C = q AD_p n_0^2/N_B W_B(1 + D_p/v_p W_B) \exp(qV_{eb}/kT). \]

Here \( D_p \) is the diffusivity of minority carriers in the base, \( W_B \) the base width, \( v_p \) the velocity of minority carriers in the base at \( x = W_B \), and \( N_B \) the dope concentration in the base.

It should be noted that the derivation of the expressions for both \( S_{I_e} \), in (23) and \( S_{I_c} \) in (30) can be found in [12]. This derivation is more accurate than in [3]. For \( D_p \ll v_p W_B \) and \( D_n \ll s_n W_E \) the expressions given in [3] and in [12] become the same.

### C. Series Resistance Noise

The internal base resistance \( r_b \) consists of contact resistance \( r_{bc} \), resistance between contact and emitter \( r_{b1} \) and resistance for the base region under the emitter \( r_{b2} \), thus \( r_b = r_{bc} + r_{b1} + r_{b2} \). The resistance \( r_{b2} \) always has Nyquist noise \((4\pi T/r_0)\) and can have \( 1/f \) noise, GR noise, and possibly, RTS noise. For a circular emitter with radius \( R_s \), Kleinpenning [20] found the \( 1/f \) resistance noise in \( r_{b2} \) to be

\[ S_{r_{b2}} = 4\pi r_0^2/3f N \]

with \( N \) the effective number of charge carriers in the total base region.

The internal emitter series resistance \( r_e \) consists also of contact resistance and bulk resistance. Here we have

\[ S_{r_e} = \alpha r_e^2/f N_e^2 \]

with \( N_e^* \) the effective number of charge carriers.

For any GR noise contribution we can similarly write

\[ S_{r_e}/r_e^2 = S_{N_e^*}/N_e^2 = \frac{4(\Delta N_e^2)^2}{1 + (2\pi f t_1)^2} \]

with \( \Delta N_e^2 \) the variance and \( t_1 \) the relaxation time. A similar expression holds for GR noise in \( r_e \).

### V. EXPERIMENTAL DATA

In this section we shall discuss a number of experimental results obtained during the last decade. First, we start with some results obtained from conventional bipolar junction transistors (BJT's) with deviations in the expected current dependence of the \( 1/f \) noise at higher emitter currents. These deviations are the first indication that series resistances influence the LF noise. Subsequently, we shall discuss recent experimental results from polysilicon-emitter BJT's and from heterojunction bipolar transistors (HBT's).

#### A. Conventional BJT's

Pawlakiewicz et al. [15] studied the \( 1/f \) noise in p+-n-p silicon BJT's. At higher collector currents (\( \sim 2 \) mA), they found the \( 1/f \) noise in the collector current to be less than proportional to \( I_C \). If the \( 1/f \) noise is due to mobility fluctuations, the noise density should be proportional to \( I_C \) (see (30)). This deviation may be ascribed to the influence of the emitter series resistance. According to (12) and (14) we have

\[ S_{I_{c_e}} = \left[ \frac{r_e}{r_e + (\beta + 1)r_e} \right]^2 S_{I_{c_e}} \]
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provided that \( r_c \gg r_b + r_e \), and that the contributions from both \( S_{ib} \) and \( S_{vc} \) can be neglected. At \( I_C = 2 \) mA they found \( S_{ic} \) a factor 4 too low. On the other hand, it holds both \( S_{ib} \) and \( S_{vr} \) can be neglected. At IC provided that

It cannot be excluded that the existence of some recombinations related \( 1/f \) noise is responsible for the contribution from the series resistances. Here we have

According to (13) this deviation can be ascribed to a noise contribution from the series resistances. Here we have

with \( S_{ib} \sim I_B \) and \( S_{vc} \sim I_B^2 \). Using (23) and (30) the Hooge parameter \( \alpha \) was found to be of the order of \( 10^{-8} \), both for the \( 1/f \) noise in the base current and in the collector current [15].

It is not possible to obtain \( \alpha \)-values from series resistance \( 1/f \) noise, since in [15] data are missing to calculate \( S_m \) and \( S_{ib} \).

It cannot be excluded that the existence of some recombination related \( 1/f \) noise is responsible for the contribution \( B_I \). In view of the specific requirements for the distribution of relaxation times such a contribution is not very likely. A clearer indication for the existence of series resistance \( 1/f \) noise will be given in Section V-B.

Zhu et al. [16] investigated the \( 1/f \) noise in n-p-n microwave transistors. The collector current noise was measured with an ac short-circuited base (\( R_B = 0 \)) and with \( R_E = 0 \). According to (7) and (12), and the approximation \( Z = Z_0 \approx r_\pi \), the \( 1/f \) noise in the collector current is given by

Zhu et al. established that the first term in (38) is considerably smaller than \( S_{ic} \), the third term has not been taken into account. Consequently, one can expect

Interpreting the contribution \( A_{IC} \) in terms of mobility fluctuations, Zhu et al. found a Hooge parameter of the order of magnitude of \( 10^{-8} \). It is not possible to determine \( \alpha \) values from \( S_{vc} \) for lack of data in [15].

The experimental results of Zhu et al. are replotted in Fig. 2(b) as \( S_{ic}/I_C \) versus \( I_E^2 \). An excellent linear relationship was found, which is a strong indication that the \( 1/f \) noise in series resistances becomes important at higher currents.

B. Polysilicon-Emitter BJT's

Polysilicon emitter bipolar transistors have higher current gain than conventional transistors. Such high current transistors are good candidates for analog applications. For these applications the LF noise performance of the transistor is very important. Here we shall discuss some experimental data of LF noise presented in the literature.

Kleinpenning and Holden [6], [17] investigated the low-frequency noise in self-aligned, polysilicon-emitter, n-p-n silicon BJT's, with emitter areas \( A_{0.5 \times 1.5, 0.5 \times 4.5, 0.5 \times 9.5} \), and \( 1.25 \times 4.5 \mu m^2 \), respectively. For all transistors the collector current at room temperature can be described by

For most devices at collector currents in the range of 0.1 \( \mu A \) - 1 mA, the base current followed the relation

Data are from [16], [17]. From Fig. 2(a) and with

Consequently, one can expect

As \( f \rightarrow 0 \), the \( 1/f \) noise can be strongly reduced by adjusting \( R_B = r_\pi /B - r_\pi \), and according to (6)
Fig. 3. White noise and 1/f noise versus $I_E$ of two polysilicon-emitter transistors in the common-collector configuration. The current-dependency lines are described by (40) and (41). The calculated values of $4kT(r_{e} + r_{h})$ are given by dashed lines, the upper line belongs to $A = 0.75 \mu m^{2}$ and the lower line the other one. (See [6]).

It can be concluded that the 1/f noise in $S_{IB}$ is dominant. Consequently, for the 1/f noise (6) and (40) reduce to

$$S_{1/f}^{IV} = |r_{e}/(\beta + 1)|S_{1/f}^{IV}.$$  (42)

Since $S_{1/f}^{IV} \sim I_E^{-1}$ and $r_{e} \sim I_B^{-1}$, the current noise $S_{1/f}^{IV}$ is proportional to $I_B$, which is predicted by the mobility fluctuation model (23).

Kleinpenning and Holden [6, 17] investigated about 15 transistors and they found ($f = 1$ Hz and $I_B = 10^{-8}$ A) the current noise $S_{1/f}^{IV}$ to be in the range of $3 \times 10^{-24} - 3 \times 10^{-23}$ $A^{2}/Hz$. So the quantity $fS_{1/f}^{IV}/I_B$ is in the range of $3 \times 10^{-16} - 3 \times 10^{-15} A$. Using (23), $\alpha$ values are found to be in the range of $2 \times 10^{-6} - 2 \times 10^{-5}$. At high currents ($I_E > 100 \mu A$) it was found $S_{1/f}^{IV} \sim I_B^{2}$, which can be ascribed to resistance fluctuations in either $r_{e}$ or in $r_{h}$. Using (33) and (34) $\alpha$ values in the range of $10^{-6} - 10^{-3}$ were reported.

Kleinpenning and Holden have also measured $S_{1/f}^{IV}$ in the CE-configuration with $R_E = 0$ and $R_B \gg r_{e} + r_{h} + (\beta + 1)r_{e}$, thus $Z \approx R_B$, and at emitter currents in the range of 1 $\mu A$–1 mA. In this case (7) reduces to

$$S_{VC}/R_C^2 = \beta^2 S_{IB} + S_{IE} + 4kT/R_C \approx \beta^2 S_{IB}.$$  (43)

The white noise observed agrees with $\beta \cdot 2qI_B$ and the 1/f noise with $\beta^2 \cdot S_{1/f}^{IV}$, taking the result from the CC-configuration measurements for $S_{1/f}^{IV}$. In other words, both the magnitude and the current dependence of $S_{1/f}^{IV}$, obtained in the CC-configuration at $I_E \leq 10 \mu A$, correspond with the results obtained in the CE-configuration in the current range of 1 $\mu A$ < $I_E$ < 1 mA.

In some transistors Kleinpenning and Holden [17] observed RTS noise or burst noise. In the CC-configuration the RTS noise can be removed by adjusting $R_E = r_{e}/B - r_{h}$ (see Fig. 4(a)). Consequently, the RTS noise stems from fluctuations in the base current. The magnitude of the RTS step in the base current $\Delta I_{B,RTS}$ was found to be almost independent of $I_E$ (see Fig. 4(b)). With respect to the RTS current step of about 20 nA, it is striking to notice the following. The base current is equal to $qP_{exc}/\tau$, with $P_{exc}$ the excess number of holes in the emitter and $\tau = W_{B}/2D_{e}$, the transit diffusion time in the emitter. A step $\Delta P_{exc}$ leads to a step $\Delta I_B = q/\tau \approx 10$ nA. So, low-frequency fluctuations in the number of excess carriers by trapping in the emitter could be the origin of RTS noise.

Pong-Fei Lu [18] studied the LF noise in self-aligned n-p-n bipolar transistors with a polysilicon emitter. The transistors were biased in the CE-configuration. Generally, at low frequencies he observed 1/f noise and sometimes burst (RTS) noise. In devices without burst noise he observed l/f noise and sometimes burst (RTS) noise or burst noise. In the CC-configuration he observed l/f noise and sometimes burst (RTS) noise. The magnitude of the RTS noise was found to be unchanged when the base current was varied, in line with the results of Kleinpenning and Holden (see Fig. 4). From the RTS noise spectra in [18] the RTS step $\Delta I_{B,RTS}$ can be estimated using the relation

$$S_{1/f}(f) = \frac{4\Delta I_{B,RTS}^2/\tau_{p}}{1 + (2\pi f\tau_{p})^2} = \frac{S_{1/f}(0)}{1 + (2\pi f\tau_{p})^2}$$  (44)

with $\tau_{p}^{-1} = \tau_{i}^{-1} + \tau_{h}^{-1}$ and $\tau_{e} = \tau_{i} + \tau_{h}$, where $\tau_{h}$ and $\tau_{i}$ is the average time in the high and low noise state, respectively. From (44) it follows:

$$\Delta I_{B,RTS} = \left[\tau_{p}S_{1/f}(0)/4\pi^2\right]^{1/2} \geq \left[S_{1/f}(0)/\tau_{p}\right]^{1/2}.  (45)$$

Here we have used the inequality $\tau_{p}/\tau_{p} \geq 4$. Using (45) the current steps for the RTS in Figs. 4 and 5 in [18] are found to be at least 15 nA, 7 nA, and 1 nA, respectively. These steps are of the same magnitude as the RTS steps in [17].

In transistors without burst noise Pong-Fei Lu observed only 1/f noise and shot noise. In device A with $I_B$ in the range of 0.5-10 $\mu A$ (i.e., $I_E$ in the range of 50 $\mu A$-1 mA), he found $S_{1/f}^{IV}$ to be proportional to $I_B^2$, instead of $I_B$ as expected for mobility fluctuations. In this current range Kleinpenning and Holden [17] observed a changeover in the...
current dependence of the noise due to series resistance effects. Note that Pawlikiewicz et al. [15] found \( S_{DB} \) to be proportional to \( I_E \) at low currents and proportional to \( I_B \) at higher currents (see Fig. 2). Such behavior can be ascribed to series resistance effects (see Section V-A). From the spectra presented in [18] the magnitude of the 1/f noise in terms of \( fS_{IB}^{1/f}/IB \) was found to be in the range of \( 5 \times 10^{-16} - 3 \times 10^{-15} \) A for \( IB \) values in the range of 1–5 μA. These values are comparable with the values observed by Kleppenning and Holden; \( 3 \times 10^{-16} - 3 \times 10^{-15} \) A. For a conventional diffused transistor with Al metal contact Pong-Fei Lu found \( S_{IB} = 2 \times 10^{-17} \) A at \( IB = 1 \) μA, which is comparable with the results presented in Fig. 2(a).

Siabi-Shahrivar et al. [21] investigated the 1/f noise in polysilicon emitter BJT’s. They claim that the introduction of the polysilicon contact significantly increases the 1/f noise in transistors. This conclusion is uncertain. Expressing the magnitude of the 1/f noise in the base current in terms of \( fS_{IB}^{1/f}/IB \), conventional transistors have values in the range of \( 10^{-17} - 10^{-12} \) A [15], [18], [20] and polysilicon emitter transistors in the range of \( 10^{-17} - 10^{-14} \) A [6], [17], [18], [22]. So the claim that polysilicon emitter transistors have higher 1/f noise is questionable.

It has been shown that the 1/f noise in polysilicon emitter BJT’s is strongly related to the type of surface treatment prior to polysilicon deposition [21]. It is not possible to discuss the results in [21] in more detail on the basis of (6)–(8), (11), and (12), since the authors did not give information about the circuit used for their noise measurements. However, some remarks can be made.

Figs. 2 and 4 in [21] present the input referred noise \( E_n(nV/\sqrt{Hz}) \) versus emitter area \( A_e \) at fixed emitter current \( I_E = 0.2 \) mA for four different types of BJT’s. After removing the errors in these figures, i.e., the noise data of the BJT’s with area \( 18 \times 6 \) μm² are placed at incorrect positions, we find the input noise \( E_n \) to be inversely proportional to the root of the emitter area \( A_e \). Such an area dependence can be expected, if the noise is due to 1/f noise in the base series resistance. According to (7) and (33) we then have

\[
E_n^2 = S_{V_T} = \alpha r_s^2 I_B^2 / I_E^2 \sim 1 / A_e. \tag{46}
\]

Note that in Fig. 3 the 1/f noise above \( I_E = 0.1 \) mA is also determined by series resistances, most likely by \( r_s \) [6].

In order to investigate the effect of emitter junction scaling on the noise performance, Siabi-Shahrivar et al. have studied three different BJT’s with varying junction depths. They found the referred noise \( E_n \) at constant \( I_E = 0.2 \) mA to be adversely affected by scaling down the vertical dimensions. However, they did not give information about the depth dependence of the base current \( I_B \). Normally, \( I_B \) increases with decreasing depth, so according to (46) \( E_n \) should increase with decreasing junction depth.

Finally, we discuss the results of Mounib et al. [22]. For different technological treatments given to the silicon surface prior to polysilicon deposition, they studied the base and collector 1/f current spectral densities as a function of base and collector current, respectively. For the interpretation of their results we have to use (12)–(14). Results are reported of \( S_{IB} \) versus \( I_B \) of the same device structure (\( A_e = 1000 \times 10^\mu m^2 \)) with two different technological treatments: type 1 with an important interfacial oxide and type 2 with no oxide layer. In view of the size of \( A_e \), the emitter series resistance \( r_s \) can be neglected [5]. Assuming \( r_s \ll r_T \), formula (13) reduces to

\[
S_{IB}^{1/f} = S_{IB}^{1/f} + r_s^2 S_{V_T} = \alpha I_B + bI_B^2. \tag{47}
\]

For \( I_B < 1 \) μA they found \( S_{IB}^{1/f} \sim I_B \). Just like in [6], [17] they found that for \( I_B > 10 \) μA the 1/f noise increases strongly with increasing \( I_B \). Comparing the experimental data with (47), the conclusion is reasonable that at low base currents the 1/f noise is in the base current and at high currents in the base series resistances. For type 1 they found \( fS_{IB}^{1/f}/IB \approx 10^{-10} \) A, and for type 2 \( \approx 3 \times 10^{-12} \) A. These values are lower than the values reported in [6], [17], [18]. Just as is reported in [21] the 1/f noise in BJT’s with an oxide layer is higher than without an oxide layer. This can be explained as follows. Since the diffusion-recombination length \( L_p \) in the emitter is of the order of 0.1 μm, we have \( L_p \leq W_E \) so that (21) prevails rather than (23). If the lifetime of minority carriers in the emitter is influenced by the chemical treatments, then the 1/f noise is too. Possibly, this may explain the differences in 1/f noise densities.

For the same transistors Mounib et al. [22] measured the collector current 1/f noise. For \( I_C < 10 \) μA both types 1, 2 have \( S_{IC} \sim I_C \) and the same noise magnitude. They found \( fS_{IC}^{1/f}/IC = 10^{-17} \) A, which is of the same magnitude as in Fig. 2(a). Above \( I_C = 30 \) μA the 1/f noise increases strongly with increasing \( I_C \). Now according to (12) we have

\[
S_{IC}^{1/f} = (3\tau_b/r_s)^2 S_{IB}^{1/f} + (3\tau_b/r_T)^2 S_{V_T}^{1/f}. \tag{48}
\]

The conclusion is reasonable that at low currents the noise is determined by \( S_{IC}^{1/f} \) and can be interpreted in terms of

\[
E_n^2 = S_{V_T} = \alpha r_s^2 I_B^2 / I_E^2 \sim 1 / A_e. \tag{46}
\]
mobility fluctuations of minority carriers in the base (30). Here, it should be noted that according to (30) the magnitude of $S_{Ve}^{1/f}$ has to be independent of the emitter technology, which is in agreement with the experimental findings by Mounib et al. at high currents the 1/f noise is due to either $S_{Ve}^{2/f}$ or to $S_{Ve}^{3/f}$. Both for the transistors with $A_e = 1000 \times 10^{-6}$ $\mu m^2$ and for small geometry transistors ($A_e = 2 \times 1 \mu m^2$ or $5 \times 2 \mu m^2$) there is influence of the chemical treatments only on the 1/f noise in the base current. They found that defects created at the Si-SiO$_2$ interface at the periphery of the emitter-base junction have a fundamental impact on the noise in the base current and a very low influence on the fluctuations in the collector current. This is not surprising, as such defects decrease the minority carrier lifetime and thus increase the noise (see (21)).

C. Heterojunction Bipolar Transistors (HBT's)

HBT's play an important role as sources at microwave and millimeter-wave frequencies. Upconversion of the 1/f noise provides information on how to design low-noise devices. Here, we shall present an overview of the literature on 1/f noise in GaAs HBT's during the last five years.

Kleinpenning and Holden [7] investigated the 1/f noise in n-p-n GaAs/AlGaAs HBT's with an emitter area of $2.5 \times 5 \mu m^2$. The internal series resistances of the emitter, base, and collector are roughly 40 $\Omega$, 80 $\Omega$, and 30 $\Omega$, respectively. The ideality factor for the collector current $I_C$ was found to be 1.3 and for $I_B$ it was 2.0. The current gain $\beta$ was found to be proportional to $I_C^{0.4}$, they found $\beta \approx 1$ at $I_C = 1 mA$ and $\beta \approx 20$ at $I_C = 1 mA$. Noise measurements were carried out in both the CC-configuration with $R_E \gg r_\pi$ and $R_B = R_C = 0$ and the CE-configuration with $R_B \gg r_\pi$, $R_E = 0$ and $R_C = 1 \, k\Omega$. In all devices 1/f noise was observed, mostly over at least three decades of frequency, generally in the range of 1 Hz-10 kHz. In Fig. 5 typical 1/f noise density plots are presented of $S_{Ve}$, $S_{Ve}$, and $S_{Ve}$ versus collector current $I_C$. The 1/f noise density $S_{Ve}$ is measured in the CC-configuration, the other two densities in the CE-configuration. For this situation (6)-(8) reduces to

\[
g_{\text{ine}}^2 S_{Ve} = \left(1 - \beta r_e/r_\pi\right) S_{Ve} b + S_{IL} + g_{\text{ine}}^2 S_{Ve} \tag{49}
\]

\[
S_{Ve}/R_e^2 = \beta^2 S_{Ve} + S_{IL} + \left(\beta/R_B\right)^2 S_{Ve} \tag{50}
\]

\[
S_{Ve}/R_e^2 = \left(1 + \beta r_e/r_\pi\right)^2 S_{Ve} + r_e/r_\pi^2 S_{Ve} + S_{Ve}/r_\pi^2 \tag{51}
\]

Here, $g_{\text{ine}} = (\beta + 1)/r_\pi$ is the emitter conductance of the intrinsic transistor, thus $g_{\text{ine}} = dI_E/dV_{bc}$. Interpretation of the experimental data of Fig. 5 in terms of the formulas given by (49)-(51) leads to the following results:

- At $I_C = 1 mA$, where $\beta \approx 1$, we obtain $S_{IL} \approx S_{Ib} \approx 5 \times 10^{-21} A^2/Hz$.
- At $I_C = 30 mA$, where $\beta \approx 4$, we obtain $S_{IL} \approx S_{Ib} \approx 6 \times 10^{-17} A^2/Hz$ and $S_{Ib} \approx 4 \times 10^{-10} A^2/Hz$.
- Above $I_C = 100 mA$ there is a change over in the current-dependences of both $S_{Ve}$ and $S_{Ve}$.

The changeover with respect to $S_{Ve}$ can be ascribed to the fact that the term $\beta r_e/r_\pi$ becomes dominant, i.e., larger than one. The change in the slope of $S_{Ve}$ versus $I_C$ can be ascribed to the term $g_{\text{ine}}^2 S_{Ve}$. In view of the scatter in the experimental data, it is difficult to determine exactly the current dependence of $S_{Ve}$. Therefore it is impossible to determine which contribution dominates $S_{Ve}$ or $S_{Ve}$.

In view of these results Kleinpenning and Holden concluded that at lower currents, i.e., $1 \mu A < I_C < 100 \mu A$ and $I_B < 25 \mu A$, the 1/f noise density $g_{\text{ine}}^2 S_{Ve}$ is practically determined by $S_{IL}$ and the density $S_{Ve}/R_e^2$ by $S_{Ib}$. They found $S_{IL} \sim I_C^4$ and $S_{Ib} \sim I_B^5$.

In Fig. 6 the results of $g_{\text{ine}}^2 S_{Ve}$ versus $I_C$ of three HBT's are plotted together with other data in the literature of $S_{Ve}$ versus $I_C$. In Fig. 7 $S_{Ve}/R_e^2$ versus $I_B$ of the same three HBT's as in Fig. 6 are shown, and for comparison other data of $S_{Ib}$ versus $I_B$. Comparison of the data both in Fig. 6 and in Fig. 7 shows a corresponding magnitude of the 1/f noise at lower currents. At higher currents there are differences, which can be ascribed to parasitic series resistances.

Tutt et al. [23] also studied the 1/f noise in GaAs/AlGaAs HBT's. They measured both $S_{Ic}(f)$ and $S_{Ib}(f)$. For frequencies below about 1 kHz, 1/f noise was observed. Above 1 kHz they often observed a Lorentz (GR) spectrum. Just like Kleinpenning and Holden, they found the 1/f noise in $S_{Ic}$ to be larger than in $S_{Ib}$. Some of their results are plotted in Figs. 6 and 7. Comparing the 1/f noise results of Tutt et al. with the results of [7], it can be concluded that the 1/f noise densities $S_{Ib}$ and $S_{Ic}$ in [7] and [23] are of the same magnitude. The GR noise is ascribed to traps with an activation energy of 0.16 eV. In view of the experimental data of Tutt et al., we suppose that the GR noise is due to fluctuations in the part of the base resistance below the emitter $r_e$. The argumentation is
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as follows. Considering the results in Figs. 2 and 3 in [23] we observe the following at low base currents ($I_B$):  

1) $S_{\text{IC}}^2 (I_B = 0.25 \text{mA}) / S_{\text{ROB}}^2 (I_B = 0.125 \text{mA}) \approx 10$. If the noise is due to fluctuations in $r_{q2}$, then according to (12) and (14) this ratio can be derived from the relation $S_{\text{IC}} = (\beta / Q_0) I_B^2 S_{\text{ADB}}$. If $Q_0 \approx r_{n}$ the ratio is found to be $36$, and if $Q_0 \approx (\beta + 1) r_{n}$ the ratio is $4.5$. Here we have used $\beta (0.25 \text{mA}) \approx 8.3$ and $\beta (0.125 \text{mA}) \approx 5.5$.

2) $S_{\text{IC}}^2 (I_B = 0.25 \text{mA}) / S_{\text{IC}}^2 (I_B = 0.25 \text{mA}) \approx 100$. According to (12) and (13) this ratio has to be $\beta^2 \approx 70$.

3) At higher base currents ($> 1 \text{mA}$) the GR noise disappears.

According to Tutt et al. the HBT then operates in the current crowding regime, which implies that the current through $r_{q2}$ becomes reduced and thus the GR noise from $r_{q2}$ does too.

In a more recent paper Tutt et al. [24] studied the LF noise in HBT’s in more detail. The results obtained are rather similar to the results in [23]. However, they made an important remark in [24]: “An analysis of device noise characteristics based on terminal noise properties may be highly misleading. Knowledge of the internal sources is important for complete understanding of the noise sources.” In Figs. 6 and 7 we have plotted some experimental values of the internal $1/f$ noise sources $S_{\text{IC}}$ and $S_{\text{IB}}$.

Jue et al. [25] investigated the LF noise in GaAs/AlGaAs HBT’s. Generally, the LF noise under low-bias conditions was found to be $1/f$ in nature. In Fig. 4 of [25] they have plotted $S_{\text{IC}}$ versus $I_B$, where $S_{\text{IC}}$ is measured in a circuit with $R_B = R_E = R_C = 0$. Using their $I-V$ plots and formula (12), the experimental results of Jue et al. lead to the results plotted in Fig. 6. From their results given in Fig. 6 of [25] we obtain $S_{\text{IB}} (1 \text{Hz}, I_B = 5 \mu\text{A}) \approx 1.5 \times 10^{-19} \text{A}^2/\text{Hz}$, which is plotted in Fig. 7.

Hayama et al. [26] fabricated a low-phase noise $K_u$-band oscillator using an HBT with a measured collector current $1/f$ noise of about $6 \times 10^{-17} \text{A}^2/\text{Hz}$ at $f = 1 \text{Hz}$ and $I_C = 1.2 \text{mA}$. This experimental result is plotted in Fig. 6.

Costa and Harris [14] have investigated the LF noise of $n$-$p$-$n$ AlGaAs/GaAs HBT’s as a function of bias current, device geometry, and extrinsic-base-surface condition. Their noise measurements were carried out in the CE configuration, where the noise power at the collector was measured. Using a simple low-frequency circuit model for the transistor and the gain of the system, the noise at the output was referred back to the input. According to [27] an equivalent input base noise current $S_{\text{In}}$ was defined. Since Costa and Harris did not present a formula which relates $S_{\text{In}}$ to the LF noise sources in the transistor, it will be done here. According to [27] the input noise voltage $S_{\text{Vin}}$ for a short-circuited output ($R_C = 0$) is defined by

$$S_{\text{Vin}} = [(r_b + R_B + r_n) / \beta]^2 S_{\text{IC}}.$$  \hfill (52)

The $S_{\text{In}}$ parameter is obtained from $S_{\text{Vin}}$ by assuming that $R_B$ has a very large value, specifically $R_B \gg r_n$.

$$S_{\text{In}} = S_{\text{Vin}} / R_B^2 \approx S_{\text{IC}} / \beta^2.$$  \hfill (53)

According to (7) and (12) for $R_B \gg r_b + r_n + (\beta + 1) r_c$ we obtain

$$S_{\text{IC}} = \beta^2 S_{\text{In}} + S_{\text{Is}} + (\beta / R_B)^2 S_{\text{VC}}.$$  \hfill (54)

and thus

$$S_{\text{In}} = S_{\text{IC}} + \beta^2 S_{\text{Is}} + S_{\text{VC}} / R_B^2 \approx S_{\text{Is}}.$$  \hfill (55)

In the discussion of the results of Costa and Harris, it will be assumed that they have used $R_B \gg r_b + r_n + (\beta + 1) r_c$, so that it holds that $S_{\text{In}} = S_{\text{Is}}$.

The observed current noise spectra $S_{\text{IB}}$ have three components: $1/f$ noise, burst noise, and white noise. A number of spectra can be found in [14]. These spectra were obtained from HBT’s with different emitter areas $A_e$ and from HBT’s with and without AlGaAs surface passivation ledge. We have replotted their data in Fig. 8, where $S_{\text{IB}}^{1/f}$ is plotted versus $I_B$. Here it should be noted that for the spectra given in [14], the corresponding value of $I_B$ was not always given. However, for a number of spectra it was possible to find out the lacking $I_B$, for example, with the help of the magnitude of the white noise $2qI_B$, or with the help of the values of $I_C$ together with the current gain $\beta$. From Fig. 8 we find that $S_{\text{IB}} = C I_B^{1.6}$, with $C$ almost independent of the emitter area, the presence of a passivation ledge, and the $A_1$ mole fraction. For comparison the relation $S_{\text{IB}} = C I_B^{1.6}$ is also plotted in Fig. 7. Concerning the observed burst noise, Costa and Harris argued that this noise is associated with traps in the neutral emitter or in the emitter-base space-charge region.

Finally, in Fig. 7 we have plotted some experimental data of $S_{\text{IB}}^{1/f}$ obtained by Plana et al. [28] on nonpassivated self-aligned GaInP/GaAs HBT’s.

In Section VI we shall discuss the experimental results obtained from BJT’s and HBT’s.
VI. DISCUSSION AND CONCLUSION

In conventional high-quality silicon bipolar transistors, the emitter series resistance can be neglected, the base series resistance is low, and the current dependence of the base current l/f noise is determined by shot noise in the base and collector currents, and by Nyquist noise in the base and emitter series resistances. Both the base and the collector currents have l/f noise. The l/f noise in the base current can be described by the empirical relation found from the results in Figs. 7 and 8.

\[ S_{lb}(f) = C_B I_B f \times \frac{1}{f} \frac{A^2}{Hz} \]

with \( C_B \approx 10^{-10} \frac{A^2}{Hz} \) and \( k \approx 1.6 \).

The value of \( C_B \) is almost independent of the emitter area, surface passivation ledge, the technology procedure, and the ideality factor typically in the range of 1.2–2. Here, it should be noted that the current dependence of the base current l/f noise density \( S_{lb} \) deviates from the dependence predicted by both the mobility fluctuation model (19), (21), (23) and the recombination velocity fluctuation model (28). The magnitude of the l/f noise in terms of \( f S_{lb}/I_B \) is in the range of \( 10^{-14} \) to \( 10^{-12} \) A for \( 1 \mu A < I_B < 1 \mu A \), which is some decades higher than in polysilicon emitter BJTs.

The l/f noise in the collector current observed by Kleinpenning and Holden [7], and by Tutt et al. [23], [24] can be described by the empirical relation (see Fig. 6)

\[ S_{lc} = C_C I_C f \times \frac{1}{f} \frac{A^2}{Hz} \]

with \( C_C \approx 10^{-12} \frac{A^2}{Hz} \) and \( k \approx 1.3 \).

Here, it also has to be noted that the current dependence of \( S_{lc} \) deviates from the one predicted by mobility fluctuations. The ideality factor of the HBT's in [7] is \( n = 1.3 \), which implies that the collector current noise is proportional to \( \exp(V_{be}/kT) \). According to (30) such a proportionality is predicted by the mobility fluctuation model for l/f noise in collector currents with ideality factor \( n = 1 \). For comparison we have drawn the relation between \( S_{lc} \) and \( I_C \) in Fig. 6, using (30) with \( D = 50 \text{ cm}^2/\text{s}, s = 10^6 \text{ cm/s}, W_B = 1.3 \mu m, \) and \( \alpha = 10^{-4} \). Here, we have to note that \( \alpha \) values of the order of \( 10^{-4} \) in GaAs are often reported in literature [29]. Now it can be concluded that the experimental values of \( S_{lc} \) are of the same order of magnitude as the values predicted by the mobility fluctuation model.

In what has been stated above it is clear that there is much to be desired with respect to the physical interpretation of the l/f noise both in the base and in the collector current of HBT's. The current dependence of both \( S_{lc} \) and \( S_{lb} \) is not well-understood. The question whether the l/f noise stems from mobility fluctuations or from trapping noise cannot be solved with the help of the current dependences of both \( S_{lc} \) and \( S_{lb} \).

In some HBT's burst (RTS) noise is observed. This type of noise may be associated with traps in or close to the emitter [14]. At higher bias currents the influence of the series resistance on the LF noise behavior of HBT's becomes noticeable.
References


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