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Liquid bridge length scale based nondimensional groups for mapping transitions between regimes in capillary break-up experiments

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Criteria to identify transitions between dynamic self-similar linear thinning regimes of liquid bridges are of utmost importance in order to accurately interpret results in capillary break-up rheometry. Currently available criteria encompass many experimental difficulties or rely on numerical approaches. Here, we introduce a different set of nondimensional groups, $Oh_L = \eta_{in}/\sqrt{\gamma\rho L}$ and $a = R/L$, based on the experimentally relevant axial length scale of a liquid bridge L , for viscous-dominated fluids undergoing capillary break-up in air. This framework is further extended to encompass the effect of outer viscous fluids. As a result, we present a two-dimensional operating map in which the boundaries are set by fluid properties and a single geometrical parameter, related to the experimental configuration. This approach establishes guidelines to correctly interpret experimental data and identify transitions in capillary break-up experiments of liquid bridges surrounded by fluids of different viscosities.

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Capillary break-up has been extensively employed in the past as a tool to study the thinning behavior of complex fluid bridges and to extract material properties in extensional flows such as the transient (apparent) extensional viscosity, or the longest relaxation time [1,2]. Nonetheless, a successful application of this technique relies on a proper identification of the underlying dynamics, originating either from a balance or dominance of single material properties that causes the minimum liquid bridge radius R_{min} to exhibit a certain scaling $R_{min} = Hf(t)$, with $f(t)$ some function of time t . In most cases, similarity solutions were needed to determine the necessary numerical prefactors H for a quantitative evaluation of a scaling regime [3]. A multitude of dynamical regimes and $f(t)$, such as viscopillary (V) [4], elastocapillary (EC) [5], inertia capillary (IC) [6,7], and inertia viscous (IV) [8], have been identified in the literature based on the relevant force balance. Additional regimes were highlighted in more complex scenarios, for instance, when the viscosity of the surrounding fluid cannot be neglected [two-fluid viscous (LV) and line-sink flow (LSF) regimes [9,10]], for bubbles undergoing capillary thinning in fluids of various viscosities [11] or for confined flows [12]. A comprehensive description can be found in Refs. [1,13,14].

*These authors contributed equally to this work.

Intensive theoretical studies, usually based on scaling arguments, were carried out to formulate criteria that allow one to identify the presence of these regimes and their transitions [13,15]. This is in particular necessary for regimes that exhibit the same $f(t)$ [as the linear V, IV, and LV (LSF) regimes], so that an experimentally observed scaling is not sufficient for their identification. However, Eggers and Villermaux [13] address that discrepancies exist between proposed criteria for V to IV transitions and experimental observations [16,17], possibly depending on the overall geometry, which can also be seen in Ref. [18]. One cause lies in limitations to access criteria that focus on the thinning stages close to break-up, hence close to or below (optical) resolution limits. Second, effective criteria based on local velocities, local gradients, or Reynolds numbers [19] require information that is hardly experimentally available and rely on numerical calculations. Third, and most important, the experimental axial length scales of the liquid bridge have so far not been taken into account. Although case-specific geometrical parameters were employed to determine global behavior and regime transitions, they are usually buried in prefactors and arbitrary constants.

The purpose of this Rapid Communication is therefore to establish a systematic framework to identify transition criteria between linear thinning regimes in liquid bridges, solely based on material properties and characteristic dimensions of different experimental setups. To this end, we introduce in the following a set of nondimensional groups based on the experimentally relevant axial length scale of the liquid bridge. The concept of an axial Ohnesorge number Oh_L , along with the nondimensional radius a , is initially introduced for Newtonian, viscous-dominated fluids undergoing capillary break-up in air. Subsequently, the analysis is extended to encompass the effect of outer fluids of significant viscosity. Experimental limits, which depend on the setup configuration, are employed to identify the observable regimes and their transitions. As a result, a two-dimensional (2D) operating map is introduced, in which the boundaries are set by our dimensionless groups and the dependent scaling relations. This map is an alternative guideline to identify regimes and interpret experimental observations for viscous liquids surrounded by air and fluids of different viscosities.

For Newtonian fluids, the balance controlling the radial thinning behavior has so far been given in terms of the global Ohnesorge number $\text{Oh} = \eta_{\text{in}}/\sqrt{\gamma\rho R}$ that compares radial viscous and inertial contributions (where η_{in} is the shear viscosity, γ the surface tension, ρ the density, and R the characteristic radial dimension of the liquid bridge). For a viscous-dominated thinning (V regime), Papageorgiou [4] exploited a similarity solution to show that the prefactor in the linear decay of the minimum radius of a slender liquid bridge $R_{\text{min}} \sim -H\gamma t/\eta_{\text{in}}$ takes on the value $H = 0.0709$ [20]. As the liquid bridge thins, inertia becomes progressively more significant [21], leading eventually to a transition to the also linear inertia-viscous regime (IV), for which $H = 0.0304$ [8]. However, as indicated above, a transition criterion between the V and IV regime that scales with Oh [13] deviates up to orders of magnitude for different experimental setups. We propose that the underlying difference between the experiments is the length L of the liquid bridge, which is so far missing in the dimensional analysis. Including an axial length scale L , it is straightforward to show that the Buckingham π theorem yields as one possible solution for the now two alternative groups

$$\text{Oh}_L = \frac{\eta_{\text{in}}}{\sqrt{\gamma\rho L}}, \quad a = \frac{R}{L}, \quad (1)$$

and thus as a transition criterion $\text{Oh}_L^2 a$ that can also be derived balancing axial inertial and viscous stresses. Both groups now incorporate with the axial length scale L an unconventional nondimensionalization of the fluid properties that captures, however, the essential geometrical differences between experimental setups, which was generally not possible with the traditional nondimensionalization using an often arbitrary initial radial dimension R . In the most commonly used capillary break-up techniques, the liquid bridge is held between two fixed boundaries: in capillary break-up extensional rheometry (CaBER) experiments [20] between circular plates with adjustable distances of $\text{O}(1 \text{ cm})$, in a Rayleigh-Ohnesorge jetting extensional rheometer (RO-JER) [22] between equidistant $[\text{O}(100 \text{ }\mu\text{m})]$ droplets on a flying jet, while dripping-onto-substrate

extensional rheometry (DoS) [23] probes a liquid bridge of $O(1 \text{ mm})$ confined between a nozzle and a substrate. Contrary to unconfined liquid *filaments*, extensively studied by Schulkes, Basaran, and Hutchings [24–27], the liquid *bridge* length (and thus L) is fixed for a capillary break-up experiment [13], but differs up to two orders of magnitude between the different configurations.

The significance of the axial length scale is supported by a transition criterion between the V and IV regime recently introduced by Li and Sprittles [28], which they suggested to take place when the local Reynolds number $\text{Re} = \rho u L / \eta_{\text{in}}$ (where u is the local axial velocity at an axial distance L away from the point of minimal axial velocity) reaches a critical value of $\text{Re} = 0.85$ at the point of maximum axial velocity u_{max} (at L_{max}). One can decouple Re (and conveniently avoid the experimentally difficult to access local velocity) into Oh_L and a by approximating the slender liquid bridge with a cylindrical geometry. Replacing in Re the axial velocity via the strain rate $\dot{\epsilon} = u/L = -2\dot{R}/R$, using the linear radius decay of Papageorgiou for viscous fluids [4], yields $\text{Re} = (2H\rho\gamma L^2)/(\eta_{\text{in}}^2 R) = 0.1418/(\text{Oh}_L^2 a)$.

V to IV. We can now determine the critical transition criteria for the dimensionless radius a exclusively based on fluid properties using the axial Oh_L of Eq. (1), once the critical liquid bridge length scale L is introduced. Without using numerical methods, a critical axial length scale L , defined as the axial distance L_{max} between the point of maximum and zero axial velocity (analogously to Ref. [28]), can be accessed from the velocity profiles derived from the experimentally obtained liquid bridge shapes. In the V regime, this L_{max} is predicted to scale with time only as $\sim (t_b - t)^{0.175}$ [3,4], and this near time independence has been numerically [28] and experimentally (see the Appendix) confirmed. Using the numerically determined transition criterion of $\text{Re} = 0.85$ [28] would give $(\text{Oh}_L^2 a)_{\text{crit}} = 0.17$. However, taking into account the experimentally observed deviations from the ideal cylindrical shape via an experimentally observed correction factor of 1.5 (see the Appendix) gives for the transition from V to IV

$$a_{\text{crit}} = \frac{R_{\text{crit}}}{L} = \frac{0.11}{\text{Oh}_L^2}. \quad (2)$$

V to LV. Next, we apply this alternative nondimensionalization via L to identify the transitional criteria also in the presence of an outer immiscible fluid of significant viscosity, assuming the inner fluid to be incompressible and the density mismatch between the two fluids $\Delta\rho$ insignificant [29,30]. Lister and Stone [9] have shown that, even for low viscous outer fluids, the drag exerted by the outer liquid can no longer be neglected when break-up is approached. Introducing the nondimensional viscosity ratio $p = \eta_{\text{in}}/\eta_{\text{out}}$ of inner to outer fluid, for $p \gg 1$ the flow inside the liquid bridge is predominantly a uniaxial extension and causes a radially decaying shear drag on the outer fluid [see Fig. 1(a)]. They approximated this drag as the shear stress induced by a cylinder sliding axially through the outer fluid, yielding the momentum balance [in terms of a of Eq. (1)]

$$\frac{\gamma}{R} = 3p\eta_{\text{out}}\dot{\epsilon} - \frac{B\eta_{\text{out}}}{2a^2}\dot{\epsilon}, \quad (3)$$

where $B = 2/|\ln a|$ is a dimensionless coefficient [9]. The dimensionless group that arises when balancing inner and outer fluid stresses on the right-hand side of Eq. (3) is $pa^2|\ln a|$, which describes the transition from the V regime, where viscous stresses generated by the outer fluid are negligible, to one in which they control the thinning behavior (LV). Again, we can describe the transition in terms of a critical radius,

$$a_{\text{crit}}^2 |\ln a_{\text{crit}}| = \frac{1}{3p}. \quad (4)$$

LSF to LV. As pointed out by Sierou and Lister [10], a drastically different physical picture is seen for small viscosity ratios ($p \ll 1$). In the outer fluid, the flow is a nearly pure radial extension, resembling a line distribution of sinks, while a parabolic shear (Poiseuille) flow occurs in the inner

FIG. 1. (a) High-resolution images from CaBER experiments performed with surrounding immiscible outer liquids. The schematics highlights the differences in the expected inner and outer flow profiles for $p = 18.7 \gg 1$ and $p = 0.002 \ll 1$, respectively. (b) 2D operating map as a function of the dimensionless groups Oh_L and p . The derived criteria are used to delimit the areas within which specific regimes and transitions can be experimentally detected. Circled green letters correspond to the capillary break-up experiments for various L , and inner and outer fluid viscosities of Fig. 2.

liquid, as illustrated in Fig. 1(a). The momentum balance takes on the form

$$\frac{\gamma}{R} = \frac{4up\eta_{out}L}{R^2} + \eta_{out}\frac{u}{L}, \quad (5)$$

in which u is the radially averaged velocity in the axial direction in the inner fluid. Balancing the two terms on the right-hand side in Eq. (5) establishes the transition from a thinning regime dominated by the radial drag of the outer fluid [line-sink flow (LSF)] to the point where viscous friction of the inner fluid can no longer be neglected (LV), and determines a dimensionless group p/a^2 . The critical transition criterion can then be rewritten as

$$a_{crit} = \sqrt{4p}. \quad (6)$$

Observation limits for transitions. The transitional criteria for a introduced above are defined solely based on material properties and one geometrical parameter via the dimensionless groups Oh_L and p . It is crucial to note that an a_{crit} can vary significantly for the same fluid due to the intrinsically different axial dimensions and length scales L employed in the various capillary break-up techniques CaBER [20], DoS [23], and ROJER [22]. This also entails that the same regimes and transitions might not necessarily be observable in capillary break-up experiments performed on the same fluid, but with different techniques (and thus different L). However, since L is observed to not change significantly in time in the V regime, this geometry-dependent length scale can be used to assess the observation range for different setups. The derived transitional criteria can be reworked as

$$Oh_L = \sqrt{\frac{0.11}{a_{crit}}}, \quad p \gg 1 = \frac{|\ln(a_{crit})|^{-1}}{3a_{crit}^2}, \quad p \ll 1 = \frac{a_{crit}^2}{4}. \quad (7)$$

Setting a_{crit} equal to the upper and lower observation limits of the radius for a given L of a setup allows us to determine *a priori* for which Oh_L , $p \gg 1$, or $p \ll 1$ an a_{crit} can be experimentally observed. Since most regimes are based on a slenderness assumption (i.e., $a = R/L \ll 1$), a first limit is set by an upper radius R_{up} , so that $a_{crit} \leq a_{up} = R_{up}/L$ in order for a transition to be observable. Using Eq. (7), a_{up} identifies then the critical global $Oh_{L,up}$ below which no transition but only the IV regime is observed. Similarly, the upper slenderness limit a_{up} can also be used to determine the viscosity ratio $p_{up} \gg 1$ below which only the LV regime is visible for a set L . An upper criterion for $p \ll 1$ can, however, not be derived based on the same argument in a straightforward fashion. Due to the quadratic nature of the liquid bridge profile in the LSF regime [32], L is much smaller compared to

the other cases [see, for example, the image for $p \ll 1$ in Fig. 1(a)] and the bridge only becomes sufficiently slender when the transition to LV itself takes place. Nonetheless, a slenderness-based limit $p_{\text{up}}^{\ll 1}$ can still be used to determine the critical viscosity ratio below which the LSF regime can be detected right before transitioning to the slender LV regime.

The lower critical boundary is set by the radial resolution limit R_{res} , which varies significantly with the experimental detection technique [11] and is usually disregarded in numerical studies. As for the upper limit, from $a_{\text{crit}} \geq a_{\text{res}} = R_{\text{res}}/L$ the lower limits $\text{Oh}_{\text{L,res}}$, $p_{\text{res}}^{\gg 1}$, and $p_{\text{res}}^{\ll 1}$ are obtained via Eq. (7).

All the aforementioned limits are illustrated in Fig. 1(b) where a 2D map describes the observable regimes and transitions in terms of Oh_{L} and p and thus the respective radii (once the fluid properties and in particular the axial length L of the setup are known).

Experimental verification. To verify our introduced criteria and limits, we use the map in Fig. 1(b) to predict the behavior and transitions for a number of experiments encompassing the 2D parameter space. The capillary break-up experiments are performed using a CaBER rheometer (Thermo Haake, high-speed video-imaging re-equipped). a_{up} is calculated assuming a slenderness limit $L/R = 10$ [28], and a_{res} is calculated based on the limit of the optical setup, which can accurately resolve down to a radius of $5 \mu\text{m}$. The geometrical parameter L is determined following the Appendix, and is experimentally found to be directly related to the final plate separation distance. Water and glycerol-water mixtures are used as inner fluids, and air and silicon oils of different viscosities as outer fluids.

To show the importance of the geometry to determine the onset of the V to IV transition, in a first series of experiments [A, B, and C in Fig. 1(b)] we move through the map down the vertical axis for a high, fixed value of p . The experiments are performed with the same inner fluid ($\eta_{\text{in}} = 0.365 \text{ Pa s}$, $\gamma = 65 \text{ mN m}$) surrounded by air ($p = 24\,333$), while the geometrical factor L is changed by varying the final plate distance. The temporal evolution of the minimum radius is shown in Fig. 2(a) for the three cases, together with the thinning predictions for the V regime ($H = 0.0709$) and the IV regime ($H = 0.0304$). Figure 2(a) clearly illustrates how the window between R_{up} and R_{crit} for the observation of a transition drastically increases by increasing L . Moreover, R_{crit} markedly corresponds to the radius at which experimental data start deviating from the theoretical V thinning, thus accurately predicting the onset of a transition to IV. A second series of experiments [D and E in Fig. 1(b)] shows the effect of increasing viscosity of the outer fluid while keeping L and inner fluid properties constant ($\eta_{\text{in}} = 0.518 \text{ Pa s}$). With air as the outer fluid, case D ($p = 34\,435$) is comparable to case A, where the transition to IV is below the resolution limit, as shown by the minimum radius evolution in Fig. 2(b). By adding an outer liquid of sufficiently high viscosity ($p = 96$), R_{crit} calculated with Eq. (4) lies now within the experimentally detectable range and nicely corresponds to the experimentally observed onset of the LV regime in Fig. 2(ii). Moving to the other side of the map towards low viscosity ratios, case F in Fig. 1(ii) ($\eta_{\text{in}} = 10^{-3} \text{ Pa s}$, $p = 0.002$) represents an area of the map at the limits of experimental accessibility. Nonetheless, the R_{min} evolution in Fig. 2(c) shows that Eq. (6) precisely predicts the transition from LSF to LV.

To conclude, in this Rapid Communication, we introduce a theoretical framework for capillary break-up experiments to determine the critical transition radii between dynamical regimes when viscous stresses are governing the inner or outer fluid flows (or both). Our criteria depend solely on fluid properties via an alternative set of nondimensional groups incorporating the axial length scale L of the liquid bridge, which is for slender filaments in the V regime directly related to the axial dimension of the experimental setup. The criteria describe a 2D map to be used as a guideline to correctly pinpoint the observability of transitions between linear thinning regimes in experiments, as proven by examples covering a wide parameter range. Still, further experiments are needed to refine the inner part of the parameter space. In particular, the IV to LV transition is indicated to take place at $a \sim p^{-1/2}$ [9], but the correlation of the length scale L to the geometrical parameters of the bridge in the IV regime is unexplored. A full comprehension of predominantly viscous fluids will allow us to expand the map to more difficult scenarios, including the presence of

FIG. 2. Minimum radius evolution ($R_{\min}$) in time, with t_b as the break-up time, for several fluids and geometrical conditions in CaBER experiments performed in air [(a), (b) (open circles)] and with an outer liquid [(b) (open squares), (c)]. Solid dots represent calculated R_{crit} . Thinning curves in A are shifted 10 ms apart for clarity. (a) Experimentally detectable regimes are determined by the set geometrical conditions. For the same fluid ($\eta_{\text{in}} = 0.365$ Pa s, $\gamma = 65$ mN m), R_{crit} via Eq. (2) shifts to larger radii and the experimental window ($R_{\text{up}} - R_{\text{res}}$) expands as the geometrical parameter L increases (right to left: 480, 600, and 1000 μm). Consistently, the thinning dynamics appear to be solely V dominated for the lowest L (open squares), whereas a region following the IV scaling is clearly distinguishable for the highest L (open triangles). R_{crit} predicted with Eq. (2) matches the deviation of the data from the predicted V scaling ($H = 0.0709$, red solid line) towards the IV scaling ($H = 0.0304$, orange dashed-dotted line). (b) Thinning curves of the same inner fluid ($\eta_{\text{in}} = 0.518$ Pa s, $\gamma = 63.7$ mN m and 30.0 mN m for D and E, respectively) at comparable geometrical conditions show different behaviours depending on the outer medium viscosity (open circles $p = 34435$, open squares $p = 96$). For $p \gg 1$, the transition from V ($H = 0.0709$, red solid line) to LV regime [$H(p) = 0.02$ [31], blue dashed line] is detectable only if η_{out} is sufficiently high to fulfill the condition $p_{\text{res}} \ll p \ll p_{\text{up}}$. (c) For $p = 0.002$, R_{crit} according to Eq. (4) correspond to the deviation from LSF ($H = 0.5$, blue solid line) to the LV regime [$H(p) = 0.04$ [10], blue dashed line].

viscoelasticity, for which the operating space could be expanded to 3D by introducing the Deborah (De) or Weissenberg (Wi) numbers.

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APPENDIX

To decouple Re into Oh_L and a , the liquid bridge was approximated as a perfect cylinder for which the axial velocity $u = \dot{L}$ increases linearly along the bridge axis. Nonetheless, the self-similar profiles of actual fluid bridges exhibit an axial curvature [Fig. 3(a)], which causes a significant deviation of $u(z)$ from linearity. Here, we introduce an experimental method to determine the radially averaged axial velocity $u_a(z, t)$, a numerical correction factor C accounting for this deviation for the determination of a_{crit} [Eq. (2)], and the length L_{max} at $u_{a,\text{max}}$.

$u_a(z, t)$ [Fig. 3(b)] can directly be obtained from the experimentally observed evolution of the bridge shape, following the approach of Rothert *et al.* [16]. For this the cumulative volume $V_{\text{cumul}}(z = z_0 + i\Delta z, t) = \sum_{z_0}^{z_0 + i\Delta z} \Delta z \pi R^2(z_0 + i\Delta z, t)$ is determined from the radius evolution [with $z_0(t)$ the position of the minimum radius, and Δz the pixel size]. Assuming zero axial velocity at $z_0(t)$, the axial velocity at position z is

$$u_a(z, t) = \frac{1}{\pi R^2(z, t)} \frac{dV_{\text{cumul}}(z, t)}{dt}. \quad (\text{A1})$$

FIG. 3. (a) Capillary thinning evolution of a Newtonian fluid with $\eta_{in} = 0.365$ mPa s in air and with $L_{max} = 900$ μ m. R_{crit} calculated from the linear evolution of u (black solid dot, high-resolution image in the inset) overestimates the V to IV transition, which is instead correctly captured by R_{crit} calculated incorporating the corrective factor C in Eq. (2) (black solid star). The enlargement of the inset shows the visible difference between the ideal cylinder geometry (black dashed lines) and the actual profile (red solid lines). (b) Temporal evolution of $R(z)$ and $u_a(z)$ in a capillary break-up experiment of a glycerol-water mixture in air ($\eta_{in} = 0.365$ mPa s) with $L_{max} = 900$ μ m (-18.33 ms $< t - t_b < -6.33$ ms at $\Delta t = 0.66$ ms). Inset: The deviation of the actual profile from the ideal cylinder geometry implicates a large difference at L_{max} between $u_a = 0.15$ m/s (red solid line) and $u = 0.22$ m/s (black dashed line) calculated assuming a linear evolution of the axial velocity. (c) Direct comparison between the temporal evolution of R_{min} (open symbols) and L_{max} (solid symbols), determined from the experimental u_a profiles. The characteristic length remains approximately constant throughout the complete bridge evolution for case A of Fig. 2 (top, red squares). Also for cases B (middle, orange circles) and E (bottom, blue triangles) L_{max} remains constant in the V regime, up to the transitions to the asymmetrical thinning regimes (IV or LV).

Due to axial curvature at the bridge end bulges, the actual average axial velocity profile exhibits a sinusoidal shape [Fig. 3(b)], allowing us to determine a u_{max} at L_{max} . Plotting $L_{max}(t)$ in Fig. 3(c) shows that, within the V regimes, L_{max} remains approximately constant for different experimental conditions of Fig. 2. The inset in Fig. 3(b) shows the overestimation of the velocity at $z = L_{max}$ when assuming a linear increase of u with z . Evidently, also the calculated R_{crit} in Fig. 3 (solid dot, calculated from $a_{crit} = R_{crit}/L_{max} = 0.17$ Oh $_L^2$) lies then above the actual transition radius compared to experimental data, while the theoretical V and IV scalings (red solid and orange dashed lines, respectively) suggest a much later transition. To correct for this overestimation, $C = u_{act}/u$ at L_{max} has been calculated for several CaBER experiments performed on V-dominated fluids at different L . As expected for self-similar thinning, C assumes a constant value of 1.5, and is used to quantitatively correct the criterion derived for a_{crit} [Eq. (6)]. The corrected R_{crit} [Fig. 3(a), black solid star] corresponds then to the deviation from the V scaling, indicating the transition to the IV regime.

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