Homogeneous nucleation of water between 200 and 240 K: New wave tube data and estimation of the Tolman length

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(Received 6 June 2005; accepted 14 July 2005; published online 12 September 2005)

We have measured homogeneous nucleation rates of water at 200–240 K in the carrier gas helium, in the range of $10^{13} - 10^{17}$ m$^{-3}$ s$^{-1}$ using an expansion wave tube. The rates agree well with the results of Wölk and Strey [J. Phys. Chem. B 105, 11683 (2001)] in the range of overlap (220–240 K), and are summarized by the empirical fit $J = S \exp[4.6 + 0.244T - (906.8 - 2.914T)/(\ln S)^2]$, with $J$ the nucleation rate in m$^{-3}$ s$^{-1}$, $S$ the supersaturation, and $T$ the temperature in K. We find that the supersaturation dependence of both our rates and those of Wölk and Strey is lower than classical theory predicts, and that the critical cluster is smaller than the classical critical size. These deviations are explained in the framework of the Tolman theory for surface tension, and the “Tolman length” is estimated from our experimental results. We find a positive Tolman length that increases with decreasing temperature, from about 0.1 Å at 260 K to (0.6±0.4) Å at 200 K. We present a nucleation rate expression that takes the Tolman length into account and show that both the supersaturation and temperature dependence are improved, compared to the classical theory.


I. INTRODUCTION

Vapor-liquid nucleation of water plays an important role in our environment and numerous industrial processes. It is the first step in the phase transformation of the only substance that occurs naturally in liquid, solid, and vapor forms. In 1897, Wilson$^1$ studied the onset of nucleation by measuring the critical supersaturation; for about 30 years, researchers have also been able to determine the rate of the homogeneous nucleation of water—an overview of experiments is given in Ref. 2. A recent example of accurate rate measurements are the experiments by Wölk and Strey,$^3$ performed between 220 and 260 K in a nucleation pulse chamber.

In 2002, Peeters et al.$^4$ published nucleation rates obtained in a pulse-expansion wave tube, down to 200 K. A striking feature of these data was a jump in nucleation rates at 207 K, which was interpreted as a transition from vapor-liquid to vapor-solid nucleation. To confirm this transition, we repeated Peeters’s measurements in 2003; these new measurements in the range of 200–240 K and some experimental improvements are presented in this paper. Our new data did not show any transition, so we reanalyzed the results of Peeters et al. It was found that an inaccuracy in vapor fraction calculations had caused the apparent jump; the corrected data (published separately$^5$) show no evidence of a transition in the nucleation process. Our experimental nucleation rates are summarized by an empirical fit, which we will compare with Wölk and Strey’s data in the range of overlap, 220–240 K.

It is usually assumed that the supersaturation dependence of the nucleation rate is accurately predicted by classical nucleation theory (CNT). Equivalently, it is assumed that CNT correctly predicts the number of molecules in the critical cluster. We show that these assumptions do not hold for our experiments and those of Wölk and Strey. The deviations from the classical predictions will be explained with Tolman’s surface-tension theory, which is briefly described. At the end of the article, we will estimate from our experiments the “Tolman length,” a parameter that describes the dependence of the surface tension on droplet size.

II. CLASSICAL NUCLEATION THEORY

Although a complete expression of the nucleation rate was presented as early as 1935 by Becker and Döring,$^6$ developments are still ongoing. Some recent improvements have focused on properly accounting for translation of the drop,$^7$ the influence of the spinodal,$^8$ and cluster size fluctuations.$^9$ To analyze experiments we will use the nucleation rate expression from CNT, because it is still the most widely used theory. The classical rate $J_{cl}$ is given by

$$J_{cl} = K \exp(-W_{cl}/kT).$$

(1)

Here $k$ is the Boltzmann constant, $T$ is the absolute temperature, and $W_{cl}$ is the work of formation of a critical cluster: a cluster that is in unstable equilibrium with the surrounding vapor. The classical value of the formation work is

$$W_{cl} = \frac{16\pi\sigma_s^2 v^2}{3(kT\ln S)^2},$$

(2)

with $\sigma_s$ the surface tension of the planar liquid-vapor interface, $v$ the molecular volume, and $S$ the supersaturation. For vapor-carrier gas mixtures at near-atmospheric pressure, the supersaturation can be expressed as
\[ S = p_v / p_e = y p / p_e, \]  
\[ K = \frac{2 \sigma_{\infty} v_1 S}{kT}, \]  
where \( m_1 \) is the mass of a molecule. This expression for \( K \) contains a factor \( S \) instead of the \( S^2 \) in the CNT result. We will use this modification (known as the 1/S correction factor) because it makes the equilibrium cluster size distribution satisfy the law of mass action, although it is not the correct correction that does so.

In CNT, the number of molecules \( n_{cl}^* \) in the critical cluster is given by the so-called Gibbs-Thomson equation
\[ n_{cl}^* = \frac{32 \pi \sigma_{\infty} v_1^2}{3 (kT \ln S)}. \]

If we assume that the cluster is a sphere with radius \( R_{cl}^* \) and that each molecule occupies a volume equal to the molecular volume, so that the total cluster volume is \((4 \pi/3)(R_{cl}^*)^3 = n_{cl}^* v_1\), we find for the critical radius
\[ R_{cl}^* = \frac{2 v_1 \sigma_{\infty}}{kT \ln S}. \]

A further important relation in nucleation research is the “nucleation theorem” developed by Kashchiev and recently generalized by Bowles et al. It relates the experimentally measurable \( J(S) \) dependence of constant temperature to the molecular composition of the critical cluster. Applied to one-component nucleation of a condensed phase in a dilute vapor, the nucleation theorem reads
\[ n^* = \left( \frac{\partial \ln J}{\partial \ln S} \right)_T - 1, \]  
with \( n^* \) the actual number of molecules in the critical cluster.

### III. TOLMAN’S THEORY

In reality, a droplet is a heterogeneity which is characterized by a gradually changing density. In the thermodynamics of Gibbs, this density fluctuation is replaced by a simpler two-phase system: a hypothetical system that consists of a homogeneous spherical droplet embedded in a homogeneous vapor. The pressure of the hypothetical vapor \( p_{vap} \) is simply taken equal to the pressure in the real system far away from the droplet. On the other hand, the pressure inside the imaginary droplet \( p_{liq} \) is not the pressure in the center of the real density fluctuation, but the pressure of a hypothetical bulk liquid at the same chemical potential as the uniform-density vapor. This equality of chemical potentials implies that we restrict our analysis to critical droplets.

The infinitely thin interface between the cluster and the vapor is called the “dividing surface;” its position can be freely chosen. For any dividing surface, the work of formation is given by the exact expression
\[ W = 4 \pi (R^*)^2 \sigma(R^*) - (4 \pi/3)(R^*)^3 \Delta \rho, \]
where \( R^* \) is the radius of the droplet (the location of the dividing surface) and \( \Delta \rho = p_{liq} - p_{vap} \). Because \( W \) and \( \Delta \rho \) are well-defined physical quantities that do not depend on the choice of a dividing surface, we see that the surface tension \( \sigma \) must depend on this choice. [Once \( R^* \) is chosen, Eq. (8) can be seen as a definition of \( \sigma \).] A commonly used dividing surface is the “surface of tension” (indicated by a subscript \( s \)), for which the so-called Laplace equation is valid in its simplest form:
\[ R^*_s = 2 \sigma_s (R^*_s) / \Delta \rho, \]
where \( \sigma_s \) is the surface tension at the surface of tension. Another choice is the “equimolar dividing surface” (indicated by subscript \( e \)), with a radius \( R^*_e \) that is chosen such that
\[ 4 \pi \int_0^\infty [\rho(R) - \rho_s] R^2 dR = (\rho_t - \rho_s) \frac{4}{3} \pi (R^*_e)^3. \]

We now define the “Tolman length” \( \delta \) as the radial distance between the equimolar dividing surface and the surface of tension:
\[ \delta = R^*_e - R^*_s. \]

The value of \( \delta \) may depend on the droplet size and can be positive or negative. Tolman derived that for relatively large droplets \( (R \gg \delta) \) and for a \( \delta \) that is independent of droplet radius, the dependence of surface tension on droplet size is
\[ \frac{\sigma_s (R^*_e)}{\sigma_{\infty}} = \frac{1}{1 + 2 \delta / R^*_e}. \]

In the so-called capillarity approximation, the real surface tension is approximated by \( \sigma_{\infty} \). Eq. (9) then becomes
\[ R_{cl}^* = 2 \sigma_{\infty} / \Delta \rho, \]
with \( R_{cl}^* \) the radius in the capillarity approximation. Taking the ratio of Eqs. (9) and (13) gives
\[ \frac{R^*_e}{R_{cl}^*} = \frac{\sigma_s (R^*_e)}{\sigma_{\infty}} = \frac{1}{1 + 2 \delta / R^*_e}, \]
which can be rewritten into
\[ R^*_e = R_{cl}^* - 2 \delta. \]

This result states that the surface of tension is located at a distance of \( 2 \delta \) from the classical radius. From Eqs. (11) and (15) it follows immediately that
\[ R^*_e = R_{cl}^* - \delta, \]
which shows that the equimolar dividing surface lies between the surface of tension and the classical radius at a distance of \( \delta \) from each.
To evaluate the work of formation, we choose the surface of tension as a dividing surface. The Laplace equation, Eq. (9), can then be used to eliminate $R^*$ from Eq. (8), yielding

$$W = \frac{(16\pi/3)[\alpha(R_s^*)]^3}{\Delta p^2}.$$  

(17)

In the capillarity approximation, $\alpha_{cl}$ is used instead of $\alpha$, so that $W_{cl} = (16\pi/3)\alpha_{cl}^3/\Delta p^2$. The ratio of the real and classical work of formation is then

$$\frac{W}{W_{cl}} = \left[\frac{\alpha(R_s^*)}{\alpha_{cl}}\right]^3 = \left[\frac{R_s^*}{R_s^{cl} + 2\delta}\right]^3 = \left(1 - \frac{2\delta}{R_s^{cl}}\right)^3.$$  

(18)

The second equality follows from Eq. (12) and the last equality from Eq. (15). This result was derived earlier by Abraham$^{17}$ and by Schmelzer and Baidakov.$^{18}$

We can now introduce a corrected nucleation rate $J_{Tub}$, in a form analogous to Eq. (1):

$$J_{Tub} = K \exp(-W^*/kT) = K \exp[-(W_{cl}^*/kT)(1 - 2\delta R_s^{cl})^3],$$  

(19)

where $K$ is the classical prefactor of Eq. (4), $W_{cl}^*$ is given by Eq. (2), and $R_s^{cl}$ is given by Eq. (6). The parameter $\delta$ remains unknown at this point and must be estimated by other means. We will describe how to determine it from nucleation rate data in Sec. V F.

IV. EXPERIMENTS

A. Setup

The experiments were performed in a so-called pulse-expansion wave tube, which is a modified shock tube (see Fig. 1). The high-pressure section (HPS) serves as a test section in which nucleation occurs. It contains the vapor-carrier gas mixture, which is produced in a dedicated mixture preparation device.$^{21}$ We used helium (purity 99.999%) as a carrier gas and varied the molar fraction of water vapor between 2 x 10^-4 and 5 x 10^-3, at initial total pressures in the range of 160–270 kPa. The water was purchased from Merck (proanalyse, resistivity >1 MΩ cm). A diaphragm separates the HPS from the low-pressure section (LPS) that contains helium only, at a pressure of about 110 kPa. Before the experiment, the HPS is flushed for 1 h with the test mixture, to ensure adsorption equilibrium with the walls. After the rupture of the diaphragm, the pressure history of Fig. 2 is obtained at the HPS end wall. The pressure dip or pulse, occurring immediately after the large pressure decrease, is caused by pressure waves reflecting from widening W in the LPS (Fig. 1) and traveling back into the HPS. The temperature history has a similar shape and is calculated from the pressure using the ideal-gas isentropic relation

$$T = T_0(p/p_0)^{(\gamma-1)/\gamma},$$  

(20)

where $\gamma=c_p/c_v$ is the ratio of the specific heats, and $p_0$ and $T_0$ are the initial pressure and temperature, respectively. The $\gamma$ value is corrected for the presence of water vapor in the mixture and lies close to 5/3, the $\gamma$ of pure helium.

At the beginning of the pulse, the temperature drops by about 10 K. Because the equilibrium vapor pressure $p_e$ depends strongly on temperature, $p_e$ decreases to less than half of its value and consequently the supersaturation $S$ more than doubles. This, in turn, causes the nucleation rate to increase by about six orders of magnitude (see Fig. 2).

At the end of the pulse, the nucleation process is quenched; the amount of droplets formed after the pulse is negligible. The supersaturation remains higher than unity, however, so that the droplets that were formed during the pulse grow to a detectible size. Close to the end wall of the HPS, the number density of droplets $\rho_{exp}$ is determined by a combination of constant-angle Mie scattering at 90° and extinction measurements of a laser beam with a wavelength of 514.2 nm. Finally, the nucleation rate is found as the ratio of the droplet density and the pulse duration $\Delta t$:

$$J = \rho_{exp}/\Delta t.$$  

(21)

B. Improvements

1. Pressure measurement

The pressure changes at the end wall of the HPS were recorded by a piezoelectric pressure transducer (Kistler type 603B). Transducers of this type measure relative pressure changes, that is, the output voltage difference is proportional to...
to the pressure difference. Their fast response is a prerequisite for our experiments, but they also have a number of disadvantages. The proportionality constant can only be determined by calibration to a known pressure change, and such a calibration must be done regularly. In addition, the head of the piezoelectric transducer is sensitive to thermal gradients and must be coated; also, the tension which results from mounting influences the characteristics.

To increase the reliability of the pressure measurement, we modified the setup in 2004 to allow an in situ calibration of the piezoelectric transducer during the experiment. This was achieved by installing an additional transducer at the end wall, capable of measuring absolute pressures. The new piezoresistive transducer (Kistler type 4043A5) can be calibrated statically (at constant pressure) and is less sensitive to thermal gradients and mounting tension. Although the piezoresistive transducer cannot accurately measure fast pressure changes, it can be used to calibrate the piezoelectric one. The piezoelectric signal is scaled such that it is equal to the piezoresistive signal at a time just before and just after the experiment; in this way the proportionality constant is determined. In our 2004 series of experiments, the maximum deviation of the proportionality constant from the mean was 0.1%, which is within the accuracy of the method of about 0.2%.

2. Pulse conditions

With our setup the droplet density can be determined with a reproducibility better than 5%. However, when calculating the nucleation rate with the traditional method of Eq. (21), this accuracy is lost because the pulse duration is much more uncertain. Ideally, the pulse duration can be defined as the length of the bottom of the pulse where the pressure and temperature are constant. In reality, the edges of the pulse are never sharp and the pressure varies between these edges. The experimenter then has to determine the pulse boundaries by visual inspection of the pressure signal; a subjective method which causes an uncertainty in $\Delta t$ that can be as large as 30%. In addition, the uncertainty in the position of the pulse edges also introduces errors in the pulse conditions $p_{\text{pulse}}$ and $T_{\text{pulse}}$, which are found by averaging over the range between the pulse edges.

To overcome these difficulties, Wölk and Strey$^3$ fitted the pressure around the pulse with a trapezoidal construction, illustrated earlier by Viisanen et al.$^{22}$ Our more irregular pulses cannot be easily fitted to such a shape. Instead, we use a method that allows us to obtain the nucleation rate without the subjective definition of the pulse duration: an integration over the entire pressure history. This technique was used by Miller et al.$^{23}$ and (in a modified form) by Schmitt and co-workers.$^{24,25}$ In our case, we integrate a theoretical nucleation rate $J_m(t) = J_m[T(t), S(t)]$ over the entire pressure history, resulting in a modeled droplet density $\rho_m$: 

$$\rho_m = \int J_m(t) dt. \quad (22)$$

Because the value of $J_m$ outside the pulse is orders of magnitude lower than it is during the pulse, $\rho_m$ does not depend on the integration limits as long as the pulse is included in the integration interval. By a similar integration, the pulse conditions $p_{\text{pulse}}$ and $T_{\text{pulse}}$ can be found. For that purpose we define the pulse pressure as a weighted average over the entire pressure history, where the weight factor is proportional to the number of droplets that were formed at a certain pressure. Using this definition, the weighted pressure average is computed by taking the nucleation rate as a weight factor:

$$p_{\text{pulse}} = \frac{\int p(t) J_m(t) dt}{\int J_m(t) dt} = \frac{1}{\rho_m} \int p(t) J_m(t) dt. \quad (23)$$

The corresponding pulse temperature $T_{\text{pulse}}$ is calculated from $p_{\text{pulse}}$ by the isentropic relation of Eq. (20). Alternatively, the temperature could be calculated as a weighted average; then $T_{\text{pulse}} = \rho_m^{-1} \int T(t) J_m(t) dt$. In practice, the difference between the two methods is small (1 mK) so either method can be used. The pulse supersaturation $S_{\text{pulse}}$ is found from Eq. (3).

To obtain the experimental nucleation rate that corresponds to the pulse parameters $T_{\text{pulse}}$ and $S_{\text{pulse}}$, we correct the theoretical nucleation rate with the ratio of experimental and modeled droplet densities,

$$J_{\text{exp}} = \frac{\rho_{\text{exp}}}{\rho_m} \times J_m(T_{\text{pulse}}, S_{\text{pulse}}). \quad (24)$$

The three values $T_{\text{pulse}}$, $S_{\text{pulse}}$, and $J_{\text{exp}}$ constitute the result of the integration method and are used in all subsequent graphs and calculations. As mentioned before, the advantage of the integration method is the elimination of subjectiveness; a disadvantage is the need for a nucleation rate model. However, as we will see later, the choice of a particular model has little influence on the results.

C. Accuracy

Nucleation rates are known with about 25% accuracy. The uncertainty in the conditions of the 2003 results is 0.7% in $p_{\text{pulse}}$, 0.5 K in $T_{\text{pulse}}$, and 3%–8% in $S_{\text{pulse}}$ (higher uncertainty at low temperature). Because of the new pressure calibration, the conditions of the 2004 results are known with a slightly higher accuracy of 0.4% in $p_{\text{pulse}}$, 0.3 K in $T_{\text{pulse}}$, and 3%–4% in $S_{\text{pulse}}$.

V. RESULTS

A. Experimental supersaturations

Experiments were performed at pulse temperatures between 200 and 240 K at constant nucleation pressures of about 100 kPa. Figure 3 shows the supersaturation during the nucleation pulse, obtained with Eq. (3), for our experiments and those of Wölk and Strey.$^3,26$ With decreasing temperature, the supersaturation must be increased to keep nucleation rates within the experimental measurement window, in our case $3 \times 10^{13} - 3 \times 10^{17}$ $m^{-3}$ $s^{-1}$. At equal temperature, the supersaturations of Wölk et al. are lower than ours, reflecting the lower nucleation rate window of $10^{11} - 10^{15}$ $m^{-3}$ $s^{-1}$ of their nucleation pulse chamber. Their
B. Empirical fit of nucleation rates

We proceed now to the way our nucleation rates were obtained. Lacking a nucleation rate model, the first step was to analyze the experiments with the traditional method, by manually defining the pulse duration and using Eq. (21) to obtain \( J \). This procedure yielded a set of preliminary nucleation rates. In order to get a nucleation rate model, the function

\[
J_{\text{cl}}(T,S) = J_0 S \exp \left[ a_0 + a_1 T - b_0 + b_1 T \right] \tag{25}
\]

was then fitted to the preliminary 2003 nucleation rate data, with \( a_0, a_1, b_0, \) and \( b_1 \) as fitting parameters and \( J_0 = 1 \text{ m}^{-3} \text{s}^{-1} \). This function is based on the empirical formula of Miller et al.,

but has fewer fitting parameters and a pre-exponential factor of \( S \) instead of \( S^2 \). The factor \( J_0 \) is included for dimensional consistency. When the logarithm of Eq. (25) is taken, the model becomes linear in the parameters, so that they can be determined by a least-squares linear fitting procedure.

Having available a nucleation rate model, the next step was an analysis using the integration method. The maximum differences of the integration results with the preliminary dataset were 40% in \( J \), 0.3 K in \( T \), and 0.4% in \( p \). The fact that these differences are not too large indicates that the accuracy of the traditional method is acceptable. However, because the pulse integration method eliminates human subjectiveness, it decreases the scatter in the results.

To improve the accuracy even further, Eq. (25) was again fitted to the newly obtained data, after which the pulse integration method was reapplied to update nucleation rates, temperatures, and pressures. This procedure was repeated several times until the fitting parameters changed by less than 0.01%. The results were

\[
a_0 = 4.6, \quad a_1 = 0.244 \text{ K}^{-1},
\]

\[
b_0 = 906.8, \quad b_1 = -2.914 \text{ K}^{-1},
\]

valid for temperatures between 200 and 240 K and nucleation rates in the range of \( 3 \times 10^{13} - 3 \times 10^{17} \text{ m}^{-3} \text{s}^{-1} \). The fit function \( J_{\text{cl}} \) reproduces almost all of our 2003 nucleation rates within a factor of 2 (Fig. 4), which is an acceptable error when we take into account the uncertainties of the experimental rates, temperatures, and supersaturations.

Finally, to examine the sensitivity of the integration method on the specific model used, we analyzed all experiments using \( J_{\text{cl}} \) [Eq. (1)] as the model instead of Eq. (25). Although the predictions of \( J_{\text{cl}} \) differ by several orders of magnitude from \( J_{\text{fit}} \), the resulting \( J_{\text{exp}} \) changes only a few percent. We therefore conclude that the integration method is relatively insensitive to the rate model and the resulting nucleation rates are reliable.

C. Comparison with the Wölk and Strey results

In Fig. 5 the nucleation rates of the three isotherms in our 2004 series and those of three Wölk and Strey isotherms are plotted as a function of the supersaturation. For comparison, the fit of the 2003 rates has been evaluated at the mean temperatures of the six isotherms (dashed lines). The fit agrees well with the Wölk and Strey isotherms, both in value and in slope, and provides a plausible extension of their nucleation rates to lower temperatures and higher supersaturations.

The points of the 2004 isotherms, indicated by open circles, again show the scatter that is partially caused by
deviations of the nucleation temperature. It is possible to correct for the scatter in temperatures in a model-independent way, as follows. For each experiment, we estimate the supersaturation $S_{\text{corr}}$ that is obtained when the temperature is made equal to the mean isotherm temperature $T_{\text{mean}}$, while keeping the nucleation rate constant. In a first-order approximation, $S_{\text{corr}}$ is then

$$S_{\text{corr}} = S + \left(\frac{\partial S}{\partial T}\right)_J (T_{\text{mean}} - T).$$  


To use this expression, the derivative $(\partial S/\partial T)_J$ is required. Looijmans and van Dongen$^{20}$ and Luijten and van Dongen,$^{27}$ who also used Eq. (27), calculated it from CNT. Instead, to analyze our results in a more theory-independent way, we derived it from our experimental data, as follows. First, Eq. (25) was solved for $S$ to obtain $S$ as a function of $J$ and $T$; then, partial differentiation with respect to $T$ gave the required derivative. The corrected results, indicated by the filled circles in Fig. 5, indeed show that the correction succeeds in reducing the scatter.

D. Comparison with classical nucleation theory

Let us now compare the experimental nucleation rates with the CNT predictions of Eq. (1). This is conveniently done by plotting the ratio of the experimental rates and the CNT rates as a function of temperature, as in Fig. 6(a). Only at 260 K there is agreement between experiment and theory; at lower temperatures the deviation increases—at 200 K the experimental rates are a factor $10^7$–$10^9$ higher than predicted. This deviation, which is caused by the incorrect temperature dependence of the CNT nucleation rate, is well known and observed in almost all water nucleation experiments$^2$ and also in the nucleation of other substances such as nonane$^{28}$ and $n$-alcohols.$^{29}$ Apart from the incorrect temperature dependence, the vertical scatter of the scaled rates is higher than expected, exceeding an order of magnitude for several Wölk and Strey isotherms. The Wölk and Strey scaled rates also show a systematic positive deviation from our 2003 rates, at equal temperature. This seems to contradict the agreement found earlier in Fig. 5, but the difference is actually caused by the incorrect supersaturation dependence of the CNT nucleation rate, as we will show later.

E. Critical cluster sizes

To determine the critical size with the nucleation theorem of Eq. (7), the slope of the isotherms must be determined. In most cases the isotherms are slightly curved, but when a straight line is fitted to the isotherm, the slope of the line is found to be a good approximation of the slope at the center of the isotherm.

In the case of isotherms that have much scatter or consist of a small number of points, another consideration should be made. The scaled error in $\ln S$ (the error in $\ln S$ times the slope of the line) is higher than the error in $\ln J$, so we fitted the lines by applying the least-squares method in the $\ln S$ direction. That is, in the $\ln J$-$\ln S$ plot of Fig. 5, we minimized the sum of squared horizontal residuals. The resulting lines are also shown in that figure. In the case of the isotherms of Wölk and Strey that have little scatter it is not necessary to specify the direction of minimization, because it has only a small (2%) influence on the slope. (Only for the
260-K isotherm, which has more scatter, the difference is 9%.

For comparison with theory we want to assign a single theoretical $n^*$ value to the isotherm, which is not straightforward since $n^*_\text{cl}$ varies along the isotherm. One could evaluate $n^*_\text{cl}$ at each isotherm point and then take the mean, as Wölk and Strey did, but we will specify a reference temperature and supersaturation at which $n^*_\text{cl}$ is evaluated. It is reasonable to take as a reference supersaturation value the mean of $\ln S$ of the points, because the lines are fitted in a plot with $\ln S$ as abscissa, and fitting a straight line to a curved isotherm gives the slope in the center of this isotherm. As a reference temperature we will take the mean of the temperatures of the isotherm points.

The empirical fit of the 2003 data of Eq. (25) also allows us to obtain an estimate of the critical cluster size. In particular, from Eqs. (7) and (25) we derive that

$$n^*_\text{fit} = \left( \frac{\partial \ln J/\text{fit}}{\partial \ln S} \right)_T - 1 = \frac{2(b_0 + b_1 T)}{(\ln S)^3}. \tag{28}$$

Using the experimental temperature and supersaturation values, an $n^*_\text{fit}$ value can be calculated for each experiment of the 2003 series.

In Fig. 7, the experimental critical sizes $n^*_\exp$ obtained with the nucleation theorem, are plotted as a function of the theoretical critical sizes $n^*_\text{cl}$ from Eq. (5). In all cases the experimental value lies below the CNT prediction. The vertical error bars shown are 90% confidence intervals. Our $n^*_\exp$ values have larger vertical error bars than Wölk and Strey’s because our isotherms have more scatter and consist of fewer experimental points.

Contrary to our findings, Wölk and Strey$^3$ concluded that their experimental critical sizes did agree with the $n^*_\text{cl}$ predictions. There are three reasons for this difference. First, we fitted lines to the isotherms by minimizing horizontal—instead of vertical—residuals in the $\ln J/\ln S$ plot. Second, Wölk and Strey used the nucleation theorem in the form $n^* = (\partial \ln J/\partial \ln S)$, ignoring the supersaturation dependence of the kinetic prefactor $K$. Our expression has $(\partial \ln J/\partial \ln S) - 1$ at the right-hand side, so that we find $n^*_\exp$ values that are 1 lower than theirs. The largest difference is caused by our model for the surface tension, which gives up to 4.5% higher values than the Wölk and Strey fit (see Appendix). As a result, our $n^*_\text{cl}$ values are higher than those found by Wölk and Strey.

In Sec. V F we describe how the differences between $n^*_\exp$ and $n^*_\text{cl}$ can be explained in the framework of Tolman’s theory.

F. Estimation of the Tolman length

In the earlier description of the Tolman correction, clusters were measured by their radius, whereas the experimental critical sizes are found as numbers of molecules. With the help of the equimolar dividing surface from Eq. (10), the radius can be related to the number of molecules,

$$\frac{4}{3} \pi R^3 = n^* v_1 \quad \text{or} \quad R^* = R_1 (n^*)^{1/3}, \tag{29}$$

with $R_1 = (3v_1/4 \pi)^{1/3}$. From Eq. (16) it then follows that the real critical cluster size differs from the classical size as

$$n^* = [(n^*_\text{cl})^{1/3} - \delta R_1^3], \tag{30}$$

where we also used that $R^*_\text{cl} = R_1 (n^*_\text{cl})^{1/3}$. Rewriting Eq. (30) gives the Tolman length as a function of the real and classical critical sizes,

$$\delta = R_1 [(n^*_\text{cl})^{1/3} - (n^*_\exp)^{1/3}], \tag{31}$$

where we wrote the real critical size as $n^*_\exp$ to indicate that this is the quantity that is found from experiments. Equation (31) can be used to calculate the Tolman length from a plot such as Fig. 7, where a $\delta$ value is found for each $(n^*_\text{cl}, n^*_\exp)$ point. The resulting $\delta$ values are plotted in Fig. 8 as a function of the nucleation temperature. All Tolman lengths are positive because, as we saw earlier, the experimental critical sizes are smaller than predicted. The $\delta$ values that belong to our 2003 results agree well with the $\delta$ calculated from the Wölk and Strey data and suggest that $\delta$ increases with decreasing temperature, reaching a value of about 0.9 Å at 200 K. The $\delta$’s from the 2004 results, on the other hand, do not exhibit such a strong temperature dependence and lie lower than the other two datasets. The error bars are rather large, so the 2004 $\delta$’s cannot be said to disagree with the other results.

Now that we know the size and magnitude of the Tolman length, we will examine how it influences the nucleation rate predictions. We start by analyzing the effect of a constant $\delta$ of 0.4 Å, arbitrarily chosen as an average value in the range of 200–260 K. The corrected nucleation rate $J_{\text{tot}}$ of Eq. (19) then predicts a nucleation rate that is about six orders of magnitude higher than the $J_\text{cl}$ rate. This is illustrated by the $J_{\exp}/J_{\text{tot}}$ ratio in Fig. 6(a) that is consequently about six orders lower. Apart from this vertical offset, the vertical scatter in our data as well as the data of Wölk and Strey decreases.
parameter remains: the Tolman length, describing the strength of the size dependence of surface tension. By matching the experimental critical sizes with the Tolman predictions, the Tolman length could be determined. We find a positive Tolman length, which means that the surface tension decreases with decreasing droplet size. The magnitude of the Tolman length increases with decreasing temperature, from about 0.1 Å at 260 K to (0.6±0.4) Å at 200 K. These values are of the same order as the molecular diameter of water, which is commonly used as an estimate of the Tolman length.\textsuperscript{14,30} Abraham\textsuperscript{17} estimated δ at half the thickness of a molecular layer in the liquid and gave for water a value of δ=1 Å, which is comparable to our findings.

We developed a nucleation rate expression that includes the Tolman size-dependent surface tension. For a constant positive Tolman length of 0.4 Å, the corrected rates have an improved supersaturation dependence and are about 10\textsuperscript{6} times higher than the CNT rates. As an illustration, we have shown that including a temperature-dependent Tolman length may also bring the temperature dependence of the rates in agreement with experiment. Then only a division by a constant factor is needed to make the theoretical rates agree within one order of magnitude with our experiments of 2003 and those of Wölk and Strey.

The nucleation rates of our 203-K isotherm of the 2004 series deviate about one order of magnitude from the 2003 rates, as can be seen in Fig. 5. This systematic deviation cannot be explained by the experimental uncertainty of the nucleation rates; therefore, it can be said that the 2003 and 2004 rates do not agree with each other at low temperature. Moreover, the slope of the 203-K isotherm also deviates from the slope of the 2003 fit, which results in lower Tolman lengths of the 2004 data. We have tried to find a reason for the differences; possibly, the 2004 results were influenced by a change in measurement position (in 2004, the distance between the laser beam and the end wall was increased from 5 to 25 mm). However, according to numerical simulations,\textsuperscript{31} this change should not influence the nucleation conditions. The issue is therefore still unresolved.

The values we obtained for the Tolman length should be regarded as rough estimates. In deriving Eq. (A2) it was assumed that δ/R is small, which is not the case for all experiments. For example, the experiment with the smallest n\textsuperscript{c} of 10 has a δ of about 0.8 Å giving δ/R\textsubscript{c}≈0.2, so that δ<<R is no longer satisfied. Moreover, the predictions of the Tolman length are sensitive to the surface-tension model that is used, because σ\textsubscript{∞} appears as a third power in the n\textsuperscript{c} formula of Eq. (5). If an alternative surface-tension model is used (the IAPWS model of the Appendix) we find that the low-temperature (200–210 K) Tolman lengths decrease by about 0.25 Å. Still, we may conclude that the Tolman length is positive and significantly differs from zero in the range 200–250 K. Therefore, to accurately predict the supersaturation dependence of the nucleation rate of water, classical nucleation theory cannot be used without modification.
The values of \( B \), \( \mu \), \( b \), and \( T_c \) were taken from Ref. 35 and are listed in Table I. As Fig. 9 shows, the IAPWS expression differs little from the polynomial equation used by Wölk and Strey.\(^3\) IAPWS endorses the validity of Eq. (A1) between 273 K and the critical point; a comparison with the Hacker data in Fig. 9 shows that the validity range can be extended down to about 268 K. For lower temperatures we propose the fit

\[
\sigma(T) = \sigma_{\text{ref}}(T) - \sigma_a \tanh[(T - T_b)/T_b] + \sigma_b
\]

\((T < 267.5\, \text{K}),\)

where \( \sigma_a, \sigma_b, T_a, \) and \( T_b \) are shown in Table I. This fit agrees with the Hacker data to within 0.2\% and may be extrapolated down to 100 K. At 200 K the estimated uncertainty is 2.5\%.

Acknowledgment

We thank Dr. J. Hrubý for his encouragement and for his most valuable contribution to the estimates of the low-temperature thermophysical properties of water.

APPENDIX: THERMOPHYSICAL PROPERTIES OF WATER

Expressions for the density and equilibrium vapor pressure of water were taken from Wölk and Strey.\(^3\) The uncertainty of the density was estimated at 0.1\% at 260 K and 2\% at 200 K, that of the vapor pressure at 0.2\% at 260 K and 1\% at 200 K. For the molar mass we used the value \( M = 18.015\, 268 \, \text{g/mol}.\)\(^32\)

For the surface tension, we developed a new fit based on Hacker’s accurate measurements\(^33\) down to 251 K (shown in Fig. 9), a model of supercooled water,\(^34\) and the IAPWS equation\(^35,36\)

\[
\sigma_{\text{sd}}(T) = B \mu^a (1 + b \tau) \quad \text{with} \quad \tau = 1 - T/T_c.
\]

The values of \( B, \mu, b, \) and \( T_c \) are listed in Table I. As Fig. 9 shows, the IAPWS expression differs little from the polynomial equation used by Wölk and Strey.\(^3\) The proposed fit of Eq. (A2) reproduces the slope of Hacker’s low-temperature data, in contrast to the other fits.

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Value</th>
<th>Parameter</th>
<th>Value</th>
</tr>
</thead>
<tbody>
<tr>
<td>( B ) (N/m)</td>
<td>0.2358</td>
<td>( \sigma_a ) (N/m)</td>
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<tr>
<td>( T_c ) (K)</td>
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<td>( \sigma_b ) (N/m)</td>
<td>1.666 \times 10^{-3}</td>
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<td>( \mu )</td>
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<td>( T_a ) (K)</td>
<td>35.35</td>
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TABLE I. Parameters used in the surface tension fits, Eqs. (A1) and (A2).