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Conclusion: We have demonstrated the possibility of frequency hopping between the fundamental frequency and third harmonic of a Love wave device during the deposition and removal of a biological mass layer. The optimum interdigital transducer metallisation and guiding layer thickness for simultaneous operation at these frequencies has been investigated.

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Temperature retrieval algorithm for brain temperature monitoring using microwave brightness temperatures

G.M.J. Van Leeuwen, J.W. Hand, J.B. Van de Kamer and S. Mizushima

A solution to the inverse problem of retrieving temperature from a set of microwave brightness temperatures together with *a priori* information regarding weighting functions and heat transfer within the infant head is introduced. The method offers the basis for non-invasive temperature monitoring appropriate for hypothermal neural rescue therapy.

Introduction: Cooling of the brain after asphyxia at birth reduces the development of brain damage [1]. Clinical trials investigating the efficacy of brain cooling require that temperatures in the deep brain can be monitored. We are developing a microwave radiometry (MWR) system with five frequency bands for the non-invasive and prolonged monitoring of deep brain temperature [2]. Here we report an improved method for retrieving tissue temperatures from MWR measurements, and examine how uncertainties in measured brightness temperatures and in the data used in the analysis affect the retrieved temperatures.

Microwave radiometry: The measured brightness temperature in MWR is defined by the tissue's thermal radiation and is, according to the Rayleigh-Jeans law, proportional to the absolute temperature:

$$T_{B,i} \equiv \frac{P_i}{k\Delta f_i} = \iint_{afv} W_i(\mathbf{r})T(\mathbf{r})dV \quad (1)$$

where P_i is the thermal power received by the radiometer's antenna in a bandwidth Δf_i centred around frequency f_i , and k is Boltzmann's constant. The rightmost term involves integration over the antenna's field of view (afv) of the product of absolute temperature T and the radiometric weighting function W_i . The frequency dependence of W_i allows extraction of the temperature-depth profile in the tissue from a set of measurements made at different frequencies.

The radiometer antenna is a ceramic loaded open-ended rectangular waveguide. A thin water bolus between the antenna and the baby's head ensures predictable coupling. Each of five receivers, with central frequencies 1.2, 1.65, 2.3, 3.0, and 3.6 GHz and 0.4 GHz bandwidth, contains a reference noise source that is temperature controlled so as to 'balance' the thermal noise radiation from the antenna. When this condition is met, the brightness temperature of the tissues under observation is equal to that of the reference noise source [3]. For our system, which uses integration times of 4 or 5 s, we have calculated the total uncertainty in the measurement of the brightness temperatures to range between 60 mK for the 1.2 GHz-centred band and 65 mK for the 3.6 GHz-centred band.

Modelling: To calculate brightness temperatures, the weighting functions and temperature distribution must be determined. Electromagnetic and thermal computations were carried out using a 3D anatomically realistic model of an infant head. The radiometric weighting function was found using the reciprocity theorem by calculating the normalised power absorption rate distribution when the antenna was operating as a source rather than as a receiver:

$$W_i(\mathbf{r}) = \frac{(1/2)\sigma_i|\mathbf{E}_i(\mathbf{r})|^2}{\iint_{afv}(1/2)\sigma_i|\mathbf{E}_i(\mathbf{r})|^2dV} \quad (2)$$

where $\mathbf{E}_i$ is the electric field intensity induced by the antenna and σ_i is the tissue conductivity. The FDTD method with retarded time absorbing boundary conditions [4] was used to calculate the $\mathbf{E}$ -field distributions. Excitation of the antenna was modelled by prescribing $\mathbf{E}$ -field values for all voxels in the respective probe plane of the waveguide antenna. Temperature distributions within our infant head model were calculated using the heatsink approach [5] and were validated by comparison with those derived using a model that accounted for the effects of discrete vasculature [6]. The base set of thermal boundary conditions represented a cooling cap at 16°C and body core temperature maintained at 34°C.

Temperature retrieval: The inverse problem of finding the best estimate for the temperature distribution requires parameterisation of the 3D temperature distribution. In view of the long computation time necessary to calculate a temperature distribution, varying a parameter in the thermal model is not an option for real-time temperature retrieval. Instead, we use pre-calculated distributions $T_1, T_2, \dots$

$$T_{retrieved}(\mathbf{r}) = T_0 + p_1(\Delta T_1(\mathbf{r})) + p_2(\Delta T_2(\mathbf{r})) + \dots \quad (3)$$

where T_0 is the cooling cap temperature, $\Delta T_i = T_i(\mathbf{r}) - T_0$, and the $p_i(T)$ are polynomial functions, the coefficients of which are the parameters to be determined. The parameters can now be taken outside of the volume integral in eqn. 1, which allows the volume integration of the product of weighting function and temperature to be performed before measurements start. For example, two pre-calculated temperature distributions can be used with dimensionless parameters a_1 and a_2 which scale the distributions:

$$T_{retrieved}(\mathbf{r}|a_1, a_2) = T_0 + a_1\Delta T_1(\mathbf{r}) + a_2\Delta T_2(\mathbf{r}) \quad (4)$$

The numerical brightness temperatures can then be written as

$$T_{B,i}(a_1, a_2) = T_0 + a_1 \iint_{afv} \Delta T_1 W_i dV + a_2 \iint_{afv} \Delta T_2 W_i dV \quad (5)$$

Solution of the inverse problem is now reduced to solving an over-determined system of linear equations.

Fig. 1 Synthetic brightness temperatures for perfusion $40 \text{ ml } (100 \text{ g})^{-1} \text{ min}^{-1}$; differences with perfusion $30 \text{ ml } (100 \text{ g})^{-1} \text{ min}^{-1}$ and difference with best fit

—◆— synthetic brightness, bolus 5 mm (scale on left axis)
 + base, bolus 5 mm (scale on right axis)
 □ base2, bolus 7 mm (scale on right axis)
 * fit with uncertainty, $T_{B,\text{synt}} - T_{B,\text{model}}$ (scale on right axis)

Accuracy: Reconstruction of the temperature distribution from synthetic brightness temperatures calculated using the same models and parameters simulates the ideal situation in which exact knowledge of the spatial distributions of all the relevant physical properties used in the electromagnetic modelling and thermal modelling is available. Because no information is discarded in our new temperature retrieval process, it results in perfect retrieval for this ideal case. By using this method, we can investigate how the uncertainties in the brightness temperatures affect the precision of the reconstructed temperatures.

We have retrieved temperatures using two different brain perfusion values (30 and $40 \text{ ml } (100 \text{ g})^{-1} \text{ min}^{-1}$) to calculate temperature distributions. The central brain temperatures are equal, so when we use the parameterisation

$$T_{\text{retrieved}}(\mathbf{r}|a_1, a_2) = T_0 + a_1 \Delta T_1(\mathbf{r}) + a_2 (T_2(\mathbf{r}) - T_1(\mathbf{r})) \quad (6)$$

the standard error in a_1 , σ_{a_1} , alone determines the standard error in the central brain temperature. With synthetic brightness temperatures from T_1 we find $a_1 = 1$, $\sigma_{a_1} = 0.041$, resulting in $\sigma_{T,\text{brain}} = 0.75^\circ\text{C}$ for $\Delta T_1(\mathbf{r}) = 18.25^\circ\text{C}$ in the central brain.

Solving the inverse problem for a set of brightness temperatures calculated for the different body core temperature of 37°C instead of 34°C (using the same T_1 and T_2 as before) results in $a_1 = 1.164 \pm 0.041$. This corresponds exactly to the difference in calculated temperatures with respect to T_0 ($\Delta T = 21.25^\circ\text{C}$ and 18.25°C , respectively, for high and low core temperature). This is a reflection of the fact that the shapes of the temperature profiles are virtually independent of the temperature difference between cap and body core.

Inaccurate data causes systematic errors in the retrieved temperature distribution. We have evaluated the effect of realistic deviations in several parameters by solving the inverse problem for synthetic brightness temperatures. In practice, the parameter uncertainty with the biggest influence can be countered by using modelling results for different values of this parameter. We found that the thickness of the cooled water bolus is a major possible source of error. Therefore, the temperature retrieval might be based on sets of model computations for different bolus thicknesses. The effect of inaccurate values of other parameters in case of analysis using different bolus thicknesses was investigated. Assuming brain perfusion $30 \text{ ml } (100 \text{ g})^{-1} \text{ min}^{-1}$, a fit to synthetic brightness temperatures obtained for brain perfusion $40 \text{ ml } (100 \text{ g})^{-1} \text{ min}^{-1}$ resulted in an overestimate of the central brain temperature by 0.5°C . Fig. 1 shows the retrieved profile fits the synthetic data very well in this case. Plausible inaccuracies in dielectric properties ($\sim 10\%$) had a smaller effect, but a different anatomical segmentation with 2 mm more bone resulted in a 2°C underestimate.

Conclusion: A new algorithm for temperature retrieval from a set of microwave brightness temperatures is introduced. It allows the

time consuming calculations of temperature distributions and weighting functions to be performed off line, reducing the solution of the inverse problem to the solution of an overdetermined system of linear equations. Use of the algorithm, together with numerical modelling in an anatomically realistic model of the infant head, enables the temperature distribution in the brain to be obtained quickly from measurements obtained using a multi-frequency microwave radiometer. The algorithm is also useful in performing an error analysis of this measurement technique.

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Optimisation chaotic synchronisation of length-limited noisy Chua's circuit signal

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A new approach to synchronisation of Chua's circuit is presented. It effectively combines the interior penalty method of optimisation and chaotic synchronisation. Even under unfavourable, noisy conditions, the approach shows attractive lower variance results, compared with conventional chaotic synchronisation in realising the synchronisation of length-limited noisy chaotic signals.

Introduction: Chaotic signals commonly have stochastic noise phenomena present in the time domain, which cannot be easily synchronised. Conventional chaotic synchronisation, which was first introduced by Pecora and Carroll [1, 2], is an efficient means of resolving this problem but it is only available under specific conditions, while in unfavourable environments with additive white