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were very stable for both cases. This shows that the PNC output was not seriously corrupted by the laser phase noise as expected [4].

Fig. 4 Measured BERs

Fig. 4 shows the measured BERs after the 25 km-long SMF transmission against received optical power measured at the input of the 3 dB optical coupler. The measured BERs for both channel selection were almost the same. BER of less than 10^-9 was achieved when the received optical power was -10 dBm. From the above results, it was experimentally verified that the proposed channel selection scheme is useful for the uplink in ROF systems.

Conclusion: We have proposed the channel selection scheme of narrow-band SCM ROF signal with optical heterodyne detection, which was performed by tuning the mode interval of the dual-mode local light. It has been shown that the desired channel could be selected without the serious laser-phase-noise and fibre-dispersion effects even if the dual-mode local light was free-running. Moreover, the channel selection of two-channel SCM ROF signal after the 25 km-long SMF transmission has been experimentally verified.

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A network node is demonstrated with two-hop transmission and all-optical label swapping based on a Mach-Zehnder semiconductor optical amplifier interferometer and electrical-optical modulator of a two-level optically labelled signal using an orthogonal IM/FSK modulation format with an overall power penalty of less than 2 dB.

Introduction: All-optical label swapping is an attractive technique for implementing packet routing and forwarding functions independently of IP packet length and payload bit rate [1]. Combined intensity modulation/frequency-shift keying (IM/FSK) or intensity modulation/phase-shift keying (IM/DSK) optical labelling has been proposed as a competing scheme to sub-carrier multiplexed optical labelling due to its compact spectrum, simple label swapping and remarkable scalability to high bit rates [2][4]. Although we have earlier demonstrated successful single hop transmission of an IM/FSK labelled signal generated by a distributed feedback (DFB) laser with an integrated electroabsorption modulator (EAM) [3], the feasibility of all-optical label swapping and multi-hop transmission of this IM/FSK labelling scheme needs to be verified.

In this Letter, we present the latest experimental investigation of the complete functionality of a real network node with two-hop transmission and all-optical label swapping of an optically IM/FSK labelled signal. Simultaneous FSK label erasure and 2R regeneration are successfully achieved in a monolithic integrated Mach-Zehnder semiconductor optical amplifier (MZ-SOA). We also demonstrate for the first time FSK label insertion based on an EAM through all-optical conversion of the 10 Gbit/s intensity modulated payload to a new wavelength. Propagation over two transmission spans (50 and 44 km SMF) separated by a network node including label removal, 2R regeneration, and label insertion functionalities, is shown to result in less than 2 dB power penalty for both the 10 Gbit/s IM payload and the 312 Mbit/s DSK labelled modulator.

Architecture of all-optical packet switched network based on orthogonal IM/FSK labelling: At the ingress edge router the incoming IP packets are assigned two-level optical labels, i.e. the wavelength of the signal carrier (carrier label) and the FSK label, orthogonally modulated to the IM payload. The packet switched network architecture requires these two-level optical labels to be swapped during the routing process in order to build up an appropriate optical path along the transmission fibre network, as shown in Fig. I.

The core nodes perform routing and forwarding operations based on the information retrieved from the optical label. They also perform label swapping with wavelength conversion to ensure that packets reach their destination. To perform label swapping, a fraction of the incoming signal is tapped for opto-electronic label processing. The remaining part of the signal is input to an MZ-SOA for label removal and 2R regeneration. Replacing the label is easy because the FSK label information is lost during the wavelength conversion in the MZ-SOA. Therefore only the payload information will be copied onto the output wavelength of the MZ-SOA, which will then be used as the pump signal to the EAM. After setting the new 2 label by accordingly setting the

References
wavelength of the tunable laser and inserting the new FSK label, the FSK modulated signal is injected into the EAM as the probe signal for frequency-modulation maintaining wavelength conversion. After these cascaded processes, both the label and the FSK label are swapped and the packet is ready for the next hop transmission.

Experimental setup and results: The experimental setup is shown in Fig. 2. The optical FSK modulation can be achieved simply by directly modulating the electrical current of a DFB laser (1549.2 nm). However, the drive current variation always results in a simultaneous intensity modulation of the emitted light, which will obviously cause a detrimental effect on the IM payload. To remove the intensity variation at the output of the laser, the inverse electrical data is injected into the integrated EA modulator with appropriate time delay and modulation voltage. In this way, a constant amplitude optical FSK signal at 312 Mbit/s (PRBS 2^31-1) is generated. The payload information of 10 Gbit/s (PRBS 2^31-1) is added by a following Mach-Zehnder modulator, thus producing an optically IM/FSK labelled signal. It should be noted that a limited IM extinction ratio is necessary for the FSK label detection, but on the other hand this low extinction ratio will deteriorate the payload detection. Therefore in our experiment a compromise value of 4.3 dB is selected for the extinction ratio of the IM payload.

The first hop consists of 50 km singlemode fibre (SMF) with matching length of dispersion compensating fibre (DCF). The dispersion of the SMF and the DCF is 16.9 ps/nm/km and ±100 ps/nm/km, respectively. In our simulation results and experimental investigation identically reveal that a pre-compensation scheme has better performance than a post-compensation scheme. Hence pre-compensated fibre spans are chosen for both fibre links. After this first stage transmission, the optically labelled signal is input to the MZ-SOA (Alcatel 19011CM) for the label erasure and 2R regeneration. A tunable external cavity laser at 1555.8 nm is used as CW input for the MZ-SOA. Very good label erasure and 2R regeneration can be achieved by the MZ-SOA. Owing to its nonlinear transfer function, the extinction ratio of the converted signal is greatly improved to 12.9 dB, which leads to a 2 dB enhancement for the receiver sensitivity. The regenerated payload is then fed to the EAM as the pump signal for the label insertion process, where the extinction ratio of the label-renewed signal will be adapted to the required value.

The advantage of using the EAM for label insertion is the negligible frequency chirp induced by EAM-based wavelength conversion, which is extremely desirable in our orthogonal IM/FSK labelling scheme [5]. The EAMs used in our experiment were kindly provided by GIIGA, an Intel company. The initial FSK signal is split into two parts with one of them acting as the second label source for the label insertion module. The nonlinear transfer function of the MZ-SOA will be beneficial to the output extinction ratio at the cost of some amplitude jitter and eye diagram distortion. This can be seen in the eye diagram recorded at the output of the MZ-SOA shown in Fig. 2. Another advantage of the label swapping based on cascaded MZ-SOA and EAM is that this amplitude jitter can be compensated for by the nonlinear absorption and saturable absorption of the EAM. As evidence a very clear eye diagram with negligible distortion was obtained when carrying out cascaded conversion of a pure IM signal. It should be noted that the noise imposed onto the EAM output eye diagram (see Fig. 2) is due to the non-optimal FSK intensity. As mentioned earlier, a limited extinction ratio is obligatory in the orthogonal labelling scheme. This relatively low extinction ratio can be easily accomplished by adjusting the reverse bias of the EAM. The output signal of the label swapper has an extinction ratio of 4.9 dB. The second hop includes 44 km SMF and 6 km DCF. At the receiver, the frequency discrimination for FSK demodulation is achieved by two optical filter stages providing more than 15 dB suppression ratio between the two FSK tones. Fig. 3 shows the BER curves in the back-to-back case, after the first hop, after the label swapper and after the second hop. The inset shows the pattern for both the payload and the label as detected after two-hop transmission including label swapping. Clearly some payload information is superimposed onto the label after the FSK demodulation, however the eye is still open and allows error-free detection. The cascaded transmission and label swapping result in 1.9 dB power penalty for the payload and 1.8 dB penalty for the label.

Conclusion: We have experimentally demonstrated the full functionality of a network node performing all-optical label swapping of a two-level optically labelled signal using orthogonal IM/FSK modulation format, two-hop transmission and 2R regeneration. The power penalty for the cascaded transmission and label swapping was shown to be below 2 dB.

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References
Mitigation of optical crosstalk penalty in photonic cross-connects using forward error correction

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The use of forward error correction (FEC) in all-optical networks for reducing the impact of dynamic crosstalk in photonic cross-connects based on three-dimensional micro-electromechanical systems (3D-MEMS) is described. Error-free operation is achieved for coherent crosstalk levels up to -16 dB, which corresponds to a 13.5 dB coherent input signal dynamic range, using a RS(255,239) Reed-Solomon error correcting code with a coding gain of 6 dB in a 288 x 288 non-blocking 3D-MEMS switch.

Introduction: Dense wavelength division-multiplexed photonic networks with all-optical (OOO) nodes for metro and long-haul applications have recently been demonstrated for network efficiency and significant cost savings by the removal of optical-electrical-optical transponders at each switching node [1]. With their potential for works with all-optical (OOO) nodes for metro and long-haul applications, significant cost savings by the removal of optical-electrical-optical transponders at each switching node 

Results: The experimental setup is shown in Fig. 1. The two 9.95328 Gbit/s complementary outputs from a bit error rate tester (BERT) with pattern lengths of 2^22-1 were synchronously fed into the RS(255,239) FEC encoder. A 1553.3 nm optical signal was then modulated with the FEC-encoded 10.66 Gbit/s data stream using a Mach-Zehnder modulator (MOD). A 3 dB coupler split the output signal and one arm, with 0.5 dBm of power, was directly connected to the main optical signal path in the PXC (mirror S_m) to So(m) with a loss of 5.5 dB. The other arm of the splitter was fed into an erbium-doped optical amplifier (EDFA), which was followed by a variable optical attenuator (VOA) and a polarization controller (PC) before it was input to the adjacent port (mirror S_a) of the main signal path. An optically amplified receiver was used at the output of the PXCs before the 10.66 Gbit/s signal was FECD-decoded to 9.95328 Gbit/s for bit error rate (BER) measurements.

Fig. 2 shows the BER results with and without FEC encoding. In these measurements, the channel isolation was held statically at the worst-case value of -35 dB experienced during switching while the crosstalk channel input power was set to various levels (no power, 7.5, 10, and 12.5 dBm). The signal input power was 0.5 dBm resulting in -5 dBm output power and a crosstalk X_m/S_m of 0, -22.5, -20, and -17.5 dB, respectively. The PC was used to align the polarizations of the two signals for maximum errors. Without crosstalk, a BER of 10^-12 was obtained for an average received power of -30.5 dBm without FEC and -36.5 dBm with FEC. As the interfering signal level was increased to 12.5 dBm to cause a coherent crosstalk level of -17.5 dB, the power penalty incurred with no FEC is more than 10 dB while FEC enables the same receiver sensitivity of -30.5 dBm that was achieved without crosstalk and without FEC.