Transactions Briefs

A Generalized Class of Dynamic Translinear Circuits

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Abstract—This brief proposes a generalization of the class of “dynamic translinear,” or “exponential state-space,” circuits. As an illustration of the proposed general class of dynamic translinear circuits, the brief describes the design of a second-order translinear filter that does not fit into the existing classification of exponential state-space filters. The externally linear behavior of the designed filter is demonstrated by means of simulations.

Index Terms—Companding filters, translinear circuits.

I. INTRODUCTION

In the area of analog continuous-time filters, the design of dynamic translinear (DTL) and log-domain circuits has become a definite (academic) trend [1]–[17]. Translinear (TL) filters were originally introduced by Adams in 1979 [1] and independently by Seevinck in 1990 [2]. The log-domain filters presented by Adams and Seevinck were first-order. The interest in TL filters really started to increase from 1993, when Frey published a synthesis method enabling the design of higher order log-domain filters. Furthermore, Frey recognized that log-domain filters only constitute a subset of a more general class of “exponential state-space” (ESS) filters [18], [19]. In particular, Frey described the subsets of tanh and sinh filters.

The aim of this brief is to show that the “general” class of ESS or DTL filters proposed in [18], [19] can be generalized even further. As an illustration, the brief describes the design of a second-order TL filter that does not fit into the framework suggested in [18], [19].

Section II first provides a short review of the static translinear (STL) and dynamic translinear principles. Next, Section III treats the generalization of the class of DTL and ESS circuits. The generalization is addressed both in terms of currents and in terms of voltages, as both the current-mode and the voltage-mode approach are used in the literature. A circuit design example is described in Section IV. Finally, Section V presents the conclusions.

II. TRANSLINEAR PRINCIPLES

Translinear circuits can be divided into two major groups: STL and DTL circuits. Static TL circuits realize static transfer functions, both linear and nonlinear; DTL circuits realize frequency-dependent (transfer) functions, i.e., differential equations (DEs). The underlying principles of STL and DTL circuits are reviewed in this section.

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Fig. 1. A four-transistor translinear loop.

Fig. 2. Principle of dynamic translinear circuits.

A. Static Translinear Principle

Translinear circuits are based on the exponential relation between voltage and current, characteristic for the bipolar transistor and the MOS transistor in the weak inversion region. The STL principle applies to loops of semiconductor junctions. A TL loop is characterized by an even number of junctions [20], [21]. The number of devices with a clockwise orientation equals the number of counterclockwise-oriented devices. An example of a four-transistor TL loop is shown in Fig. 1. It is assumed that the transistors are somehow biased at the collector currents $I_1$ through $I_4$. When all devices operate at the same temperature, this yields the familiar representation of TL loops in terms of products of currents

$$I_1 I_3 = I_2 I_4.$$  \hspace{1cm} (1)

This generic TL loop equation is the basis for a wide variety of static electronic functions, which are theoretically temperature and process independent.

B. Dynamic Translinear Principle

The DTL principle can be explained with reference to the subcircuit shown in Fig. 2. Using the current-mode approach, this circuit is characterized by the relation between the collector current $I_C$ and the capacitance current $I_{cap}$ flowing through the capacitance $C$. Note that the dc voltage source $V_{const}$ does not affect $I_{cap}$. The expression for $I_{cap}$ is easily found to be given by [21], [22]

$$I_{cap} = C U_T \frac{I_C}{I_C}.$$  \hspace{1cm} (2)

where $U_T$ is the thermal voltage and the dot represents differentiation with respect to time.

Equation (2) shows that $I_{cap}$ is a nonlinear function of $I_C$ and its time derivative $I_C$. A better understanding of (2) is obtained by slightly rewriting it as

$$C U_T \dot{I}_C = I_{cap} I_C.$$  \hspace{1cm} (3)

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Equation (3) directly states the DTL principle: A time derivative of a current can be mapped onto a product of currents. Now, the product of currents on the right-hand side of (3) can be realized very elegantly by means of the STL principle. In other words, the implementation of (part of) a DE becomes equivalent to the implementation of a product of currents.

III. GENERALIZATION

The specific characteristics of each subset within the class of ESS filters (e.g., $\log$-domain, $\tanh$ and sinh filters) can be described either in terms of voltages [19] or in terms of currents [10], [23].

Using the voltage-mode approach, the capacitance voltages $V_{C_i}$ are chosen to represent the memory of a filter circuit, where $i \in \{1, \ldots, n\}$, and $n$ denotes the order of the filter. In DTL circuits, the capacitance voltages are nonlinearly related to the state variables $x_i$. For the class of ESS filters, the relations between the variables $x_i$ and $V_{C_i}$ are given by [19]

$$x_i = f_i(V_{C_i})$$

where the functions $f_i$ are transcendental and have to be strictly monotonic. Different subclasses of ESS filters result from different choices for the functions $f_i$. The functions proposed in literature are $\exp$, $\tanh$, and sinh [19]. The transcendental nature of these functions reveals the internally nonlinear behavior of ESS filters.

Alternatively, using the current-mode approach, the currents $I_{C_i}$ are chosen to represent the state of a TL filter [10], [23]. The currents $I_{C_i}$ are linearly related to the state variables $x_i$. The internally nonlinear behavior of DTL circuits is now revealed by the equations for the capacitance currents $I_{C_i}$. The current-mode equivalent of (4) is given by

$$I_{C_i} = g_i(I_{C_i}^*, I_{x_i}^*)$$

Different choices for the nonlinear functions $g_i$ result either in $\log$-domain, $\tanh$ or sinh filters. For example, note that (2) is a special case of (5). Obviously, there exists a very tight correspondence between the functions $f_i$ and $g_i$.

In (5), each capacitance current $I_{C_i}$ is a function of only one state current $I_{x_i}$ and its first-order derivative. This restriction to a dependence on one state current only is not fundamental. Equation (5) can be generalized by allowing each capacitance current $I_{C_i}$ to be a function of all state variables and their first-order derivatives, which are represented by the vectors $I_{x}$ and $I_{x^*}$, respectively. This yields

$$I_{C_i} = g_i(I_{x}, I_{x^*})$$

Equation (6) constitutes a class of DTL circuits more general than the class of ESS filters proposed in [18], [19]. The voltage-mode equivalent of (6) is given by

$$x_i = f_i(V_{C_i})$$

where $V_{C_i}$ is the vector of capacitance voltages $V_{C_i}$.

As an example, consider the definitions of two capacitance currents $I_{C_1}$ and $I_{C_2}$, given by

$$I_{C_1} = CU_T \left( \frac{I_x}{I_x^*} + \frac{I_{x^*}}{I_{x^*}} \right)$$

$$I_{C_2} = CU_T \left( \frac{I_x}{I_x^*} - \frac{I_{x^*}}{I_{x^*}} \right)$$

where the currents $I_x$ and $I_{x^*}$ are (strictly positive) linear state variables. It is easily seen that (8) and (9) do not fit into the framework suggested by (5), as both $I_{C_1}$ and $I_{C_2}$ are functions of both state currents $I_x$ and $I_{out}$.

The voltage-mode equivalents of (8) and (9) are given by

$$V_{C_1} = U_T \ln \frac{I_x}{I_x^*}$$

$$V_{C_2} = U_T \ln \frac{I_x}{I_{out}}$$

where $I_x$ is the saturation current of the bipolar transistor. Note that (10) and (11) do not fit into the general ESS framework of (4).

A possible implementation of (8) and (9) is depicted in Fig. 3(b) and (a), respectively. It is assumed that the transistors are somehow properly biased at the currents $I_x$ and $I_{out}$. These subcircuits can be used as parts of a complete TL filter implementation.

IV. DESIGN EXAMPLE

As an illustration of the proposed generalization, we now describe the design of a second-order TL filter, based on (8) and (9). Starting with a suitable DE, the current-mode synthesis path of DTL circuits comprises the following design steps: definition of capacitance currents, translinear decomposition and hardware implementation [23].

A possible state-space description of a second-order Butterworth low-pass filter is given by

$$2CU_T I_{out} = I_x(I_x - 2I_{out})$$

$$CU_T I_x = I_x(I_x - 2I_{out})$$

where $I_x$ is a dc current, $I_{in}$ is the input current and $I_{out}$ is the output current. The (linear) state variables are $I_x$ and $I_{out}$. The filter cutoff frequency $\omega_c$ equals $I_x/(\sqrt{2CU_T})$.

A. Definition of Capacitance Currents

The first step toward the TL implementation of (12a) and (12b) is the definition of two capacitance currents. These capacitance currents are used to implement the derivatives $I_{out}$ and $I_x$. We use (8) and (9) to obtain a circuit that is not a member of the class of ESS filters. These definitions are valid if $I_x$ and $I_{out}$ are class-A biased, i.e., if they are strictly positive. Assume that $I_{in}$ contains a dc component $I_{in,dc}$. Then, as a result, $I_{out}$ and $I_x$ contain dc components equal to $I_{in,dc}$ and $2I_{in,dc}$, respectively. Consequently, for a sufficiently “small” ac signal swing $\Delta I_{in}$, if $I_{in}(i.e.,|\Delta I_{in}|<I_{in,dc})$, $I_{out}$ and $I_x$ are strictly positive and can be implemented by collector currents (see Fig. 3).

Solving (8) and (9) for $I_{out}$ and $I_x$ and substitution in (12a) and (12b) yields two current-mode polynomials

$$I_{out}(I_{C_1} - I_{C_2}) = I_x(I_x - 2I_{out})$$

$$I_x(I_{C_1} + I_{C_2}) = 2I_x(I_{in} - I_{out})$$

B. Translinear Decomposition

To implement (13a) and (13b) using STL circuit techniques, suitable TL decompositions have to be derived, resulting in TL loops [21], [23]. In principle, many TL decompositions exist for (13a) and (13b). The
solution described below is only one of many possibilities and not necessarily the best or most simple one.

First, we derive a TL decomposition for (13a). Addition of a redundant term \(2I_o I_{out}\) to both sides of (13a) directly yields a valid TL loop equation

\[
I_{out}(2I_o + I_{C1} - I_{C2}) = I_o I_e. \tag{14a}
\]

Note that all linear factors in (14a) are strictly positive. Hence, they can be mapped directly onto collector currents; compare Fig. 1 and (1).

A second TL decomposition, for (13b), can be derived by adding a term \(2I_o I_e\) to both sides of (13b). This yields

\[
I_e(2I_o + I_{C1} + I_{C2}) = 2I_o(I_{in} - I_{out} + I_e). \tag{14b}
\]

All factors in (14b) are again strictly positive making (14b) a valid TL loop equation.

C. Hardware Implementation

Next, (14a) and (14b) have to be mapped on TL loops and a proper biasing scheme has to be designed. This step requires quite a bit of heuristics and the implementation depicted in Fig. 4 is again only one of many possible implementations. The only aim here is to demonstrate the existence of a more general class of DTL circuits.

Equation (8) for \(I_{C1}\) is implemented by transistors \(Q_1, Q_7,\) and \(C_1\). The collector currents of these two transistors are the state variables, i.e., \(I_{C1}, q_6 = I_{out}\) and \(I_{C1}, q_7 = I_e\). Note that the loop \(Q_6 - Q_7 - C_1\) is identical to the subcircuit shown in Fig. 3(b).

The second capacitance current is implemented in a different way. Combining (9) and (14a), an alternative expression for \(I_{C2}\) is obtained

\[
I_{C2} = C_U \frac{I_{C1} - I_{C2}}{2I_o + I_{C1} - I_{C2}}. \tag{15}
\]

Equation (15) is implemented by the loop \(Q_1 - Q_2 - C_2\), where the collector current of \(Q_2\) equals \(I_{C2}, q_2 = 2I_o + I_{C1} - I_{C2}\). Note that the dc bias current of \(Q_1, I_{C1}, q_1 = I_o\), does not affect \(I_{C2}\); compare \(V_{const}\) shown in Fig. 2.

Translinear loop (14a) is implemented by transistors \(Q_6 - Q_{10} - Q_8 - Q_2 - Q_1\), where \(I_{C8}, q_8 = I_o, I_{C9}, q_9 = I_e,\) and \(I_{C10}, q_{10} = I_e\). The second TL loop, (14b), is not implemented directly. Instead, combining (14a) and (14b) results in an alternative second TL loop equation, given by

\[
I_{out}(2I_o + I_{C1} - I_{C2})(2I_o + I_{C1} + I_{C2}) = 2I_o^2 (I_{in} - I_{out} + I_e). \tag{16}
\]

This third-order loop is implemented by transistors \(Q_1 - Q_2 - Q_3 - Q_4 - Q_5 - Q_6\), where \(I_{C3}, q_3 = 2I_o + I_{C1} + I_{C2}, I_{C4}, q_4 = I_o,\) and \(I_{C5}, q_5 = I_{in} - I_{out} + I_e\). The factor 2 at the right-hand side of (16) is realized by the scale factor of \(Q_3\). All unnumbered p-n-p transistors (and also \(Q_8\) and \(Q_9\)) constitute simple level shifts and nullor implementations, required for biasing purposes. The p-n-p transistors implement a current mirror, which is also used for biasing the TL loops. Note that the subtraction of \(I_{C2}, q_2\) and \(I_{C2}, q_{2b}\) equals \(2I_{C2}\), and the addition of \(I_{C2}, q_2\) and \(I_{C2}, q_{2b}\), implemented by the p-n-p mirror, equals \(2(I_o + I_{C1})\).

The output current \(I_{out}\) of the filter is the collector current of \(Q_6\). A copy of \(I_{out}\) can be obtained by connecting an additional p-n-p transistor in parallel with \(Q_6\).

D. Simulation Results

Correct operation of the circuit was verified by means of simulations, using realistic transistor models. In the simulations, the dc current \(I_{dc}\) equals 0.5 \(\mu A\). The supply voltages are \(+2.1-1.3\) V. Fig. 5 shows a transient simulation at 40 kHz. The amplitude of the input signal is 90% of \(I_{in, dc}\), which equals 1 \(\mu A\). With \(C = C_1 = C_2 = 100\) pF, \(U_T = 26\) mV and \(I_o = 1\) \(\mu A, \omega_s\) equals 43.3 kHz.

Fig. 5 clearly shows that the relation between \(I_{in}\) and \(I_{out}\) is linear. Hence, the circuit is externally linear [24]. However, internally, the filter is strongly nonlinear, which is evidenced by the wave forms of
and circuits which employ a very small number of circuits designed using the compensation–poles of the traditional Design Using CFOA-Poles: New Resonators, Internally nonlinear behavior is a general characteristic of companding filters [24].

V. CONCLUSION

This brief has described a class of dynamic translinear circuits, or exponential state-space circuits, that is more general than the existing classification found in literature. The proposed generalization has been articulated both in terms of voltages and in terms of currents. As an example, a second-order translinear filter has been designed, that fits articulated both in terms of voltages and in terms of currents. As an example, a second-order translinear filter has been designed, that fits only into the generalized class of dynamic translinear circuits.

REFERENCES


Active-\textit{R} Design Using CFOA-Poles: New Resonators, Filters, and Oscillators

Abhdes K. Singh and Raj Senani

Abstract—Recently, the active-\textit{R} circuits utilizing the current feedback op-amps (CFOAs)-pole have been shown to be superior alternatives to the active-\textit{R} circuits designed using the compensation–poles of the traditional voltage-mode op-amps. The object of this brief, is to present some new CFOA-pole-based active-\textit{R} circuits which employ a very small number of active and passive components, and yet, offer features which have not been attained simultaneously from any of the previously known active-\textit{R} circuits using CFOA-poles such as, noninteracting controls of parameters, and the availability of the intended properties, in spite of the presence and consideration of all the parasitics (even other than those forming CFOA-pole). The workability of the proposed circuits has been confirmed by PSPICE simulations and hardware implementations based on AD844 type CFOAs.

Index Terms—Active filters, active-\textit{R} circuits, current feedback op-amps, gyrators, resonators, sinusoidal oscillators.

I. INTRODUCTION

The transimpedance op-amps, popularly known as current feedback op-amps (CFOAs), are receiving growing attention as alternative building blocks for analog circuit design, because they offer several advantages over the traditional voltage–mode op-amps (VOAs). These advantages include, wider bandwidth (relatively independent of the closed loop gain), very high slew rates, and ease of realizing...