Leaky Wave Enhanced Feed Arrays for the Improvement of the Edge of Coverage Gain in Multibeam Reflector Antennas

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Abstract—The performance of multibeam focal plane arrays feeding a single aperture is usually reduced due to conflicting requirements on the feed elements. Dense packing is usually required to minimize the beam separation, while typically large feed apertures are needed to provide the high feed directivity to reduce spillover losses from the reflector. In this paper the use of dielectric super-layers to shape the radiation pattern of each feed is demonstrated. The shaping is obtained by exciting, according to design, a pair of TE/TM leaky waves. The spillover from the reflector is reduced without physically increasing the dimensions of each single element aperture. A prototype of a feed array composed of 19 waveguides arranged in a hexagonal lattice was designed, manufactured and tested. The measured embedded patterns provided an increase of the edge of coverage gain, with respect to the free space case, of at least 0.6 dB in an operating bandwidth (BW) of \( \approx 12\% \). Moreover when reactive loading of adjacent feeds is adopted the increase in the edge of coverage with respect to the free space case was demonstrated to be larger than 1.6 dB over a 3\% BW.

Index Terms—Leaky wave antennas, leaky waves, reflector antenna feeds, reflector antennas.

I. INTRODUCTION

PRESENT and next generation satellite telecommunication systems often require multiple beam capability. In particular Ka band multibeam down links are being used to achieve efficient coverage of the earth and continents. The three fundamental ways to achieve high coverage gain are overlapping feed arrays with sophisticated feed networks, interleaved beams with multiple apertures (typically 4 reflector), and a single aperture with a single feed per beam designs [1]. This last approach is clearly much less expensive to implement, however it suffers from reduced performance.

A. General Problem With the Single Feed Per Beam Design

Let us consider a generic array aimed at generating multiple independent beams, separated by a given angle \( \Delta \theta \). The array is assumed to be in the focal plane of a reflector system as in Fig. 1. The basic parameters characterizing such a multibeam system are: the beam separation \( \Delta \theta \), the reflector diameter, \( D \), and the focal distance, \( F \). These three parameters always define a sampling rule for the focal plane array depending on the desired beam properties and cross over between the beams. As an example, a first order dimensioning could be based on the assumption that the reflector is uniformly illuminated and that, at the cross over between two adjacent beams, the roll-off (field drop with respect to beam peak) is \(-3\) dB. In this case (see Appendix) the basic sampling rule is

\[
d \approx (F/D) \lambda_0 \tag{1}
\]

where \( \lambda_0 \) is the wavelength at the central operating frequency, \( f_0 \). All the power that is launched by the feed but that is not intercepted by the reflector is effectively lost for the system (spillover). In order to enhance the spillover efficiency one would like to use large, more directive feeds. But (1) suggests that the dimensions of the apertures are limited by the period. As a rule of thumb, the radiation patterns (\( |E|^2 \)) from standard feeds, e.g., horns, can approximately be modelled as \( \cos^q(\theta) \), where \( q \) depends on the feed type and aperture size.
formulas to evaluate the $q$ parameter for standard horns are given in [12]. The spillover efficiency associated to center fed reflectors can be approximated as $\eta_{sp} = 1 - \cos^{q+1}(\theta_{sub})$. As shown in Fig. 1 $F/D$ also defines the subtended angle $\theta_{sub}$. As a relevant example, an aperture of $\lambda_0 \cdot \lambda_0$ roughly corresponds to $q = 5$, which for $\theta_{sub} = 30^\circ$ corresponds to losses in spillover of 2.4 dB.

Equivalent conclusions would hold for any reflector illumination and beam overlap configurations: spillover is the limiting factor for a full field of view. For this basic reason, as also discussed in [1], the single feed per beam approach is usually not adopted for telecommunication satellite systems. This paper proposes an improvement that could make this single feed per beam option viable and would significantly reduce the costs of multibeam systems.

B. Leaky Wave Enhancements of Antenna Performances

G. V. Trentini [2] was the first to propose the use of a partially reflecting screen to increase the directivity of a single aperture. A point source would generate an ensemble of waves that impinge on a screen that is partially reflective and partially transmitting. The reflected rays propagate laterally and then are redirected towards a partially reflecting screen, so that they generate a unique wave that mainly radiates in the broadside direction. Since then this technique has been proposed in many different variations that involve periodic super-layers realized in dielectric or metal materials [3]–[6]. In [7] the fact that the enhancement in gain is due to the excitation of leaky waves has been clarified. Most recently, [8] studied the compromise between bandwidth and directivity for printed antennas and arrays in the presence of periodic super-layers.

In [9], leaky waves were also used to enhance the radiation performance of small antennas. The emphasis was, contrary to other works, not on the increase of the directivity of the source, but on the shaping of the pattern. In fact the target was to optimize the gain of the overall system composed by a feed + reflector and not the source alone. In [9] both taper and spillover efficiencies were improved choosing centrally fed reflectors as an example. In a $p$-feed demonstrator, an operational bandwidth of 10% was achieved for the antenna system.

In this paper, the design of multibeam focal plane arrays using an overlapped feed concept realized via dielectric super-layers is discussed. The results of [10] are used as starting point. In fact in [10], after a discussion on the impact of mutual coupling on overlapped feeds configurations, a specific radiator design was presented.

C. Structure of the Paper

The structure of the paper is as follows. First a short introduction on the use of focal plane multibeam systems is provided with the parameters characterizing the properties of such systems and in particular the edge of coverage (EoC) gain. A reuse scheme is considered to maximize the isolation of neighboring beams. The performance of a standard array configuration operating in free space (without superstructures to create overlapping between feeds) is used as reference. Then a first system design, indicated as resistively loaded design, is described. The proposed structure was manufactured and measured showing a moderate gain enhancement, with respect to the reference, over 12% bandwidth (BW). For moderate operational BW, higher EoC gain enhancement with respect to reference can be obtained by reactively loading the neighboring waveguides. A second prototype demonstrator was manufactured to explicitly demonstrate this aspect. The relation between the design methodology described in this paper and the Stein’s Limit, [18], [19] is discussed just before the conclusions.

II. System Parameters and Formulation of the Problem

In this section the requirements are first given and explained, then the performances realized with a standard reference array are described in order to establish a benchmark for a comparison with leaky wave enhanced feeds that will follow in the next sections.

A. System Requirements

The specific telecom scenario that is considered will be that of satellite based down-link in Ka band. The area to be covered by independent beams is arranged in an hexagonal lattice with beam separation $\Delta \theta \approx 1^\circ$. Correspondingly, an hexagonal array is placed in the focal plane of a reflector system. Moreover, a reuse scheme (x4) will be used in order to achieve a maximal isolation between the neighboring channels (beams). The implementation of the interleaved beams and of the single aperture corresponding focal plane array is based on the scheme
described in Fig. 2. As will be discussed in the next sections the scheme can be implemented simply by a x4 frequency reuse or by a mixed frequency and polarization reuse. It can be anticipated that the reflector system will be an offset fed Gregorian in order to minimize the blockage of the direct radiation by a large feed array. The array elements are assumed circularly polarized in order to maintain the highest applicability. Finally, the bandwidth is required to be at least 6% which encompasses many applications. While in standard multibeam systems the F/D of the reflector is often a parameter that can be used for system optimization, in leaky wave enhanced feed systems, the F/D is mostly dependent on the target bandwidth. Thus, if the BW is a requirement, the F/D is already fixed in a certain range. For instance, as was clarified in [9] and [10], a BW of 6% for the impedance or the mutual coupling approximately corresponds to leaky waves pointing towards 15° from broadside. Consequently, the reflector half angle $\theta_{\text{sbh}}$, which needs to be optimized can be anticipated to be in range from 25° to 40°, corresponding to an F/D in the range 1.2-0.8. Such a moderate F/D ratio limits the scanning performance of the antenna system. However the limited scanning should not be seen as a definitive limit. A smaller bandwidth could have allowed the selection of a super-layer that supported leaky waves pointing to smaller angles from broadside so that overall the definition of systems with $F/D$ significantly larger would have been possible. This study aims at providing general design guidelines, which can then be tuned to the more specific needs of an engineer.

B. A Reference Array

A standard waveguide array, whose geometry is described in Fig. 3, is investigated. An hexagonal grid array is chosen with periodicity, $d$, set to 1.2 $\lambda_0$. Such an array is suitable to feed reflector systems characterized by relatively small $F/D$ ratios ($F/D \approx 1$), comparable with the ones anticipated for the leaky wave enhanced feeds.

The array consists of 19 circular waveguide horns that open in an finite ground plane of dimensions (12$\lambda_0$ x 12$\lambda_0$). The reference system has the z axis normal to the ground plane. The circular apertures are obtained by flaring the feeding waveguides of diameter 0,7$\lambda_0$ to a diameter of 1,1$\lambda_0$, over a taper of length $t = \lambda_0$. With this arrangement the apertures cover almost the entire central part of the ground plane. The reflection coefficients, $S_{ii}$ parameters, of each of the waveguides are lower than $-23$ dB’s and the mutual coupling coefficients, $S_{ij}$ are lower than $-30$ dBs over the entire operational BW.

C. Edge of Coverage Gain and Other Performance Parameters

The use a dual reflector system is proposed. The scanning impairment due to the offset is reduced using the Mizucuchi’s condition [13] which conserves the optical symmetry of a center fed reflector system. Also the sub-reflector magnification can be used to match the feed subtended angle (and hence spillover) to the main reflector F/D ratio. The geometry of the system is shown in Fig. 4 and the nominal dimensions are reported in Table I (the reflector system is assumed to be in X band, representing a 2.8 times scaled version of the Ka one). As a starting point the design of the system was still based on the equivalent diameter D and focal distance F using the equivalent paraboloid concept, [12].

To accurately evaluate the performances of a reflector system fed by the reference array in Fig. 3, the far fields of the reflector need to be calculated. The fields radiated by the reference array, calculated using Microwave Studio CST [15], have been used as inputs to calculate the secondary fields via the Physical Optics code GRASP, [14]. The key merit parameter for these multibeam systems is the edge of coverage, EoC, gain, which in the hexagonal lattice is defined at the cross over between three adjacent beams: $G_{\text{EoC}} = G(\Delta \theta, \theta, 3)$. Fig. 5 shows the EoC gain calculated from the radiation patterns predicted by the reference array in Section II.B, for a reflector that provides $\Delta \theta \approx 1^\circ$, which, given the array spacing of 1,2$\lambda_0$, corresponds to $F = 67\lambda_0$. The EoC gain is shown as a function of the normalized frequency and for different F/D, since the F/D ratio was the main design parameter in order to find the maximum EoC gain. The optimum F/D ratio was found to be around 0.85. Another optimization parameter was the feed axial position, corresponding to finding the optimum phase center. In the optimum case the roll-off at the edge of coverage and at the central frequency (10 GHz) is $-5.46$ dB. The relevant 10 GHz patterns are shown in Fig. 6.

Table II shows the most important parameters characterizing the secondary beams from each of the feeds in the reference multibeam array, for $F/D = 0.85$. Note that the roll-off is also evaluated at the EoC. Adopting a reuse scheme of 4x, assumed to be realized via frequency switching, the isolation is the maximum overlap between beams located at two beam-separations, Fig. 6. The obtained isolation is around 15 dB which can be marginal in some applications. A reuse scheme of at least 7x will, however, provide a beam isolation of well below 20 dB.
TABLE II
PARAMETERS CHARACTERIZING THE SECONDARY BEAMS FROM EACH FEED IN THE REFERENCE MULTIFEED ARRAY (F/D = 0.85)

<table>
<thead>
<tr>
<th>Freq (GHz)</th>
<th>G_{max}(dB)</th>
<th>G_{EoC}(dB)</th>
<th>Roll-off (dB)</th>
<th>Spill</th>
<th>Isolation x4</th>
<th>X-Pol</th>
<th>θ_{3dB} (deg)</th>
</tr>
</thead>
<tbody>
<tr>
<td>9.4</td>
<td>43.8</td>
<td>39</td>
<td>4.8</td>
<td>-2.8</td>
<td>14.7</td>
<td>38.3</td>
<td>0.91</td>
</tr>
<tr>
<td>9.6</td>
<td>44.2</td>
<td>39.2</td>
<td>5</td>
<td>-2.6</td>
<td>14.5</td>
<td>37.4</td>
<td>0.89</td>
</tr>
<tr>
<td>9.8</td>
<td>44.5</td>
<td>39.3</td>
<td>5.2</td>
<td>-2.5</td>
<td>14.3</td>
<td>36.6</td>
<td>0.87</td>
</tr>
<tr>
<td>10</td>
<td>44.7</td>
<td>39.3</td>
<td>5.5</td>
<td>-2.4</td>
<td>14.4</td>
<td>35.2</td>
<td>0.86</td>
</tr>
<tr>
<td>10.2</td>
<td>44.9</td>
<td>39.3</td>
<td>5.7</td>
<td>-2.3</td>
<td>14.5</td>
<td>34.3</td>
<td>0.84</td>
</tr>
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<td>10.4</td>
<td>45.1</td>
<td>39.2</td>
<td>5.9</td>
<td>-2.1</td>
<td>14.8</td>
<td>33.7</td>
<td>0.82</td>
</tr>
<tr>
<td>10.6</td>
<td>45.4</td>
<td>39.3</td>
<td>6.1</td>
<td>-2.2</td>
<td>15.1</td>
<td>34</td>
<td>0.81</td>
</tr>
</tbody>
</table>

III. PATTERN SYNTHESIS BASED ON LEAKY WAVE ENHANCEMENT

In [10] a super-layer configuration, characterized by \( h_1 = 0.5\lambda_0, h = 0.25\lambda_d \) and dielectric constant \( \varepsilon_r = 4.5 \) was used for the design of a waveguide array. In that paper it was demonstrated that the mutual coupling between neighboring array elements in an hexagonal lattice configuration was dominated by the first couple of TE/TM leaky waves that were supported by the structure. When the inter-element spacing was \( 1.2\lambda_0 \), the \( S_{11} \) parameters, with 1 indicating the central element and \( j \) indicating any of the neighboring ones was in the order of \(-20\) dB. When the array configuration was based on square waveguides loaded with irises, as shown in Fig. 7, the radiation patterns would turn out to be rotationally symmetric, and also minimal perturbed by the unwanted second TM mode.

The predicted patterns, at the central operating frequency, \( f_0 \) corresponding to \( \lambda_0 \), in four planes are reported in Fig. 8 for completeness. Both embedded and isolated patterns are shown to highlight the effects of mutual coupling on the patterns. The embedded patterns (dashed lines) are representative of a scenario in which all the waveguides surrounding the central one are terminated in matched loads: in the rest of the paper this configuration will be referred to as resistively loaded design.

The isolated patterns would instead be representative of a configuration in which the adjacent waveguides are not present and the equivalent inter-element period is \( 2.4\lambda_0 \). In fact in that case the mutual couplings would be so low that they can be completely ignored. This configuration can be realized by introducing reactive loads in the adjacent waveguides, which synthesize equivalent short circuits. In the rest of the paper this second configuration will be referred to as reactively loaded design.

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IV. RESISTIVELY LOADED DESIGN

A prototype array was manufactured to implement the resistively loaded design at X band. An added advantage of the small
waveguides, with respect to the larger waveguide of the reference array, is that they are easier to manufacture and connect to the common ground plane.

The central operating frequency of the prototype was chosen as $f_0 = 10$ GHz. The elements to be fed or measured are excited, in linear polarization, by a WR-90 feeding waveguides ($w_g = 22.86$ mm and $h_g = 10.16$ mm), after a smooth transition ($t = 17.3$ mm, $t_a = 10$ mm), see Fig. 9. These feeds can be mounted with two possible orientations so that also the mutual coupling between orthogonally polarized waveguides can be measured. The remaining waveguides are closed in resistive matched loads. The dielectric material has been selected to be the TMM4 from Rogers (dielectric constant of 4.5). The thickness of the slab was $h = 3.5$ mm. The remaining dimensions of the prototype are: $w = 26$ mm, $d = 36$ mm, $h_1 = 15$ mm, $w_i = 3.4$ mm, $S = 16.85$ mm, $w_e = 0.35$ mm. Both the transverse dimensions of the substrate are 360 mm. A photo of the resistively loaded prototype is shown in Fig. 10. Note that the length $t_g$ is not important if the WR90 waveguides are closed in resistive matched loads. However this will be an important parameter in the reactively loaded prototype that will be discussed in the next section.

### A. S-Parameters Measurements

The reflection coefficient of the central waveguide has been measured when all the others are loaded. The results are presented in Fig. 11. The leaky wave enhanced prototype’s reflection coefficient is below $-15$ dB’s, over a very large BW, which indicates that in this case the matching does not limit the system performances.

The mutual coupling parameters between the central waveguide and 6 neighboring ones (indicated with indices 1–7 in Fig. 7) have been measured and are shown in Fig. 12. Only the $S_{12}$ and $S_{14}$ couplings are significant. However they are still below $-18$ dB’s, until 10.6 GHz.

The S parameters pertinent to orthogonally polarized feeds were measured and were always lower than $-30$ dB’s over the entire investigated BW.
B. Measured Patterns

The patterns from the prototype were also measured. The far field E and H plane measured embedded patterns of the central waveguide at different frequencies are shown in Fig. 13–16. The $\phi = 30^\circ$ and $\phi = 60^\circ$ planes have also been measured. They turned out to be an average of the E and H plane patterns as expected. The measurements closely resemble the predictions, Fig. 8. The only noticeable differences are associated to amplitude ripples of less than 1 dB in the H-plane main beam. Cross polarization level are below 25 dB with respect to co-pol in all $\phi$ cuts. This result was to be expected due to recent findings on the polarization properties of the Green’s function of a dielectric super-layer [17].

C. System Performances

The patterns were then used to calculate (using GRASP) the edge of coverage gain of a system composed by the feed array and a reflector. A parametric study of the $G_{rc}$, assuming different $F/D$ (0.85, 0.87, 0.95) and fixed focal distance $F = 2.06$ m, equivalent to that in Section II.C, is plotted in Fig. 17 as a function of the frequency. For all three $F/D$ the gain presents a frequency dependence. Comparing it with the gain obtained
TABLE III
PARAMETERS CHARACTERIZING THE SECONDARY BEAMS FROM EACH FEED IN THE RESISTIVELY LOADED CASE

<table>
<thead>
<tr>
<th>Freq (GHz)</th>
<th>$G_{\text{max}}$ (dB)</th>
<th>$G_{\text{eoc}}$ (dB)</th>
<th>roll-off (dB)</th>
<th>Spill</th>
<th>Isolation</th>
<th>X-Pol</th>
<th>$\theta_{3\text{dB}}$</th>
</tr>
</thead>
<tbody>
<tr>
<td>9.4</td>
<td>44.7</td>
<td>39.8</td>
<td>4.9</td>
<td>-2</td>
<td>13.6</td>
<td>42.9</td>
<td>0.91</td>
</tr>
<tr>
<td>9.6</td>
<td>45.2</td>
<td>40</td>
<td>5.2</td>
<td>-1.8</td>
<td>12.9</td>
<td>43.8</td>
<td>0.88</td>
</tr>
<tr>
<td>9.8</td>
<td>45.7</td>
<td>40.2</td>
<td>5.4</td>
<td>-1.5</td>
<td>12.8</td>
<td>43</td>
<td>0.86</td>
</tr>
<tr>
<td>10</td>
<td>46</td>
<td>40.4</td>
<td>5.6</td>
<td>-1.3</td>
<td>13</td>
<td>41.4</td>
<td>0.85</td>
</tr>
<tr>
<td>10.2</td>
<td>46.3</td>
<td>40.4</td>
<td>5.8</td>
<td>-1.2</td>
<td>13.4</td>
<td>40.4</td>
<td>0.83</td>
</tr>
<tr>
<td>10.4</td>
<td>46.3</td>
<td>40.3</td>
<td>6</td>
<td>-1.3</td>
<td>14.3</td>
<td>37.5</td>
<td>0.82</td>
</tr>
<tr>
<td>10.6</td>
<td>46.1</td>
<td>39.9</td>
<td>6.3</td>
<td>-1.7</td>
<td>15.7</td>
<td>34.3</td>
<td>0.81</td>
</tr>
</tbody>
</table>

Fig. 16. Phase of the H-plane patterns as a function of the frequency.

Fig. 17. Edge of coverage gain calculated from the leaky wave feeds, in the resistively loaded case. The Curves are plotted as a function of the frequency and parameterized for different $F/D$ ratios.

Fig. 18. Secondary pattern after the reflector in the E-plane calculated at frequency $f = 10$ GHz using as feed array patterns those from the measured leaky wave feed array, $F/D = 0.85$.

have then been subtracted from the edge of coverage gains obtained using the leaky wave enhanced feed (resistively loaded case). The maximum edge of coverage gains achieved for both the reference array and the enhanced feed with $F/D = 0.85$ are compared in Fig. 19. The secondary patterns, for $F/D = 0.85$ are shown in Fig. 18, at the central frequency (10 GHz), including the isolation to an adjacent pattern in a 4x frequency reuse scheme. Here the patterns associated to the two feed arrays are very similar but the leaky wave enhanced feeds provide simply higher gain values due to the fact that the power saved from spillover is radiated. It is apparent that the increase of the gain at the edge of coverage with respect to the free space case is essentially the same as that observed at broadside. Thus the leaky wave enhanced feed is more efficient in general and not only at the edge of coverage.

To summarize the results in Fig. 19 show that, even in the presence of resistively loaded neighboring waveguides, over a band width of about 12%, a minimum increase of the EoC gain of 0.6 dB can be observed. This increase becomes 0.8 dB if the band is restricted to 6%.

V. REACTIVELY LOADED DESIGN

The system performance enhancements observed in the resistively loaded array prototype were encouraging, but in order to obtain a higher increase of the EoC gain, a reactively loaded array prototype was manufactured. In this case it was assumed using the reference array it is apparent that there is a significant improvement that can be as high as 1.2 dB for $F/D = 0.85$.

In Table III the most significant system parameters for this resistively loaded case are summarized, assuming $F/D = 0.85$.

When evaluating the system performances one should take into account that part of the available power launched by the feeds is coupled in the 6 neighboring waveguides, as anticipated in [10]. The pertinent actual values of the losses as a function of the frequency have been calculated using the measured mutual couplings. They are in the order of 0.25 dBs. The losses
that 4x re-use scheme was realized using two frequency bands (27.5–27.75 GHz and 28.25–28.5 GHz) and two linear polarizations to obtain a 4x frequency/polarization reuse scheme. The implementation of interleaved beams and of single aperture corresponding focal plane array is based on the same scheme described in Fig. 2. However in this case the correspondence between channel frequency and polarization was the following: $I \rightarrow \alpha f_1^I; II \rightarrow \alpha f_2^I; III \rightarrow \alpha f_1^I; IV \rightarrow \alpha f_2^I$.

The reactively loaded prototype is very similar to the resistively loaded prototype. It is scaled to operate in the X band. The implementation of a linear polarization is simply obtained by short circuiting one of the pairs of irises in each element. The implementation of frequency selectivity is obtained loading the waveguides with two different filters which operate in the lower and the higher reflection bands respectively. The amplitudes of the $S_{II}$ parameters can be kept below $-25$ dB in the pass band and essentially $0$ dB in the rejection band. The phase of the reflection at the filter cross section can be made almost constant, varying less than $15^\circ$ in the rejection band. For budget reasons it was not possible to manufacture the filters. However, thanks to the smooth behavior as a function of the frequency of the phase of the reflection coefficient, the reactive load can be represented by a piece of waveguide loaded at a certain distance ($t_g = 15$ mm) by a real short circuit. The distance of the reflection plane from the aperture is tuned to achieve an effective short circuit at the aperture. The effective geometry manufactured to simulate the waveguides terminated in rejecting filters is the one shown in Fig. 9. The simulated phase of the $S_{AA}$ parameter as seen from plane A is also reported in Fig. 20. It varies less than $40^\circ$ degrees over the rejection BW.

The iris has been fine tuned in order to obtain the proper matching. In this case the iris parameters are: $S = 16.7$ mm, $w_i = 3$ mm and the slot edges are increased from an angle relative to the axis of $45^\circ$ to an angle of $47.3^\circ$. The prototype for this reactively loaded design is shown in Fig. 21.

The measured $S_{11}$ of the central element of the array in the presence of the reactive loading of the neighboring waveguides is presented in Fig. 22.

The radiation patterns have also been measured and they are shown in Fig. 23–26. The patterns obtained with these reactive
loading are essentially the same as the isolated ones in Fig. 8. Some amplitude oscillations (of amplitude lower than 1 dB) can be observed in the main beam, however these differences turn out to be not significant in terms of the performance evaluation that follow in the next section.

A. System Performances

These feed patterns were then used to find the optimum EoC gain of a system composed by the feed array and the same Gregorian reflector system as for the other feeds. The optimum F/D was 0.87 and the $G_{\text{EoC}}$ is plotted in Fig. 27 as a function of the frequency.

The gain shows stronger frequency dependence than in the other cases, due to the path length for the signal reflected in the filters, simulated in the adjacent feeds. In this case the obtained gain is significantly improved both with respect to the free space case and the resistively loaded design. In Table IV the most significant system parameters for the reactively loaded case are summarized, considering $F/D = 0.87$.

The maximum increase in edge of coverage gain in the leaky wave enhanced feed configuration is as high as 1.7 dB. Over a 6% bandwidth the EoC gain is increased by 1.3 dB. Fig. 28 shows the secondary patterns with EoC limits indicated. Comparing the secondary beams of this reactively loaded design (Fig. 28) with the ones from the resistively loaded ones (Fig. 18) one can observe larger secondary beams due to a bigger aperture taper. This leads to smaller roll-off which is the second cause of EoC enhancement, after the reduced spillover. In this case the loss due to coupling to the neighboring feeds is negligible since the amplitude of the relevant $S_{12}$ is lower than $-35$ dB. Also the adjacent beam with same frequency and polarization is shown to highlight the beam isolation, which is in the range 12 to 18 dB. Larger improvements in terms of edge of coverage gain could have been obtained, but at the expense of bandwidth.

VI. RELATION TO STEIN’S THEOREM

The ruling theorem that is usually mentioned when dealing with multibeam antenna systems was formulated by Stein in [18]. Simply stated, it says that whenever an antenna presents multiple beams, the mutual coupling between the different beams limits the efficiency of the system. The mutual coupling between the beams can be quantified by calculating the $S_{ij}$ between beam $i$ and $j$ either in free space or, equivalently, at feed level. A high mutual coupling implies high losses because part of the power radiated by feed $j$ is lost in the load of feed $i$. If the feeds are located too close one to the other the mutual coupling grows and so do the losses. For the specific case
of multifeed imaging [19] presented an in-depth study of the maximum realizable secondary aperture efficiencies. There it has been shown that packing the feed elements together too much diminishes the broadside gain of the primary pattern of each of the feeds. However in [19] all feeds considered were characterized by patterns of the type \( \cos^2(\theta) \). The efficiency of circular reflectors with F/D’s in the order of unity was shown to be limited to about 55%.

In the present paper, the finding of the Johansson paper are essentially those represented by the reference configuration. Thus, in this paper, the comparison with the reference case could be considered as a comparison with the findings of [19]. The resistively loaded imaging configuration of Section IV shows a higher efficiency by about 15%. This finding explicitly shows that the results of [19] only constitute a upper boundary if the shape of the radiated beam obeys a \( \cos^2(\theta) \) type of rule. There is no contradiction of Stein’s limit since there are no greater broad side gains of the primary patterns. The rectangular primary beam shapes, that can be achieved via the leaky wave super-layers, lead to the higher primary beam efficiency, which in turn leads to a more efficient use of the reflector. This finding can be useful in those scenarios in which the attention is not necessarily to the edge of coverage but on the maximum amount of power radiated in a beam.

On the contrary the finding of the reactively loaded scenario, Section V do not imply any further improvement of the system efficiency with respect to the findings in [19]. In fact the overlap between different feeds is not really occurring. The neighboring feeds in the reactively loaded configurations are operated orthogonally, either on a different frequency or on a different polarization.
better performance, with respect to the resistively loaded design, is due to higher directivity from each feed which focuses the radiated beams in the central part of the reflector. Consequently the secondary beams are broader lowering the roll-off. In this reactively loaded design, a relaxation of the BW requirements would lead to better scanning performances for systems using larger equivalent F/D ratios. This further steps probably would require higher level trade offs in the system but the single reflector option for multibeam satellite telecommunication scenarios seems a viable option.

### APPENDIX

**FOCAL PLANE ARRAY FOR A FULLY SAMPLED FIELD OF VIEW**

Three basic design parameters, with their approximate relationships, seem to be defining the performances of the imaging system: the beam separation \( \Delta \theta \), the reflector diameter, \( D \), and the focal distance, \( F \) (see Fig. 1).

If the system needs to make use of the entire available field of view, the half power beam width will be designed to be equal to the beam separations: \( \theta_{3 \text{dB}} \approx \Delta \theta \). Since \( \theta_{3 \text{dB}} \) can be approximated as a function of the reflector diameter as \( \theta_{3 \text{dB}} \approx \lambda_0 / D \) it follows that the beam separation is linked to the antenna diameter by: \( \Delta \theta \approx \lambda_0 / D \)

\( F \), relates the beam separation to the separation, \( d \), in the focal plane between the different array elements: \( \Delta \theta / d \approx F / d \), is a simplified formula provided in [12] for small values of \( \Delta \theta \). From the use of these simple relationships between the previous three parameters follows the key imaging array law that estimates the separation between the different feeds in order to achieve a fully sampled sky:

\[
d = F \cdot \Delta \theta = D \cdot (F/D) \lambda_0 / D \approx (F/D) \lambda_0. \quad (2)
\]

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### REFERENCES


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