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2D electron cyclotron emission imaging at ASDEX Upgrade (invited)\textsuperscript{a)}

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The newly installed electron cyclotron emission imaging diagnostic on ASDEX Upgrade provides measurements of the 2D electron temperature dynamics with high spatial and temporal resolution. An overview of the technical and experimental properties of the system is presented. These properties are illustrated by the measurements of the edge localized mode and the reversed shear Alfvén eigenmode, showing both the advantage of having a two-dimensional (2D) measurement, as well as some of the limitations of electron cyclotron emission measurements. Furthermore, the application of singular value decomposition as a powerful tool for analyzing and filtering 2D data is presented. © 2010 American Institute of Physics. [doi:10.1063/1.3483214]

I. INTRODUCTION

Many processes and instabilities in tokamak plasmas exhibit two-dimensional (2D) dynamics, thereby making them difficult to diagnose by one-dimensional (1D) diagnostics. The strength of 2D electron cyclotron emission imaging (ECEI) was first demonstrated at the TEXTOR tokamak.\textsuperscript{7} It provided valuable physics insight in the research of, among others, the sawtooth instability\textsuperscript{2,3} and tearing modes.\textsuperscript{4,5} An overview of the development of ECEI systems since the first TEXTOR diagnostic can be found in the literature.\textsuperscript{6}

Recently an ECEI system has been installed at ASDEX Upgrade in order to investigate the 2D electron temperature dynamics of other reactor relevant instabilities, including edge localized modes (ELMs) and neoclassical tearing modes, not easily accessible at TEXTOR. This system images a plasma area of approximately 12 by 40 cm\textsuperscript{2} and thus a 2D measurement, as well as some of the limitations of electron cyclotron emission (ECE) measurements (Sec. V). Finally, a singular value decomposition (SVD) is used to overcome the limitations set by thermal noise, which allowed the visualization of Alfvén waves (Sec. VI).

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II. THE PRINCIPLE OF ECEI

A standard 1D ECE radiometer measures the electron temperature at different radial locations along a single line of sight, making use of the magnetic field dependence of the electron cyclotron frequency $\omega_{ce}=eB/m_e$ due to the variation of the magnetic field with major radius $B=B_R R_0/R$ as is seen in Fig. 1(a). In the thermal equilibrium, the measured intensity at a given resonant frequency (and corresponding radius) is given by the Rayleigh–Jeans limit of Planck’s law $I_{BB}(\omega) = \omega^2 k_B T_e (8\pi^3 c^3)$, so the plasma behaves as a black-body and the intensity is proportional to the electron temperature. Therefore, a frequency resolved measurement of the electron cyclotron emission intensity constitutes a radially resolved measurement of the electron temperature.

The same principle is employed in a 2D ECEI diagnostic, except that multiple lines of sight are simultaneously quasioptically imaged onto a linear array of diode detectors [see Fig. 1(b)]. Each of the lines of sight is treated as a 1D ECE radiometer. This gives a direct 2D measurement of the electron temperature; radially resolved due to the frequency resolved measurement of the ECE intensity along each line of sight, vertically resolved due to the multiple lines of sight corresponding to the detectors on the array.

III. ASDEX UPGRADE ECEI

In Fig. 2, a schematic representation of the various components of the ASDEX Upgrade ECEI system is given. ECEI uses the same 36 cm diameter quartz vacuum window as the 1D ECE radiometer (“manhole” in sector 9), and also shares part of the (newly designed) optics with this diagnostic. The two systems are separated by a beam splitter (a thin dielectric foil) that has an approximately 50/50% transmission/reflection over the full range of frequencies, with the ECEI optical path in reflection. The ECEI optics actually consist of
two branches, the front side optics that images the plasma radiation on the detector array, and the LO side optics (separated from the first one by a further beamsplitter) that images the local oscillator BWO beam on the array. All ECEI components (except the computers) are positioned in the ASDEX Upgrade torus hall. The various components of the system are described in the following paragraphs.

The ASDEX Upgrade ECEI system utilizes the detector array and intermediate frequency (IF) electronics of the previous TEXTOR ECEI system. The detector array employs 16 dual dipole antennas with an array of 16 miniature elliptical substrate lenses (minilenses) in front of them, yielding highly Gaussian, parallel field patterns. In Fig. 3, a schematic layout of the ECEI electronics of a single antenna is shown. The signal is downconverted two times. The first downconversion occurs at the array by mixing the plasma signal with the BWO signal (tunable between 90 and 140 GHz). This is a single sideband downconversion; the lower sideband is rejected by using quasioptical high pass filters (dichroic plates) in front of the array. The downconverted broadband signal of each of the 16 antennas is transmitted to the 16 IF electronic modules by microwave cables.

In the IF modules, the signal is divided into eight portions, which are subsequently mixed with eight local oscillator signals (voltage controlled oscillators at \( f_{LO} = 2.4, 3.2, 4.0, 4.8, 5.6, 6.4, 7.2, \) and 8.0 GHz) in the second downconversion step. The frequency difference between these local oscillators determines the radial interchannel spacing of ECEI and is hence 800 MHz. This typically corresponds to 1.5 cm in the plasma, depending upon the gradient of \( B \). The full radial coverage of ECEI is hence approximately 12 cm. The resulting signals are band pass filtered (double sideband), with an intermediate frequency bandwidth \( B_{IF} \) of 700 MHz. This determines the frequency bandwidth of the ECE radiation selected by each channel and, along with broadening effects, the radial resolution. After detection, the signals are low pass filtered (with a tenth order filter) with adjustable video bandwidth \( B_v = 25–400 \) kHz, determining the time resolution of ECEI. The sampling frequency is normally set to (at least) twice \( B_v \). Finally, the signals are converted to a digital signal by 12 bit digitizers, capable of storing 2 Msamples per channel at a maximum sampling rate of 2 Msamples/s. More technical details concerning the array and electronics can be found in the literature.

The front side optics, shown in Fig. 4, consist of a set of high density polyethylene (HDPE) lenses, part of which is shared with a 60 channel 1D ECE radiometer. The line of sight of the 1D system is designed to coincide with the optical axis of ECEI, simultaneously providing in the same poloidal plasma cross section a measurement of the full 1D electron temperature profile as well as the detailed 2D coverage of a selected area of about 12 by 40 cm (8 by 16 channels). This also makes cross calibration with the absolutely calibrated 1D system easier.

ECEI lines of sight have adjustable (although not independent) foci. This is made possible by translating one of the lenses to shift the position of the focal plane to the desired radius (Fig. 4). This makes it possible to always operate ECEI in focus (unlike 1D ECE, which has a fixed focus). Also, the confocal parameter (about 40 cm) is larger than the radial coverage, ensuring all ECEI channels are in focus.

The optics have been designed such that the location

![Fig. 1. Comparison between (a) a standard 1D ECE radiometer and (b) a 2D ECEI system. In an ECEI system, multiple lines of sight are imaged onto a 1D array of detectors.](image)

![Fig. 2. (Color online) Diagram showing all major components of ECEI.](image)

![Fig. 3. Schematic representation of the electronics of a single detector for a typical ECEI system.](image)

![Fig. 4. (Color online) Optics of the ASDEX Upgrade ECEI system. Part of the optics are shared with the 60 channel 1D ECE radiometer. The position of the focal plane can be shifted by translating one of the HDPE lenses.](image)
along the beam path where all 16 beams from the detectors exactly overlap each other in space (the Fourier plane of the optics) lies close to the window aperture. In this way, all beams use as much of the aperture as possible, thereby optimizing the perpendicular spatial resolution. The window aperture is hence the limiting factor determining the (diffraction limited) Gaussian beam waist \( w_0 = 2d \lambda / \pi D \), where \( d \) is the distance from the window aperture (1.8 m at the center of the plasma) and \( D = 0.36 \) m is the window aperture diameter (see Fig. 4). This gives a smallest possible spot size of about \( w_0 = 15 \) mm in the plasma, which is also achieved by the optics. The antenna pattern of each of the detectors (including their associated minilens) can be approximated by a Gaussian beam with a waist of 7 mm in the object plane (at the detector), and the array of 16 detectors has a length of 20 cm. The optics images this object plane (array) onto the focal plane in the plasma. Note that the spot size and vertical coverage in the plasma cannot be independently imaged. Consequently, the ideal spot size of 15 mm in the plasma (about a factor of 2 larger than the spot size at the array), also fixes the vertical coverage in the plasma, which is about 40 cm (twice the size of the array). Therefore, with the current array, a smaller vertical coverage is not possible (the beams would not fit through the window aperture), and a larger coverage would lead to a proportionally larger spot size.

The local oscillator for the first downconversion step is a backward wave oscillator (BWO). This is a tunable microwave source that typically delivers a 50 mW microwave beam at an adjustable frequency between 90 and 140 GHz (F-band) with a frequency stability of 0.02%. The BWO optics image the radiation quasi-axially onto the detector array as an elongated Gaussian beam, in order to illuminate all 16 detectors. The BWO is enclosed in a 1 cm thick iron casing for stray magnetic field shielding.

The available cutoff frequencies of the dichroic plates for the sideband rejection are currently 99.1, 105.0, 111.7, 115.6, and 120.2 GHz. The filter has to be chosen such that the lower sideband plasma light is blocked, while permitting both the upper sideband and BWO frequencies to pass. Therefore, in practice, the filter must have a cutoff frequency just below the BWO frequency, thereby limiting the number of useful BWO frequency settings to the available dichroic plates.

The operation during 140 GHz electron cyclotron resonance heating (ECRH) is possible. In order to protect the array against stray ECRH power, three quasi-axial notch filters with a (combined) 60 dB rejection at 140 GHz (3 dB rejection at about 127 GHz) are used. No notch filters are currently available for other ECRH frequencies at the ASDEX Upgrade. Operation with a dichroic plate cutoff frequency above the ECRH frequency is always possible. In other cases, the system will be shielded with a shutter.

The ECEI diagnostic has been designed to be fully remotely controlled. The position of the focusing lens, the frequency and power of the BWO and the selection of the dichroic plates (using a stepper motor controlled slide with five filters and a shutter) are all remotely controlled. Also, the system can be switched on and off remotely. No entry to the Torus Hall is required at any stage during operation, greatly enhancing the flexibility of the system.

### IV. OPERATIONAL RANGE AND LIMITS

The range of radii to which ECEI can be tuned to during experiment depends on the toroidal magnetic field and on the frequency range of the diagnostic. Figure 5 provides a graphical representation of this operational range. The horizontal shaded area represents the accessible plasma region (the second harmonic ECE radiation from the HFS is blocked by the third harmonic resonance at the low field side). The tilted shaded area represents the range ECEI can be tuned to as a function of \( B_0 \), limited by the frequency range of the BWO. In reality, not all BWO frequency settings can be used, due to the limited number of available dichroic plates to reject the lower sideband. The dark shaded area gives the limitation set by the currently available dichroic plates. Therefore, currently the plasma center is accessible between \( B_0 = 1.8 \) and 2.25 T and the low field side (LFS) edge between 2.35 and 2.9 T.

Another limitation is set by cutoff. For a second harmonic X-mode ECE diagnostic, the cutoff occurs at the right hand cutoff frequency \( \omega_c \approx \frac{1}{2} \left[ \omega_p + (\omega_p^2 + 4 \omega_p^2)^{1/2} \right] \), where \( \omega_p = \sqrt{n_e e^2 / (\epsilon_0 m_e)} \) is the density dependent plasma frequency. Figure 6 gives the density above which the cutoff occurs as a function of radius and toroidal magnetic field. Note that measurements at high density generally require a high toroidal magnetic field. When in cutoff, the second harmonic X-mode radiation cannot reach the observer, so signal levels drop toward zero, although some second harmonic O-mode radiation is normally still visible due to the finite sensitivity to O-mode of any real diagnostic. Another related effect to be aware of is the bending of the (mainly off-axis) lines of sight due to refraction. Close to cutoff, the index of refraction of the plasma becomes noticeably smaller than...
unity that refracts the lines of sight away from the plasma center. This effect rapidly becomes smaller when the plasma is further from cutoff.

Two other properties of ECE measurements to be shortly addressed are the optical thickness and broadening effects. The optical thickness for the second harmonic X-mode radiation is (for typical ASDEX Upgrade parameters $B_0 = 2.5$ T and $R_{\text{resonance}} = 2$ m) approximately given by $\tau_X = 3.3 \times T_{\text{[keV]}} \times n_e^{[10^{19}]}$ (see Ref. 10 for the exact formula). If the optical thickness is too low (comparable to or below unity), the plasma is partially transparent and the ECE measurements (the radiation temperature $T_R$) can no longer be regarded as a direct electron temperature measurement (also density plays a role). Neglecting wall reflections, the radiation temperature is given by $T_R = T_e [1 - \exp(-\tau)]$, where $\tau$ is a function of both temperature and density. For the normal ASDEX Upgrade H-mode plasmas, these only play a role at the foot of the pedestal (see Sec. V).

The frequency broadening of the ECE radiation due to relativistic effects\cite{10,11} $\Delta \omega_{\text{rel}} = n_0 \omega_c (v_{th}/c)^2$ (where $v_{th} = \sqrt{2k_B T_e/m_e}$), and Doppler broadening\cite{10,12} $\Delta \omega_d = 2 v_{th}/w_0$ (which for perpendicular observation can be regarded as an effect of the finite transit time of the emitting electrons through the Gaussian spot of size $w_0$), result in an emitting layer with significant radial extent (for ECE at 1 keV about 3 cm full width at half maximum). However, in the optically thick case, most of the radiation of the broadened emission layer is reabsorbed before it reaches the observer, and only the last layer (typically narrower than 1 cm), closest to the observer, contributes to the ECE signal, and determines the radial spatial resolution. In the optically thin plasma edge (see Sec. V) the full emission layer is observed.

**V. 2D DYNAMICS: EDGE LOCALIZED MODES**

One of the main motivations for installing ECEI at the ASDEX Upgrade was the study of ELMs, which is one of the most important and still not fully understood instabilities in fusion devices. The necessity for a 2D diagnostic is illustrated in Fig. 7, where the ECEI measurements of the LFS plasma edge during different phases of an ELM crash are presented. The data have been filtered (using singular value decomposition, see Sec. VI) to reduce the thermal noise. The observed pronounced 2D dynamics would not have been accessible with a conventional 1D ECE radiometer. Figures 7(b)–7(d) are taken during the early stages of the crash [time indicated in Fig. 7(a)] where a clear deformation of the temperature profile due to (precursor) mode activity is visible, showing a rather complicated and partly incoherent poloidal mode structure. In Fig. 7, $t_0$ (2.747 165 s) is defined as the time of the first visible deviation from the (prechase) smooth temperature profile. Figures 7(e) and 7(f) show images during a later phase of the crash [time indicated in Fig. 7(a)], where poloidally localized structures (thought to be related to the ELM filaments observed by many other diagnostics) are seen to rotate poloidally (upward in the figure). To enhance these structures in the images, not the absolute (radiation) temperature, but $T_R - T_{av}$ is shown, where $T_{av}$ is the average temperature (calculated separately for each ECEI channel) after the ELM crash [shaded area in Fig. 7(a)]. These filaments have a radiation temperature of about 200 eV.

Whether one can interpret the observed filaments as electron temperature fluctuations depends upon the optical thickness of these structures. Figure 8(c) shows the optical thickness for typical electron density and temperature profiles [shown in Figs. 8(a) and 8(b)] at different phases during the ELM cycle. For both the pre-ELM and post-ELM cases, the optical thickness drops below unity at roughly the separatrix position, with rapidly rising values inside the separatrix. In the case where the electron temperature profile has been modified to include a filament [inspired by the radiation temperatures seen in Figs. 7(e) and 7(f)] but the electron density profile is left unchanged, it turns out that the optical thickness of this filament is roughly unity. The assumption of simultaneously increased density could drastically increase this number. Consequently, the optical thickness is marginal (normally values above 2 to 3 are considered fully optically
degree of redundancy can be taken advantage of by using SVD as a powerful tool for analyzing and filtering the 2D data. SVD is a well known mathematical technique to decompose two-dimensional matrices into pairs of eigenvectors. The mathematical details can be found in the literature, but the general idea becomes clear by looking at the application of SVD for filtering ECEI data. In principle, ECEI data are three-dimensional: there are two spatial dimensions, and a time dimension. However, for the SVD decomposition, we will regard ECEI data as having one time dimension (of length \( m \), typically \( m=1000 \)), and only one spatial dimension (of length \( n=128 \)), treating the 16 by 8 two-dimensional space as a one-dimensional array of length 128. Therefore, the ECEI data are represented by a two-dimensional \( m \)-by-\( n \) matrix \( X \). The SVD decomposition of the data can now be written as

\[
X = USV^T,
\]

(2)

where \( U \) is an \( m \)-by-\( n \) matrix whose (length \( m \)) columns \( u_k \) represent time eigenvectors (sometimes called “chronos”). \( V^T \) is an \( n \)-by-\( n \) matrix whose (length \( n \)) rows \( v_k^T \) represent spatial eigenvectors (“topos”). \( S \) is an \( n \)-by-\( n \) matrix whose only nonzero elements are on the diagonal, so

\[
S = \text{diag}(s_1, \ldots, s_k),
\]

where \( s_k \), the so called singular values, are the eigenvalues belonging to the topos-chronos pairs of eigenvectors. By convention, the vectors are ordered from large to small \( s_k \). Therefore, in the case of ECEI, the SVD results in 128 pairs of eigenvectors \( (u_k \text{ and } v_k^T) \) with corresponding decreasing eigenvalues \( s_k \). The filtered ECEI data \( X' \) would then be represented by

\[
X' = \sum_{k=1}^{l} u_k s_k v_k^T, \tag{3}
\]

where \( l \) is the number of (most significant) eigenvector pairs retained in the summation. The information contained in the eigenvector pairs with \( k > l \) is hence lost. Mathematically, \( X' \) (the truncated SVD) is the closest rank \( l \) matrix to the original matrix \( X \) and is hence the best approximation to \( X \), possible by only using \( l \) eigenvector pairs. Note that SVD filter-
where the oscillations in the data do not show too large a scaling for all three spectrograms is equal, so this clearly demonstrated that the SVD filtering significantly enhances the coherent information in the data, and the residue practically only contains noise. As in practice almost all oscillations of interest are at or below the thermal noise level, SVD filtering has proven to be almost essential for any direct plotting (still or movies) of 2D ECEI data (like also the images in Fig. 7).

Figure 10 shows examples of the spatial structure of RSAEs as measured by ECEI. The Fourier amplitude in Fig. 10(b) and mode structure (or more accurately the real part of the complex Fourier amplitude) in Fig. 10(c) show a radially localized oscillation with a poloidal mode number of around m=8. An RSAE with a second radial harmonic is shown in Figs. 10(d) and 10(e). This analysis made use of both SVD filtering to get rid of the majority of the noise, and subsequent Fourier frequency selection to pick out the separate modes. These first, local, 2D ECE measurements of the mode structure of Alfvén waves reveal more information than previous 1D measurements, and could contribute to the understanding of these modes and the associated fast particle transport. Similar results have in the mean time been achieved with another ECEI system on DIII-D.

An example of SVD filtering is shown in Fig. 9. Shown are three spectrograms of the data from a single ECEI channel (channel 8-4, shot 25525) that contains Alfvén wave activity, so called reversed shear Alfvén eigenmodes (RSAEs). These coherent oscillations have relative temperature fluctuation amplitudes of around 1%, and are hence below the thermal noise level. Figure 9(a) shows the spectrogram of the raw data (X). Figure 9(b) shows the SVD filtered data (X'), where l=10, and Fig. 9(c) shows the residue X-X'. The color scaling for all three spectrograms is equal, so this clearly demonstrated that the SVD filtering significantly enhances the coherent information in the data, and the residue practically only contains noise. In practice almost all oscillations of interest are at or below the thermal noise level, SVD filtering has proven to be almost essential for any direct plotting (still or movies) of 2D ECEI data (like also the images in Fig. 7).

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