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Techniques for Flexible Radio-over-Fibre Networks

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Abstract: Radio-over-fibre systems can efficiently deliver broadband wireless services in access and in-building networks. RoF signal transport and routing techniques are presented which are robust against fibre dispersion and provide capacity-on-demand for high-capacity multi-tone radio signals.

Keywords: Radio-over-Fibre, broadband wireless service, access network, in-building network, optical routing

1. Introduction

People have a growing need to be on-line wherever they are, in order to browse the internet, read their e-mails, exchange data files, etc. Hence telecommunication networks need to be able to provide wireless broadband services everywhere, preferably by carrying these in overlay over the same network infrastructure on which they are already transporting their wired services. In the public access domain, an UMTS base station can serve users within a cell of several km-s in diameter, and can provide wireless data services up to 2 Mbit/s. Inside buildings, an WLAN IEEE 802.11g system may cover a cell containing multiple rooms within a reach up to tens of meters, and can provide up to 54 Mbit/s. Those limited data rates have to be shared among the many users which potentially may be within a cell, hence the data rate available per user may be small and will heavily depend on the traffic loads generated by the other users in the same cell. By shrinking the cell size and increasing the wireless data rate, less users have to be served out of a larger capacity. Thus, by introducing so-called radio pico-cells the capacity per user can be significantly increased. Moreover, within such a pico-cell less users have to compete for capacity, hence the availability will be improved. An outdoor pico-cell may be constituted by an antenna creating a fixed wireless access connection in the access network (e.g. a radio beam directed to a few houses), and an indoor pico-cell by a microwave antenna covering a room.

The increased system complexity incurred with pico-cell architectures can be reduced by deploying radio-over-fibre (RoF) techniques, where the generation and modulation of the microwave signals is done at a central site, from where by means of optical fibre the signals are distributed to the simplified antenna stations.

Due to the reduced cell size, the number of users in a pico-cell may vary much more than in a UMTS or WLAN cell. Dimensioning the system such that it provides each pico-cell continuously with the maximum capacity it may need may lead to excessive overprovisioning and thus an excessive amount of system resources needed. Dynamic provisioning of capacity to each cell, i.e. just-in-time delivery of the capacity which is actually needed, can significantly improve the operation efficiency of the system.

In this paper, we report on flexible RoF systems, in which a combination of dispersion-robust RoF techniques and dynamic optical routing are deployed in order to achieve this dynamic wireless capacity provisioning.

2. The Optical Frequency Multiplying technique

Flexibly reconfiguring RoF networks implies that the link lengths along which the RoF signals have to travel may vary sizeably. Hence the RoF system should be able to handle a widely varying fibre dispersion. In access networks, the system notably has to deal with the chromatic dispersion in SMF, and in in-building networks there is a great challenge to overcome the modal dispersion occurring in multimode silica (or polymer) optical fibre. Our Optical Frequency Multiplying (OFM) RoF technique has been shown to be robust against both of these dispersion types [1].

![Fig. 1 Optical Frequency Multiplying](image-url)

As shown in Fig. 1, it is based on periodically sweeping the optical frequency of a light source in the Central Station (CS), followed by FM-to-IM conversion in an interferometric filter (e.g. an MZI). After intensity detection in the simplified Radio Access Point (RAP), the output signal of the photodiode (PD) contains many harmonics of the sweep frequency, and one of these can be selected by an electrical bandpass filter (BPF) as the desired microwave signal. The purity of the obtained microwave signal is determined by the phase noise of the sweep generator in the CS, and is not affected by the phase noise of the laser diode. As this sweep generator can be shared by multiple RAP-s, its higher costs associated with a low phase noise performance will not have a large impact on the costs per RAP. Microwave linewidths of less than 1kHz have been obtained at frequencies beyond 30 GHz; this allows comprehensive high-capacity wireless signal modulation formats such as quadrature amplitude modulation (QAM) schemes. Also it has been shown that the signal transmission is very robust...
against chromatic dispersion in SMF; Fig. 2 [2] shows the fading dips which occur with double-sideband intensity modulation (IM-DSB), while our OFM technique clearly avoids these dips. Using OFM, we showed the successful transmission of 16-QAM and 64-QAM radio signals up to 20Msymbols/s (so up to 80 and 120Mbit/s) at 39.9GHz over up to 25km of SMF in the 1310 nm wavelength band [3].

![Fig. 2 Impact of SMF dispersion on the delivery of a 22GHz RoF signal, with IM double-sideband modulation and with OFM (fibre losses are not taken into account)](image)

Also modal dispersion in multimode fibre can be overcome by our OFM technique. Successful transmission has been demonstrated of 16-QAM and 64-QAM signals up to 120 Mbit/s in the 24-30GHz band over 4.4 km silica 50μm core graded-index fibre [4]. In addition, we succeeded in handling multitone wireless signals, by transmitting 210Mbit/s 64-QAM over the same fibre link by using up to 10 subcarriers [5].

![Fig. 3 Bi-directional OFM system with remote LO delivery](image)

Next to downstream microwave signal delivery, the OFM technique can also facilitate the remote delivery of a local oscillator (LO) signal to the RAP. As illustrated by Fig. 3, bidirectional transmission has been shown over 4.4km graded-index silica fibre with a 24Mbit/s 64-QAM downstream signal at a subcarrier of 200MHz which is upconverted to 5.8GHz by the OFM technique, as depicted in Fig. 3. The 24Mbit/s 64-QAM upstream signal at 5.8GHz is downconverted to an IF of 200MHz by using the remotely generated 6GHz LO signal, and sent upstream using a relatively low-frequency FP laser diode. Also bidirectional transmission of 100Mbit/s 16-QAM signals at 17.2GHz over 100 metres of 50μm graded-index POF has been shown [7].

When conveying wireless signals over fibre links, care should be taken that the wireless transmission protocols are still respected. E.g., in the IEEE 802.16 WiMAX protocol, the time-division-duplex communication takes place alternately in the downlink (DL) and uplink (UL) subframes, which are spaced by a time gap. In an RoF system setup, this time gap is enlarged by the round trip delay of the fibre link. Hence the DL and UL subframes become shorter, and the link throughput is decreased. However, for typical frame sizes it can be shown that this decrease is less than 1% provided that the fibre link length is less than 500 meters [1].

![Fig. 4 Impact of RoF on handling of wireless protocols](image)

Thus we have demonstrated the suitability of the OFM RoF technique for both outdoor SMF and indoor MMF/POF systems.

### 3. Dynamic radio-over-fibre signal routing

In a hybrid WDM-TDM Fibre-to-the-Home network, wavelength routing can provide dynamic allocation of capacity to the individual homes, and thus improve the operation efficiency of the system’s resources. Similarly, wavelength routing in a Fixed Wireless Access (FWA) system may also improve its performance. As shown in Fig. 5, along a ring-shaped fibre access network the various RoF signals may be dropped to local antenna stations by means of tunable optical add-drop nodes (ADN-s) [8]. An ADN may also only partially drop a wavelength signal, and drop the rest at one or more other ADN-s, thus realising multi-casting. As the same RoF signal then needs to travel through different fibre lengths, the dispersion-immunity of the OFM technique enables such multicasting schemes.
feeding the RAP-s in a building. As illustrated in Fig. 6 for an in-building wireless services scenario, dynamical routing of RoF signals may be done by means of optical routing in the add-drop nodes (ADN-s) according to the ‘remote’ address information extracted from the downstream optical signal, thus enabling remotely controlled routing. Using the OFM principle, the CW optical signal is phase-modulated by the RF sweep signal \( f_{SW} \) to generate multiple optical harmonics. This phase-modulated optical signal \( \lambda_{CW} \) is injected into the SOA together with the intensity-modulated (IM) optical signal \( \lambda_{IM} \) carrying the radio signals from the CS. By tunable wavelength conversion of the RoF signal, within the RG the routing of the RoF signals can be set. Simultaneously converting an RoF signal to multiple wavelengths enables to do multicasting as well.

Based on the OFM technique, the tunable wavelength conversion can be implemented by replacing the intensity modulator in the conventional OFM configuration by cross-gain modulation (XGM) in a semiconductor optical amplifier (SOA). As illustrated in Fig. 7, we have up-converted radio signals and changed the wavelength of the OFM-swept optical signal to a new wavelength simultaneously, where the new wavelength \( \lambda_{CW} \) is provided by a local tunable CW optical source. This new wavelength can be selected according to the ‘remote’ address information extracted from the downstream optical signal, thus enabling remotely controlled routing. Using the OFM principle, the CW optical signal is phase-modulated by the RF sweep signal \( f_{SW} \) to generate multiple optical harmonics. This phase-modulated optical signal \( \lambda_{CW} \) is injected into the SOA together with the intensity-modulated (IM) optical signal \( \lambda_{IM} \) carrying the radio signals from the CS. By cross-gain modulation (XGM) in the SOA, the radio signal is duplicated onto the phase-modulated optical signal \( \lambda_{CW} \) as illustrated in Fig. 7. The converted optical signal \( \lambda_{CW} \) is routed by means of an AWG to each destination (room), where they are detected and the radio signal is selected by an electrical bandpass filter (BPF).

Fig. 8 shows the RF spectra of the input radio signal from CS and the up-converted radio signal routed to the destination, respectively. The input radio signal (64-QAM, 20MSymbol/s, \( f_{RF} = 3.6\text{GHz} \)) is successfully up-converted together with the harmonics of \( f_{SW} \) to \( f_{UP} = n f_{SW} + f_{RF} \) (where \( n \) is the order of harmonics) in Fig. 8(b). The SNR of the routed radio signal at 39.6GHz is reduced by around 16dB and there is an EVM penalty of 2.5% as compared to the input radio signal. In addition, a nonlinear skirt slope appears at the edge of the signal band. This degradation comes from the ASE.
noise of the SOA, the wavelength-conversion penalty, and the nonlinearity of the SOA gain profile. To evaluate the routing and up-conversion performance at different optical channels (wavelengths), we have measured the EVM of the routed channel ($\lambda_{CW}$) as a function of the input optical power ($P_{in}$) at the fixed IM optical power ($\lambda_{MDD}$). As shown in Fig. 9, the performance of the routed microwave signals at each channel is nearly the same, with around 4.5% EVM performance [6].

![Fig. 8 RF spectra (a) input 64-QAM signal (20MS/s) at 3.6GHz, (b) routed 64-QAM signal (20MS/s) at 39.6GHz (Inset: constellation diagram)]

![Fig. 9 Performance of up-converted radio signal at different optical channel (the power of input IM optical signal : +3dBm)]

3. Conclusions

The optical frequency multiplication technique is a promising approach for providing high-capacity wireless services over fibre in access and in-building networks. By means of optical routing in a point-to-multipoint wireless network architecture, the fibre network can efficiently deliver wireless capacity on demand. Flexible routing of radio-over-fibre signals can be realised with tunable wavelength converters in combination with passive wavelength add-drop modules.

4. Acknowledgement

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5. References