The conversion matrix for optical filters with arbitrary transfer function
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Abstract
Full analytical expressions for the effect of an arbitrary optical transfer function on small signal RF modulations are presented. Simulations of a device, having both amplitude and phase variations, were performed to prove its validity.

Introduction
Today’s modern radar systems, employing true time delay beamformers, are implemented using dispersive devices such as chirped Bragg gratings [1], as well as other dispersion compensating modules. These devices are characterized by a transfer function of the form [2]

$$H(\omega) = A(\omega) \exp\{-j\phi(\omega)\}.$$  

Future wide-bandwidth RF systems will have bandwidths representing a large fraction of the center frequency. Under these circumstances, the traditional method of analysis [3,4,5], which assumes a frequency-independent $A(\omega)$ and expands $\phi(\omega)$ around $\omega_0$, may not provide the system designer with the required accuracy. In a previous paper [6], we generalized the conversion matrix, [3,4,5], relating the optical input intensity and phase modulations to their corresponding output values, to include an arbitrary form of $\phi(\omega)$, using a fairly simple small signal analysis. However, these analyses ignore the frequency-dependence of the amplitude of the transfer function, $A(\omega)$. In this paper, we further generalize the conversion matrix to also take into account the ever-present frequency-dependent variations of the magnitude of $A(\omega)$.

Theory
The field of an input optical signal of the form

$$E_{in}(t) = \sqrt{I_{in}(t)} \exp[j\phi_{in}(t)] \exp[j\omega_0 t]$$,

caracterized by small intensity and phase variations, can be approximately expressed by

$$E_{in}(t) = \sqrt{I_{in}(t)} \cdot \left[ 1 + \frac{A_{in}(t)}{2} \right] \exp[j\omega_0 t]$$.

(1)

Assuming single tones for the intensity

$$|A_{in}(t)/2| = m/2 \cos(\omega_{RF} t + \phi_{RF})$$

and phase

$$\phi_{in}(t) = n/2 \cos(\omega_{RF} t + \phi_{RF})$$

variations, the input field can be written as

$$E_{in}(t) = \sqrt{I_{in}(t)} \left[ 1 + \frac{m}{4} \exp[j(\omega_{RF} t + \phi_{RF})] \right]$$

$$+ \frac{m}{4} \exp[-j(\omega_{RF} t + \phi_{RF})]$$

$$+ j \frac{\omega_{RF}}{4} \exp[j(\omega_{RF} t + \phi_{RF})]$$

$$+ j \frac{\omega_{RF}}{4} \exp[-j(\omega_{RF} t + \phi_{RF})]$$

$$\cdot \exp[j\omega_0 t]$$

(2)

This optical signal comprises five optical frequencies $\omega_0, \omega_0 \pm \omega_{RF}$, $\omega_0 \pm \omega_{RF}$. The propagation of the electromagnetic field through a linear optical medium is described by

$$E_{out}(\omega) = H(\omega) E_{in}(\omega),$$

where $E_{in}(\omega)$ and $E_{out}(\omega)$ are respectively, the input and output complex amplitudes of the electric field at the optical frequency $\omega$, and $H(\omega) = A(\omega) \exp[-j\phi(\omega)]$ is the optical transfer function of the
medium. Thus, at the output of the dispersive medium we get:

\[ E_m(t)/\sqrt{I} = \]
\[ \left\{ 1 + \frac{m}{4} \left[ \exp \left[ -j\Phi_{\text{in}}(\omega_m) \right] \right] \right\} \]
\[ + \frac{m}{4} \left[ \exp \left[ -j(\omega_m t - \Delta \Phi(\omega_m) + \Phi_{\text{in}}) \right] \right] \]
\[ + j \frac{m}{4} \left[ \exp \left[ -j(\omega_m t - \Delta \Phi(\omega_m) + \Phi_{\text{in}}) \right] \right] \]
\[ + j \frac{m}{4} \left[ \exp \left[ -j(\omega_m t - \Delta \Phi(\omega_m) + \Phi_{\text{in}}) \right] \right] \]
\[ \cdot (A(\omega_m) \exp \left[ j(\omega_m t - \Phi_{\text{in}}) \right] ) \]  

(3)

where

\[ \Delta \Phi(\omega_m) = \Phi(\omega_m) - \Phi(\omega_0); \]
\[ \Delta \Phi(\omega_m) = \Phi(\omega_m) - \Phi(\omega_0); \]
\[ \exp[-\gamma t] = A(\omega_m) \exp \left[ j(\omega_m t - \Phi(\omega_0)) \right] \]  

(4)

Using

\[ \Gamma_1 = \left[ \exp(-\gamma t) \right] / 2 \]
\[ \Gamma_2 = \left[ \exp(-\gamma t) \right] / 2 \]
\[ \Gamma_3 = \left[ \exp(-\gamma t) \right] / 2 \]
\[ \Gamma_4 = \left[ \exp(-\gamma t) \right] / 2 \]  

(5)

Eq. (3) can be manipulated by dividing the output \( E \) field into odd and even harmonic functions to obtain:

\[ E_m(t)/\sqrt{I} = \left\{ 1 + \frac{m}{4} \left[ \exp \left[ -j\Phi_{\text{in}}(\omega_m) \right] \right] \right\} \]
\[ + \frac{m}{4} \left[ \exp \left[ -j(\omega_m t - \Delta \Phi(\omega_m) + \Phi_{\text{in}}) \right] \right] \]
\[ + j \frac{m}{4} \left[ \exp \left[ -j(\omega_m t - \Delta \Phi(\omega_m) + \Phi_{\text{in}}) \right] \right] \]
\[ + j \frac{m}{4} \left[ \exp \left[ -j(\omega_m t - \Delta \Phi(\omega_m) + \Phi_{\text{in}}) \right] \right] \]
\[ \cdot (A(\omega_m) \exp \left[ j(\omega_m t - \Phi_{\text{in}}) \right] ) \]  

(6)

For similar expressions for \( \Phi_{\text{out}}(\omega_{\text{me}}) \) and \( \Phi_{\text{out}}(\omega_{\text{me}}) \). Thus, the Fourier transforms of the output intensity and optical phase variations at the single frequency \( \omega_{\text{me}} \), are related to their input values by:

\[ \left[ \begin{array}{c} \Delta(I/\sqrt{I}) \, \Phi(j \omega) \end{array} \right] = \left[ \begin{array}{c} T(\omega) \Phi(j \omega) \end{array} \right] \]
\[ \Delta_1 = \sqrt{[\Gamma_1 \cos(\Phi_{\text{in}}(\omega))]/[1 - \Gamma_1 \cos(\Phi_{\text{in}}(\omega))]^2} \]
\[ \Delta_2 = \sqrt{[\Gamma_2 \sin(\Phi_{\text{in}}(\omega))]/[1 - \Gamma_2 \sin(\Phi_{\text{in}}(\omega))]^2} \]
\[ \beta_1(\omega) = -\tan^{-1} \frac{\Gamma_1 \sin(\Phi_{\text{in}}(\omega))}{\Gamma_1 \cos(\Phi_{\text{in}}(\omega))} \]
\[ \beta_2(\omega) = \tan^{-1} \frac{\Gamma_2 \cos(\Phi_{\text{in}}(\omega))}{\Gamma_2 \sin(\Phi_{\text{in}}(\omega))} \]  

(9)

Since Eq. (1) is linear in both the intensity and optical phase fluctuations, and complex excitation may be Fourier decomposed and treated, frequency by frequency, by Eq. (9). To compare Eq. (9) with previously obtained results, we expand \( \Phi(\omega) \) in a Taylor series around \( \omega_0 \):

\[ \Phi(\omega + \omega') = \Phi(\omega_0) + \frac{\partial \Phi}{\partial \omega} \frac{\omega'}{\omega_0} + \frac{1}{2} \frac{\partial^2 \Phi}{\partial \omega^2} \left( \frac{\omega'}{\omega_0} \right)^2 + \frac{1}{6} \frac{\partial^3 \Phi}{\partial \omega^3} \left( \frac{\omega'}{\omega_0} \right)^3 + \ldots \]  

(10)

It is then easily shown that if only the first and second derivatives of \( \Phi(\omega) \) are non-zero (i.e., constant dispersion), Eq. (9) reduces to that of [3], and to
that of [2] when the third-order derivative is not neglected.

**Discussion**

For RF CW modulation, the phase of the intensity transfer function will not affect transmission. However, in the case of a broadband RF signal, both the phase and magnitude of the RF frequency transfer function (the top left element of the conversion matrix, $T(\omega)$, Eq. (9)) will affect the output intensity. For a wideband RF pulse, slow fluctuations of the phase error (with respect to the pulse bandwidth) will broaden the response in time, while fast fluctuations will raise its time side-lobes [5]. Using small signal analysis for an optical device with a known optical transfer function, the RF phase and amplitude of the transfer function can be quickly found from Eq. (9) and the output signal in the time domain accurately recovered. From Eqs. (9-10), when the initial excitation is pure intensity modulation, the even derivatives of the optical phase of the transfer function affect the amplitude of the intensity, while odd derivatives of the optical phase of the transfer function affect its phase. Attenuation ripples will also deteriorate the output signal, as shown below.

$$E_n(t) = \sqrt{|t|} \left[ 1 + \frac{n}{2} \cos(\omega_{\text{RF}} t + \phi_{\text{RF}}) \right] \exp[j \omega_{\text{RF}} t]$$

To calculate the effect of the optical filter, the Fourier transform of $E_n(t)$ (excluding $\exp[j \omega_{\text{RF}} t]$), obtained via an FFT, was multiplied by the filter transfer function: $A(\omega) \exp[-j \phi(\omega)]$. Finally, using the inverse FFT, the output optical field $E_{\text{out}}(t)$ is evaluated, from which, we numerically deduce the RF output intensity at $\omega_{\text{RF}}$ and its corresponding RF phase. These numerical values were compared with an analytical calculation based on Eq. (9). Our simulated optical device had a sinusoidal frequency-dependent phase, $\phi(\omega) = 40^\circ \sin[10^{-10} (\omega - \omega_0) + \pi / 4]$, with an amplitude of 40 degrees over a period of 10 GHz. As for the magnitude of the filter transfer function, several cases were examined, where the lower sideband of double sideband modulation (with $m=0.3$) was progressively attenuated by 6 and 20 dB (optical power) up to complete attenuation, namely: single sideband modulation (SSB), see Fig. 2. As expected, the results show that as the asymmetry grows larger, the resulting phase and amplitude approach that of SSB modulation [7]. Indiscernible in the figures is the fact that both numerical simulation and calculation


