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Single-transistor method for the extraction of the contact and channel resistances in organic field-effect transistors

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A simple and accurate method for the extraction of the contact and channel resistances in organic field-effect transistors (OFETs) is proposed. The method is of general applicability since only two measured output-characteristics of a single OFET are needed and no channel-length scaling is required. The effectiveness of the method is demonstrated by means of both numerical simulations and experimental data of OFETs. Furthermore, the provided analysis quantitatively shows that the contact resistance in OFETs depends on both \( V_G \) and \( V_D \), and, in the case of non-linear injecting contact, the drain-source voltage (viz. the electric field along the channel transport direction) plays a major role.

The performance of organic field-effect transistors (OFETs) is strictly connected to the charge injection from the source electrode into the organic semiconductor and to the charge transport in the channel accumulated at the gate-insulator/organic-semiconductor (OSC) interface. In the last years, the improvement of both holes and electrons mobility has been impressive. State-of-art single crystal OSCs yields OFETs with an average field-effect mobility as high as 16.4 \( \text{cm}^2/\text{V} \cdot \text{s} \). Even in the case of fully-printed low-temperature complementary organic technologies, the p- and n-type OFETs show mobilities up to 2\( \times\) 16.4 \( \text{cm}^2/\text{V} \cdot \text{s} \).

Charge injection is currently limiting the performance of organic field-effect transistors (OFETs). It restricts, and in some cases nullifies, the benefits of high-mobility organic semiconductors (OSCs) hampering the channel-length scaling. Poor charge injection results in a large contact resistance eventually leading to OFETs with reduced drive current and operating frequency, small on/off current ratio, and large threshold voltage. The aforementioned parameters are of paramount importance to achieve organic circuits operating at low supply voltage, and with a large level of integration and functionalities.

To further improve the OFET technology, it is essential to disentangle and quantify the contact and channel resistances directly from the measured electrical characteristics.

To this aim, standard techniques like four-probe measurements and transfer-line method (TLM) have been widely used. The main shortcoming is that the former require complex electrode patterning applicable only to laboratory devices; while the latter requires several nominally identical transistors with scaled channel lengths. Since organic technologies suffer from large variability and modest stability, a method able to extract the contact \( R_s \) and channel \( R_{ch} \) resistances directly from a single OFET is highly desirable. In the case of linear-injecting contacts, the transition-voltage method provides a good estimation of the contact resistance making use of the transfer and output characteristics of a single transistor. In the case of non-linear injection, which is observed in high-mobility or short-channel OFETs, the accurate extraction of \( R_p \) and \( R_A \) without the need of channel-length scaling is still an open issue.

In this letter we propose a simple and accurate method able to provide both the contact and channel resistances of OFETs with non-linear injecting contact. The method requires the measurements of only two output characteristics of a single transistor without the need of transistor scaling. We call it Single-Transistor Method (STM).

A general approach to analyze the contact is to split the channel into a small contact region, where there is a voltage drop \( V_C \), and the main channel, where the voltage drop is \( V_D - V_C \). This is schematically illustrated in Fig. 1. The contact region is spatially located at the source side of the OFET, since most of \( V_C \) drops at the injecting electrode. The drain current \( I_D \) as a function of gate \( V_G \), drain \( V_D \), and source \( V_S \) voltages is given by

\[ I_D = \beta (\Psi_S^\gamma - \Psi_D^\gamma) \]  

where \( \beta \) is a prefactor dependent on geometrical and physical parameters, \( \gamma \) accounts for the OSC energetic disorder, \( \Psi_S \) and \( \Psi_D \) are proportional to the accumulated charges per unit area at the source and drain, respectively, \( \Psi_S = V_G - V_{th} - V_{S'} \), \( \Psi_D = V_G - V_{th} - V_D \). \( V_{th} \) is the threshold voltage, and \( V_{S'} = V_S + V_C \) is the virtual source potential (i.e. the channel potential at the source side). In case of no contact resistance: \( V_{S'} = V_S \).

It was shown that the contact resistance depends on the Schottky barrier \( \Phi_B \) due to the energy misalignment between the OSC and the metal electrode, on the quality of the OSC close to the metal edge, and on the local electric fields. Hence, the contact voltage drop \( V_C \) is modeled as

\[ V_C = R_s \times I_D + V_{inj} \]

where \( R_s \) accounts for the parasitic resistance due to the OSC quality close to the contact, and \( V_{inj} \) is the contact potential required for injection.

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In the following, the idea is to calculate the contact and channel parameters (namely \( R_s, V_{inj}, \beta, \gamma, V_{th} \) in Eqs. 1-2) by means of only two output characteristics measured at two different values of \( V_G \). Once the “intrinsic” channel parameters are determined (viz. \( \beta, \gamma, \) and \( V_{th} \)), \( R_{ch} \) is given by Eq. 1 calculated at \( V_S = V_S' \) and it reads:

\[
R_{ch} = \left[ \frac{\partial I}{\partial V_D} \right]^{-1}_{\partial V_D=V_S' \atop V_S=V_S'} = \frac{1}{\beta \gamma \Psi_D^{\gamma-1}} \tag{3}
\]

and the overall contact resistance results:

\[
R_p = R_o - R_{ch} \tag{4}
\]

where \( R_o = (\partial I_D/\partial V_D)^{-1} \) is the measured output resistance. It is worth noting that the contact model (Eq. 2) is not used to directly calculate the contact resistance but only to obtain the channel parameters. This is the key point to keep both the contact model simple and the extraction procedure accurate.

Typical output characteristics and conductances measured for OFETs with non-linear injecting contacts are shown in Fig. 2. The effect of the contact resistance is readily visible in the S-shape of the \( I_D-V_D \) curve and in the non-monotonic behavior of the output conductance \( g_o = 1/R_o \).

At small values of \( V_D (V_D < V_{inj}) \), \( g_o \) strongly increases: the current is injection-limited and it is enhanced by the longitudinal electric field (viz. \( V_D \)). When \( V_D = V_{inj} \), the drain current \( I_D \approx 0 \), the measured total resistance is \( R_T = R_o(V_{inj}) \) and it reads:

\[
R_T = \left[ \frac{\partial I}{\partial V_D} \right]^{-1}_{\partial V_D=V_{inj}} = \frac{1}{\beta \gamma V_{ov}^{(1-\gamma)}} + R_s \tag{5}
\]

where \( V_{ov} = V_G - V_{th} - V_{inj} \). The inset of Fig. 2 shows the measured \( R_T \) as a function of \( V_{ov}^{(1-\gamma)} \). At least two \( I_D-V_D \) characteristics measured at different \( V_G \) voltages are required. According to Eq. 5, the intercept to the y-axis gives \( R_s \).

When \( V_D > V_{inj} \) the drain current linearly increases with \( V_D \) thus indicating that the injection process becomes rather efficient and the source contact supplies enough carriers for the channel transport. The output conductance has a maximum \( g_{15}^* \) at \( V_D = V_D^* \), and in this region the drain current \( I_D = g_{15}^*(V_D - V_{inj}) \) (Fig. 2), which gives:

\[
V_{inj} = V_D^* - I_D^*/g_o^* \tag{6}
\]

where \( I_D^* \) is the measured \( I_D \) at \( V_D = V_D^* \). \( V_{inj} \) is the crossing point between the x-axis and the linear fit of \( I_D \) around the point \( I_D = I_D^* \) (top panel of Fig. 2).

When the drain voltage is larger than \( V_D^* \) \( (V_D < V_{Dsat}) \), \( g_o \) monotonically decreases: the current is limited by the charge transport in the OFET channel, and the measured output resistance is \( R_o \approx R_s + R_{ch} \) in region the drain current \( I_D = g_o^*(V_D - V_{inj}) \) (Fig. 2), which gives:

\[
V_{inj} = V_D^* - I_D^*/g_o^* \tag{6}
\]

where \( V_{ov} = V_G - V_{th} - V_{inj} \). The inset of Fig. 2 shows the measured \( R_T \) as a function of \( V_{ov}^{(1-\gamma)} \). At least two \( I_D-V_D \) characteristics measured at different \( V_G \) voltages are required. According to Eq. 5, the intercept to the y-axis gives \( R_s \).

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\[
V_{inj} = V_D^* - I_D^*/g_o^* \tag{6}
\]

where \( I_D^* \) is the measured \( I_D \) at \( V_D = V_D^* \). \( V_{inj} \) is the crossing point between the x-axis and the linear fit of \( I_D \) around the point \( I_D = I_D^* \) (top panel of Fig. 2).

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\[
V_{inj} = V_D^* - I_D^*/g_o^* \tag{6}
\]
Hence, given an $I_D - V_D$ curve, the parameters $V_{inj}$, $\gamma$, and $V_{th}$, are obtained using Eqs. 6, 7, and 8, respectively. $\gamma$ is firstly calculated assuming $R_s = 0$ in Eq. 7, and it is used as an initial value. As a second step, another output curve is measured and $R_s$ is calculated according to Eq. 5. Then, $R_s$ is plugged into Eq. 7 and a new value of $\gamma$ is obtained. Since the OFET operating conditions guarantee that in Eq. 7 $R_o >> R_s$, only few iterations of Eqs. 5, and 7 are required. Finally, by observing that at $V_D = V_D^o$, the maximum of the output conductance can be written as $g_D^o = \beta \gamma \Psi_D^o/(1 + \beta \gamma R_o \Psi_S^o)$, the parameter $\beta$ reads:

$$\beta = \left\{ \frac{\gamma}{g_D^o} \left[ \psi_D^o (\gamma - 1) - g_D^o R_S \psi_S^o (\gamma - 1) \right] \right\}^{-1} \tag{9}$$

The contact and channel resistances determined with the proposed method (STM) and the widely used TLM are shown in Fig. 3. There is a very good agreement between the two methods in the whole range of gate voltages. It is worth noting that OFETs with different channel lengths are required by the TLM (inset of Fig. 3) while the STM enables to calculate $R_p$ and $R_{ch}$ with only one OFET.

In order to assess the accuracy of the proposed method, the “exact” contact and channel resistances calculated with the numerical model proposed in 20 are compared to the values given by the STM in Fig. 4. The numerical model 20 is taken as a benchmark because it accounts for both charge injection and transport in OFETs and it accurately reproduces the measurements reported in 20, 28. The results show a very good agreement in the whole range of gate and drain voltages. As expected, increasing $V_G$ both $R_{ch}$ and $R_p$ get smaller (Fig. 4, left panel). The lowering of the contact resistance with $V_G$ is commonly observed in contact-limited OFETs and it is explained by trap-filling 14, Schottky-gated injection 16, and spatial modulation of the contact region 19.

$R_{ch}$ and $R_p$ show an opposite dependence on the drain voltage (Fig. 4, right panel). $R_{ch}$ increases with $V_D$ because the transistor is moving towards the saturation; while $R_p$ decreases since the injection process is enhanced by the electric field. $R_{ch}$ and $R_p$ as a function of both $V_G$ and $V_D$ are shown in Fig. 5. Independently of the gate voltage, at $V_D \approx 3V$ results that $R_{ch} = R_p$. We also found that the transition voltage from contact-limited to channel-limited current corresponds to the injection voltage $V_{inj}$ and it increases at larger Schottky barriers. This behavior can be explained as follows. A depleted region in the OSC close to the source electrode is formed because of the metal-organic energy misalignment. Since the transistor is a bottom-gate bottom-contact architecture, the width of the depleted region is basically independent of the barrier height $\Phi_B$ and hence the drain voltage enhances the charge injection by lowering $\Phi_B$. Increasing the barrier height, larger $V_D$ is required to turn the non-linear injecting contact into an ohmic-like contact such that $R_p < R_{ch}$. Such a behavior suggests that a strongly contact-limited OFET biased at large $V_G$ and $V_D < V_{inj}$ could be the ideal condition to assess the metal-organic contact properties.

In the light of the previous analysis, we can conclude that at small drain voltages ($V_D \leq V_{inj}$) the current is severely contact limited, while for $V_D \geq V_{inj}^o$ the channel resistance is dominant compared to the contact resistance, and $R_o(V_D^o) \approx R_{ch}(0)$. Hence, the presented method can be further simplified and the contact and channel resistances can be extracted directly from a single output characteristic (inset of Fig. 6): when $V_D$ is small (i.e. $V_D < V_{inj}$) the overall resistance is $R_o = 1/g_D^o(0) = R_r + R_{ch}$, $R_{ch} \approx 1/g_D^o$, and $R_p = R_o - R_{ch} = 1/g_D^o(0) - 1/g_D^o$. Fig. 6 shows a good
and the drain voltage plays a major role in the charge injection process. The presented approach is general and can be applied to any transistor technology where non-linear injection takes place, as for example zinc-oxide transistors\(^2\). 


\(^26\)F. Torricelli, E. Cantatore, G. H. Gelincck, K. Myny, and J. Genoe, 13th Workshop on Nanoelectronics at the University of Twente, Enschede (The Netherlands), 179-174 (2010).

