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The Impact of Deadline Misses on the Control Performance of High-End Motion Control Systems

W. Geelen, D. Antunes, Member, IEEE, J.P.M. Voeten, R.R.H. Schiffelers, W.P.M.H. Heemels, Senior Member, IEEE

Abstract—In high-end motion control systems the real-time computational platform must execute tasks from multiple control loops operating at high sampling rates. In recent years traditional special-purpose platforms have been replaced by general-purpose multi-processor platforms, which introduce significant fluctuations in execution times. While considering worst-case execution times would severely reduce the sampling rates, accepting deadline misses and assuring that the control system still meets the desired specifications is challenging. In this paper, we provide a framework to model and assert the impact of deadline misses in a real-time control loop. We consider stochastic models for deadline misses and characterize the mean and the variance of closed-loop output variables based on a time-domain analysis. We illustrate the usefulness of our framework in the control of a benchmark motion control experimental setup and in the control of a wafer stage in a lithographic machine.

Keywords—Deadline misses, data losses, packet drops, performance analysis, stochastic analysis, industrial case study, hybrid systems, cyber-physical systems, real-time systems

I. INTRODUCTION

High-performance real-time control systems require a tight integration between embedded systems and control engineering [1]–[4]. This is the case, for example, in the context of photolithographic systems for the semiconductor industry, which require nanometer-level positioning precision. These systems incorporate multiple control loops having very high sampling rates to meet the desired precision. This imposes strict constraints on the input-output (IO) delays of a control task schedule, which should be met by the real-time computational platform. Conversely, the design of the controller should take into account the potential and limitations of the computational platform.

In the past decade traditional special-purpose platforms have been replaced by general-purpose multi-processor platforms [5], mainly due to reasons of cost and flexibility. This replacement leads to the introduction of significant variability in the task execution times [6, p. 12]. Dimensioning the platform for worst-case execution times, is either very costly or results in a large sample-rate reduction and thereby possibly unacceptable performance degradation in the context of high-performance motion control. An alternative is to still use high sampling rates, but allow task deadline misses, i.e., events where tasks are not completed within the sampling period, which in general result in data losses in the control loop. However, deadline misses are often ignored in the analysis and design of the control loops because of two main reasons: (i) realistic models of deadline misses suitable for controller design are typically not available; and (ii) it is hard to quantify the impact of data losses in the closed-loop performance with state-of-the-practice control methods. Although quite some results on the analysis of control systems subject to data losses are available in the literature, see, e.g., [7]–[17] and the references therein, these results typically lead to (asymptotic) guarantees only on (mean square) stability or quadratic costs and do not immediately provide insights on various important performance indicators such as overshoot, settling time, rise time, etc., of the time responses. Clearly, the latter performance indicators are of high importance for the controller design and are frequently used in industrial practice for controller tuning. Besides focusing mainly on stability guarantees, the analyses in the Networked Control Systems (NCS) literature sometimes rely on techniques (e.g., LMIs) that are not so common in engineering practice. In control engineering practice one often adopts time-domain or frequency-domain methods (e.g., loop-shaping techniques) for the analysis and synthesis of control systems. As a result, LMI-based tools are not so easily embraced by control engineering in industry. Since deadline misses can significantly degrade the performance of high-end motion control systems, it is extremely important to quantify their impact on the control performance in terms of, e.g., overshoot, settling-time, or rise-time. Understanding this impact provides important information for (re)designing the control system and/or the real-time platform.

Motivated by this lack of tools, the objective of this paper is to develop an analysis and design framework for motion control systems incorporating deadline misses that (i) provides results on important performance indicators such as overshoot, settling time, rise time, etc. and (ii) does connect to the motion control...
This paper is organized as follows. In Section II the problem formulation is presented, and we discuss two models for taking into account deadline misses in a control loop. Section III provides methods to analyze the models presented in the previous section. Section IV and Section V illustrate the applicability of the proposed analysis. Section IV considers a benchmark motion control experimental setup, while Section V provides an industrial case-study. Section VI provides concluding remarks.

II. PROBLEM FORMULATION

In this paper we consider industrial high-end motion control systems in which several control tasks are executed on a general-purpose multi-processor platform. The main tasks that typically have to be executed by a control loop are: (i) acquire sensor data from the IO board; (ii) compute the control inputs for the actuators; (iii) output the control inputs to the IO board. Due to the variability on the execution times of the tasks that the real-time platform must perform (see Fig. 1), deadline misses may occur in any of these tasks. These deadline misses may cause data losses in the control loop. This is portrayed in Fig. 2 considering a single-input single-output (SISO) control loop for which data losses can either occur at the plant’s input or at the output.

The plant $P$ and the controller $C_{dh}$ are assumed to be described by the linear models

$$x_{k+1}^p = A_p x_k^p + B_p (\tilde{u}_k + \nu_k),$$
$$y_k = C_p x_k^p + \eta_k$$  \hspace{1cm} (1)

and

$$x_{k+1}^c = A_c x_k^c + B_c (u_k - \tilde{y}_k),$$
$$u_k^c = C_c x_k^c + D_c (r_k - \tilde{y}_k),$$
$$u_k = u_k^d + u_k^b,$$  \hspace{1cm} (2)

respectively, where $x_k^p \in \mathbb{R}^{n_p}$ and $x_k^c \in \mathbb{R}^{n_c}$ denote the state of the plant and of the feedback controller at time $t_k := kh$, with $h$ being the sampling period and $k \in \mathbb{N}$ denoting the discrete time. Moreover, $u_k^d$, $u_k^c$, $u_k$ and $\tilde{u}_k$ denote the output of the feedback controller, the feedforward control input signal, the control output (sum of the feedback control and feedforward control input signal) and the available control signal at the plant, respectively. The available control input at the plant would coincide with the output of the feedback controller in the absence of data losses. We will model shortly how the two are related in the presence of data losses. The output of the plant and the available output of the plant at the controller are denoted by $y_k$ and $\tilde{y}_k \in \mathbb{R}^{n_y}$, respectively. Furthermore, $\nu_k \in \mathbb{R}^{n_u}$ and $\eta_k \in \mathbb{R}^{n_y}$ denote the disturbance at the input and the output of the plant, respectively, at discrete time $k \in \mathbb{N}$, with mean $\mu_\nu \in \mathbb{R}^{n_u}$ and $\mu_\eta \in \mathbb{R}^{n_y}$ and covariance $\Sigma_\nu \in \mathbb{R}^{n_u \times n_u}$ and $\Sigma_\eta \in \mathbb{R}^{n_y \times n_y}$, respectively. In addition, $r_k \in \mathbb{R}^{n_r}$ is the reference signal, at discrete time $k \in \mathbb{N}$. Finally, the real and available error are defined as $e_k := r_k - y_k$ and $\tilde{e}_k := r_k - \tilde{y}_k$, respectively, at discrete time $k \in \mathbb{N}$. For the remainder of this paper, we assume that for every $k \in \mathbb{N}$, $r_k$ and $u_k^d$ are deterministic and bounded signals.
where the entries of the first column indicate if data losses occur at discrete time $k \in \mathbb{N}$. Likewise, $\theta$ is a Bernoulli process corresponding to the chain with a transition matrix $P_\theta$ of the following special structure

$$P_\theta = \begin{bmatrix} p_\theta & 1 - p_\theta \\ p_\theta & 1 - p_\theta \end{bmatrix},$$

where $p_\theta$ denotes $\mathbb{P}[\theta_k = 1]$.

We introduce the mode $\sigma_k$ to indicate combinations of data losses that occur at discrete time $k \in \mathbb{N}$, as

$$\sigma_k := \begin{cases} 1 & \text{if } (\gamma_k, \theta_k) = (1, 1), \\ 2 & \text{if } (\gamma_k, \theta_k) = (1, 0), \\ 3 & \text{if } (\gamma_k, \theta_k) = (0, 1), \\ 4 & \text{if } (\gamma_k, \theta_k) = (0, 0). \end{cases}$$

Similar to $\gamma$ and $\theta$, $\sigma$ is a Markov chain. Its transition matrix is obtained by the Cartesian product of the two Markov chains of $\gamma$ and $\theta$, i.e., $P_\sigma = P_\gamma \otimes P_\theta$, where $\otimes$ denotes the Kronecker product [25]. Note that the proposed model for scenario 1 can be easily extended to capture MIMO systems as well. In fact, in section II-B we will provide the complete model for the MIMO case where each entry in the plant’s input and each entry in the plant’s output satisfies a model as in (3) and (4), respectively.

2) Scenario 2: In contrast to scenario 1, in this scenario a control task is not aborted when it exceeds its deadline. This behavior can be caused by a static-order task scheduler, which schedules the tasks in a certain order after which the tasks cannot be deleted or stopped.

A consequence of this scenario is that a finite number of control values need to be memorized in the model up to a certain horizon $n_\tilde{u}$, which is the worst-case number of consecutive deadline misses, assuming it is finite. This behavior can be captured by

$$\tilde{u}_k = \begin{cases} u_k & \text{if } \psi_k = e_1, \text{ no lag} \\ u_{k-1} & \text{if } \psi_k = e_2, 1 \text{ sample lag} \\ \vdots & \\ u_{k-n_\tilde{u}} & \text{if } \psi_k = e_{n_\tilde{u}+1}, n_\tilde{u} \text{ samples lag}, \end{cases}$$

where $\psi_k := [\psi_{1,k} \ldots \psi_{n_\tilde{u}+1,k}] \in \{e_1, \ldots, e_{n_\tilde{u}+1}\}$ indicates which input is applied to the plant, $e_i$ denote the vector of the standard basis in $\mathbb{R}^{n_\tilde{u}+1}$, e.g., $e_2 = [0 \ 1 \ 0 \ \cdots \ 0]$. In particular, when $\psi_k = e_1$, $\tilde{u}_k = u_{k-i+1}$ is applied. The available input at the plant can now be described by the following linear model

$$\tilde{u}_k = A_u \begin{bmatrix} u_k \\ \tilde{u}_{k-1} \end{bmatrix}, \quad \tilde{u}_k = \psi_k \begin{bmatrix} u_k \\ \tilde{u}_{k-1} \end{bmatrix},$$

where, as before, $\theta_k$ equals zero if data losses occur and equals one if no data losses occur at discrete time $k \in \mathbb{N}$. Likewise, $\theta$ is a Bernoulli process corresponding to the chain with a transition matrix $P_\theta$ of the following special structure

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where $\psi_k := [\psi_{1,k} \ldots \psi_{n_\tilde{u}+1,k}] \in \{e_1, \ldots, e_{n_\tilde{u}+1}\}$ indicates which input is applied to the plant, $e_i$ denote the vector of the standard basis in $\mathbb{R}^{n_\tilde{u}+1}$, e.g., $e_2 = [0 \ 1 \ 0 \ \cdots \ 0]$. In particular, when $\psi_k = e_1$, $\tilde{u}_k = u_{k-i+1}$ is applied. The available input at the plant can now be described by the following linear model

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$$P_\theta = \begin{bmatrix} p_\theta & 1 - p_\theta \\ p_\theta & 1 - p_\theta \end{bmatrix},$$

where $p_\theta$ denotes $\mathbb{P}[\theta_k = 1]$.
A. Markov Jump Linear System Model

The closed-loop system (see, e.g., Fig. 2) can have different modes due to data losses, see (5). These mode switches are governed by the discrete-time stochastic process $\sigma$. A crucial step in our analysis is to note that, when the stochastic process $\sigma$ is a Markov chain, the closed-loop system can be described by a discrete-time Markov Jump Linear System (MJLS) [21]. A discrete-time MJLS is a class of models taking the general form

$$\rho_{k+1} = M_{\pi_k} \rho_k + N_{\pi_k} \omega_k$$

$$u_k = Q_{\pi_k} \rho_k + R_{\pi_k} \omega_k$$

(7)

where $\rho_k$, $u_k$, $\omega_k$ denote the state, output and input signals, respectively, and $\pi_k \in \mathcal{M}$ is described by a Markov chain taking values in a finite set $\mathcal{M}$ with transition probabilities $P_{ij} = P[\pi_{k+1} = i | \pi_k = j]$ for $i, j \in \mathcal{M}$. We show next how to model the closed-loop system with deadline misses by a MJLS, with: (i) the state $\rho$ incorporating the plant and controller states and auxiliary states; (ii) $\pi$ coinciding with the stochastic process $\sigma$; and (iii) $\omega_k$ and $\nu_k$ being the external inputs and output of the closed-loop system, respectively. We also specify next the matrices appearing in the model (7).

We consider here for reasons of generality a MIMO system assuming that each entry of the plant’s input and each entry of the plant’s output satisfies a model as in (3) and (4), respectively. Naturally, it can also happen that certain entries in the plant’s output and plant’s input are gathered in one node and all of them miss the deadline or all of them do not miss the deadline. However, here we consider that each entry can have a deadline miss independently of the other entries. In this case assuming the behavior as in scenario 1, the closed-loop system, consisting of (1) to (5) leads to

$$\xi_{k+1} = A_{\sigma_k} \xi_k + B_{\sigma_k} r_k + E_{\sigma_k} u_k^p + G_{\sigma_k} w_k$$

$$\zeta_k = C_{\sigma_k} \xi_k + D_{\sigma_k} r_k + F_{\sigma_k} u_k^p + H_{\sigma_k} w_k$$

(8)

where $\xi_k := [x_k^T \ x_k^T \ y_k^{-1} \ \hat{y}_{k-1}]^T$, $\zeta_k := y_k$ is the output of the plant and $w_k := [v_k^T \ \eta_k^T]^T$. The matrices for the state equation are

$$A_\sigma := \begin{bmatrix} A_p - B_p \Sigma D_p \Theta_p & B_p \Sigma C_p & -B_p \Sigma D_p (I - \Theta) & B_p (I - \Gamma) \\ -B_p \Theta_p C_p & A_k & -B_p \beta (I - \Theta) & 0 \\ -\Gamma \Theta_p C_p & 0 & A_k & -\Gamma \Theta (I - \Theta) \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

$$B_\sigma := \begin{bmatrix} B_p \Gamma D_p \\ 0 \\ \Gamma \theta & 0 \\ 0 \end{bmatrix}, \quad E_\sigma := \begin{bmatrix} B_p \Gamma \\ 0 \\ \Gamma \theta & 0 \\ 0 \end{bmatrix}, \quad G_\sigma := \begin{bmatrix} B_p -B_p \Sigma D_p \Theta_p \\ 0 \\ \Theta & 0 \\ 0 \end{bmatrix}$$

where $\sigma \in \{1, \ldots, 2^{n_x + n_y}\}$, $\Gamma \in \{ \text{diag}(\gamma_1, \ldots, \gamma_{n_x}) \mid \gamma_i \in \{0, 1\} \}$ and $\Theta \in \{ \text{diag}(\theta^1, \ldots, \theta^{n_y}) \mid \theta^i \in \{0, 1\} \}$. The matrices for the output equation depend on the output of interest. For example, if we are interested in the output of the plant $y_k$ we have

$$C_\sigma := [C_p \ 0 \ 0 \ 0], \quad D_\sigma := 0, \quad F_\sigma := 0, \quad H_\sigma := [0 \ I]$$

and if we are interested in the error $y_k - r_k$ we have

$$C_\sigma := [C_p \ 0 \ 0 \ 0], \quad D_\sigma := -I, \quad F_\sigma := 0, \quad H_\sigma := [0 \ I]$$

Note that in this case the matrices $C_\sigma$, $D_\sigma$, $F_\sigma$ and $H_\sigma$ do not depend on the mode $\sigma$, but for reasons of generality we allow $C_\sigma$, $D_\sigma$, $F_\sigma$ and $H_\sigma$ to depend on $\sigma$, as well. For instance, if the output $\zeta_k$ of (8) is chosen as $u_k$, then these matrices depend on $\sigma$.

Due to the assumption that each entry of the plant’s input and plant’s output follows its own Bernoulli-type model (independent of the other entries), we have that each of the modes $\sigma \in \{1, 2, \ldots, 2^{n_x + n_y}\}$ has a probability $p_{\sigma}$ of occurring (which is independent of time, or what happened at the previous time step). This is basically the modeling setup we will be working with in this paper, which is a special form of a MJLS. Also in case of scenario 2, a similar special form of a MJLS can be formulated.

III. ANALYSIS

The analysis of a motion control loop in industrial practice is often pursued by either using time-domain or frequency-domain techniques for time-invariant systems. The time-domain analysis evaluates the output responses to reference signals of interest, e.g., step functions, via simulation and is concerned with properties such as settling time, rise time, overshoot, etc. The frequency-domain analysis relies typically on Bode plots of (complementary) sensitivity (transfer) functions [26] to determine how the closed-loop tracks desired input signals and rejects disturbance signals.

However, the model (8) that we have obtained to capture deadline misses in the control loop is in general a time-varying model, for which such time-domain and frequency-domain
techniques are not available, as they rely heavily on the properties of time-invariance. In fact, concepts such as step responses and sensitivity plots [26, p. 151, 279] are only useful or even applicable to time-invariant models, which is a condition not satisfied in our setup of Section II-A1 and Section II-A2 if deadline misses would occur.

In this section we present an approach which still allows to define concepts as step responses for the system of interest. To this effect, we exploit the stochastic structure in (8), i.e., the fact that the data losses caused by deadline misses are captured by a MJLS [21].

Key to our analysis is to notice that for such models, the statistical moments such as the mean and the variance are described by time-invariant systems. This enables us to provide similar techniques for the considered class of models (8) as for time-invariant systems. Although, recently a frequency-domain analysis for time-varying systems as in (8) has been developed in [19], [20], in this work we focus on time-domain techniques for reasons of completeness.

We introduce the following definitions pertaining to the matrices $A_2$ and $B_2$ in (8), which exhibit 1 to $N$ different modes, i.e., $\sigma \in \{1, 2, \ldots, N\}$, according to the Markov chain $\sigma$ described by a transition matrix $P_\sigma$:

$$A := \mathbb{E}[A_\sigma] = \sum_{i=1}^{N} p_i A_i,$$

$$\bar{A} := \mathbb{E}[A_\sigma \otimes A_\sigma] = \sum_{i=1}^{N} p_i (A_i \otimes A_i).$$

Herein, $\mathbb{E}[\cdot]$ is the expectation operator and $p_i = P[\sigma_k = i]$. In addition, for $A$ and $B$ of appropriate sizes, let $T$ be the unique matrix such that $TA \otimes B = B \otimes A$. Then, we define

$$N^A_T := \mathbb{E}[A_\sigma \otimes B_\sigma + B_\sigma \otimes A_\sigma T] = \sum_{i=1}^{N} p_i (A_i \otimes B_i + B_i \otimes A_i T).$$

We assume the following stability notion, typically considered for MJLS [21, Ch. 3].

**Assumption 2** The (unforced) system (8) with $r_k = 0$ and $u_k^f = 0$ for all $k \in \mathbb{N}$, is mean square stable, i.e., for every $\xi_0$, $\lim_{k \to \infty} \mathbb{E}[\| \xi_k \|^2] = 0$.

The MJLS is mean square stable (MSS) iff $\bar{A}$ is Schur [21, p. 36], i.e., all eigenvalues $\lambda_i$ of $\bar{A}$ satisfy $|\lambda_i| < 1$.

Consider the MJLS in (8). As we show next, although the system is time-varying, the expected value and the second order statistical moments of the state, can be described by linear time-invariant systems. Let vec$(A)$ be the vectorization operation as defined in [25, p. 60] for square matrices, and let its inverse be defined by vec$^{-1}$(vec$(A)$)$ := A$.

**Theorem 1** Consider the MJLS in (8) and suppose that Assumptions 1 and 2 hold. Then

$$\beta_{k+1} = A \beta_k + B r_k + \mathcal{E} u_k^f + \mathcal{C} \mu_{\nu \eta},$$

$$\alpha_k = \bar{C} \beta_k + \bar{D} r_k + \bar{F} u_k^f + \bar{H} \mu_{\nu \eta},$$

where $\beta_k := \mathbb{E}[\xi_k]$ is the expected value of the state, $\alpha_k := \mathbb{E}[\zeta_k]$ is the expected value of the output and $\mu_{\nu \eta} = [\nu^T \eta^T]^T$ is the expected value of $w_k$, and $\bar{A}$ is a Schur matrix. Moreover, the covariance of the output $\zeta_k$ is given by

$$\text{covar}(\zeta_k) = \mathbb{E}[(\zeta_k - \mathbb{E}[\zeta_k]) (\zeta_k - \mathbb{E}[\zeta_k])^T],$$

$$\text{covar}(\zeta_k) = \mathbb{E}[\zeta_k \zeta_k^T] - \alpha_k \alpha_k^T,$$

where $\mathbb{E}[\zeta_k \zeta_k^T] = \text{vec}^{-1}(\varphi_k)$ and $\varphi_k := \mathbb{E}[\zeta_k \otimes \zeta_k]$ is obtained in terms of $\vartheta_k = \mathbb{E}[\xi_k \otimes \xi_k]$ as follows

$$\vartheta_{k+1} = \bar{A} \vartheta_k + \mathcal{E} \nu_{\eta \nu} + \mathcal{F} \nu_{\eta \nu} + \mathcal{G} \nu_{\eta \eta} + \mathcal{H} \mu_{\nu \eta},$$

$$\varphi_k = \bar{C} \vartheta_k + \mathcal{D} \nu_{\eta \eta} + \mathcal{F} \nu_{\eta \eta} + \mathcal{H} \mu_{\nu \eta},$$

where $\Sigma_{\nu \eta} = \text{diag}(\Sigma_{\nu \nu}, \Sigma_{\eta \eta}) = \begin{bmatrix} \nu^T & \eta^T \end{bmatrix} \Sigma \begin{bmatrix} \nu & \eta \end{bmatrix}$.

**Proof:** Equation (9) can be obtained by taking expected values in the state equation in (8) and using the fact that $\mathbb{E}[A_\sigma \xi_k] = \mathbb{E}[A_\sigma] \mathbb{E}[\xi_k]$. This latter property follows from the fact that $\mathbb{E}[\xi_k]$ is only a function of the random variables $\sigma_{k-1}, \sigma_{k-2}, \ldots$ which are independent of $\sigma_k$ due to Assumption 1. The statement that (9) is stable in the sense that $\bar{A}$ is Schur is a consequence of Assumption 2 and follows from the fact that $\mathbb{E}[\zeta_k] \mathbb{E}[\zeta_k]^T \leq \mathbb{E}[\xi_k \xi_k]^T$. That is, when the variance converges the expected value converges as well, i.e., when $\bar{A}$ is Schur than $\bar{A}$ is Schur as well. The equations for the variance can be obtained by using the properties of the Kronecker product and appealing again to Assumption 1 in a similar fashion to the argument used to obtain (9). [Opt1.3 extern]

The LTI systems (9) and (11) provide us the means to infer information about the behavior of the time-varying system (MJLS) (8) in terms of the first and second moments and also the covariance of the output $\xi_k$ (10). This gives valuable information about the behavior (e.g., step responses) of the system by using classical tools for LTI systems. In a similar manner also information about higher order moments can be obtained, if needed. Note that this analysis can be carried out when different reference signals are applied (e.g. sinusoids, triangle, square or periodic signals). For each signal we can quantify if the data losses lead to acceptable performance degradation in terms of the time-responses. It is also possible to perform a frequency-domain analysis, as proposed in [19], and reason in terms of this analysis on the behavior of the output to any reference signal, in a similar fashion to the frequency-domain analysis for LTI systems. However, we do not pursue this analysis here for the sake of brevity. From this frequency-domain analysis we can also conclude that the data losses do not affect steady state errors, i.e., the asymptotic errors obtained when the input signal becomes a constant, possibly after a given time. This means that the asymptotic variance of the output response to a constant signal is zero and the asymptotic expected value coincides with the steady state value.
just where (12) was then fitted in the frequency domain, leading to the parameters frequency response of the system was first obtained. The model of each load. This results in the continuous time-invariant model constant in \( \text{N m} \). We will focus in this study on controlling the two loads, which are connected to each other by a thin, flexible bar. One of the loads is directly connected to the motor and two encoders measure the rotation of each load. The physical system and a schematic of the dynamical model are shown in Fig. 5.

The dynamics of the PATO system are described by

\[
\begin{align*}
J_1 \ddot{x}_1 &= c(x_2 - x_1) + d(\dot{x}_2 - \dot{x}_1) + u, \\
J_2 \ddot{x}_2 &= c(x_1 - x_2) + d(\dot{x}_1 - \dot{x}_2).
\end{align*}
\]

Herein, \( J_1 \) and \( J_2 \) are the moments of inertia in [kg m\(^2\)] of the two loads, \( d \) is the damping factor in [N m s] and \( c \) is the spring constant in [N m]. We will focus in this study on controlling the first load. This results in the continuous time-invariant model described by

\[
\begin{align*}
\dot{x}_p(t) &= A_p x_p(t) + B_p u(t) \\
y(t) &= C_p x_p(t), \tag{12}
\end{align*}
\]

where \( t \in \mathbb{R}_{\geq 0} \) and

\[
A_p = \begin{bmatrix}
-c/J_1 & -d/J_1 & 0 & 0 \\
0 & 0 & 0 & 1 \\
c/J_2 & d/J_2 & -c/J_2 & -d/J_2 \\
d/J_1 & 0 & 0 & 0
\end{bmatrix}, \quad B_p = \begin{bmatrix}
0 \\
1/J_1 \\
0 \\
0
\end{bmatrix}, \quad C_p = \begin{bmatrix}
1 & 0 & 0 & 0
\end{bmatrix}.
\]

By a three-point frequency measurement [27, p. 11] the frequency response of the system was first obtained. The model (12) was then fitted in the frequency domain, leading to the parameters

\[
J_1 := 2.4561 \times 10^{-4}, J_2 := 2.4642 \times 10^{-4}, \\
d := 7.7954 \times 10^{-4} \quad \text{and} \quad c := 16.069.
\]

A controller was designed such that the closed-loop system has a bandwidth of approximately 10 [Hz]. It consists of the series of a lead-lag controller, with transfer function having a zero at 3 Hz and pole at 30 Hz and with gain 0.05, and a second order notch filter described by the transfer function \( \frac{n_{f, \beta}(s)}{n_{f, \beta}(s)} \), where \( n_{f, \beta} = \frac{1}{2\pi f} s^2 + \frac{2 \beta_2}{2\pi f} s + 1 \) and \( f_1 = 57, f_2 = 58, \beta_1 = 0.01, \beta_2 = 0.1. \) The feed-forward control input signal is set to zero. Both the PATO model and the controller are discretized using the bilinear (Tustin) method [28] with a sampling period of \( h = 1 \text{ [ms]} \), leading to the plant and controller models (1) and (2).

**Remark 1** The setup has a limited control input range and as a result, the control effort is saturated. This causes non-linear behavior, which is not captured by our model. As a consequence, we designed our controller such that the control effort stays within the boundaries of the saturation. Furthermore, the setup is under the influence of other non-linear phenomena such as quantization and Coulomb and viscous friction.

We investigate the behavior of the PATO system with emulated data losses in the c-a and s-c channels corresponding to the behavior described in scenario 1, see section II-A1. Hence, \( n_a = 1 \) and \( n_c = 1 \) result in \( 2^{1+1} = 4 \) modes. Fig. 6a and Fig. 6b show the results for 250 simulations and experiments for the case where a step function is applied as a reference. On top of the simulation and experimental results the analytically computed expected value \( \mathbb{E}[y_k] \) and standard deviation \( \sigma_k \) are shown using the methodology based on (9) and (11) described in Section III. Fig. 7 shows the analytically computed variance and the variance computed based on the results from the simulation and experiments.

From Fig. 6a, with data losses in the c-a channel, we observe that the simulations of the model closely follow the results, which we obtained analytically. The experimental results show the same behavior, although, the results seem to be more concentrated. This is verified by the variance given in the left plot of Fig. 7. Looking at Fig. 6b, in which data losses occur in the s-c channel, both the model and the experiments closely follow the results that we obtained analytically. In addition, from Fig. 6 we observe that data losses, which occur in the c-a channel have a more significant impact on the responses than data losses, which occur at the s-c channel.

Looking at the left plots of Fig. 6a and Fig. 6c, which show the simulation results for 25%, 50% and 75% data losses, it is clear that an increase in the deadline miss probability increases the uncertainty in the output responses to deterministic inputs such as steps responses. The proposed analysis allows to quantify this impact of the deadline misses on the output response. In this specific experimental study one can conclude that 25% of data losses does not degrade the output responses significantly when compared to the case where deadline misses are absent. However, the degradation of 50% data losses is quite notorious and a degradation of 75% data losses is not acceptable. Using our methods we are able to quickly determine the impact of data losses. As a result, we are able to assess, for instance, the overshoot as a function of the probability that data losses occur in the c-a channel and the sampling period.
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(a) 50% chance of data losses in the controller-to-actuator channel, i.e., \( P[\gamma_k = 0] = 0.5 \) and \( P[\theta_k = 0] = 0 \).

(b) 60% chance of data losses in the sensor-to-controller channel, i.e., \( P[\gamma_k = 0] = 0.6 \) and \( P[\theta_k = 0] = 0.6 \).

(c) Two simulations for 25% and 75% chance of data losses in the controller-to-actuator channel.

Fig. 6. Step response of the PATO system and its model for 250 simulations, 250 experiments and its analytically computed expected value \( E[y_k] \) and standard deviations \( \sigma \).

the result of which is a 3D-plot Fig. 8. Indeed, based on Fig. 1, we can also plot the probability of data losses as a function of the sampling period (solid line in 8). The area underneath the probability distribution in Fig. 1 defines the probability that data losses will occur. By plotting the probability of data losses as a function of the sampling period on top of the 3D-plot

Fig. 7. Comparison of the variance computed analytically, by the model simulations and by the experiment results. Left plot corresponds to 50% chance of data-losses at the controller-to-actuator channel. Right plot corresponds to 60% chance of data-losses at sensor-to-controller channel.

Fig. 8. Percentage of the expectation of overshoot, shown in a heat-plot, as a function of the probability of data losses occurring in the c-a channel and the sampling period. On top, the probability of data losses as a function of the sampling period is plotted, which is obtained from Fig. 1.

Fig. 8 we are able to identify which sampling period is to be chosen to achieve the largest performance (expressed in terms of smallest overshoot here). This demonstrates how our tools can be used effectively in the determination of the sampling period, even though data losses occur. A traditional design in this case would choose a sampling period conservatively to avoid data losses which would correspond to a sampling period of 1.6 [ms] just to be able to apply classical LTI design techniques. Clearly in terms of percentage of overshoot this is not the optimal choice and by using our new methodology, which is still based on LTI analysis techniques, much better designs and selection of the sampling period can be obtained.

V. INDUSTRIAL CASE-STUDY

ASML Holding N.V. [29] is the world leading manufacturers of photolithography systems for the semiconductor industry. These machines have extremely high requirements regarding accuracy and throughput. Fig. 9 shows the schematics of the system and its main components.

One of the critical components of the system is the wafer-stage, a platform, which transports a silicon wafer in the system during exposure. The waferstage consists of the long
stroke and the short stroke. While the long stroke has a positioning accuracy of micrometers, the short stroke has a positioning accuracy of nanometers, which is required for the photolithography process. Both the long and the short stroke have six degrees of freedom - the position along the three spatial axis, which we denote by $x$, $y$, $z$ and 3 rotation angles around each axis, which we denote by $R_x$, $R_y$, $R_z$, and are controlled by multiple processors. The processors communicate with multiple IO boards, which are connected to a number of sensors and actuators.

Fig. 10 illustrates a control application and the mapping on a multi-processor execution platform. The control application consists of a number of tasks, which are scheduled on the processors. The task schedule is divided into two sets of tasks: i) critical tasks that have to be executed before the specified IO delay, and ii) non-critical tasks that perform preparatory work for the next sampling period. The IO delay as well as the sampling period of the system are specified as $\tau = h = 50$ [µs], i.e., control loops run at 20 [kHz].

The system uses a static-order task scheduler and the task scheduling is computed when the system is initialized. Therefore schedules are always fully executed and tasks in these schedule cannot be aborted. As a result, the task schedule of the next period can be influenced by the previous period if deadlines were not met, i.e., tasks had a longer execution time than expected. This behavior coincides, assuming that only 1 sample lag is possible, with the behavior described by scenario 2 in section II-A.

Because ASML is able to derive a probability distribution for the completion time of the task schedule we are able to use our presented methods and investigate how deadline misses affect the ASML system. For our industrial case-study we will focus on the short stroke of the waferstage with data losses in the c-a channel.

ASML has several performance criteria for their control systems, including overshoot and settling-time in the time-domain and gain-margin, phase-margin and modules margin in the frequency-domain [26, p. 151, 279]. Besides these common performance criteria, ASML also uses the moving average error (MA) as an important performance criterion. This is defined by $MA_k := \sum_{i=0}^{N-1} w_i e_{k-i}$, where $N$ is the window size, $w_i$ is the weight associated with the error $e_{k-i}$ at discrete time $k \in \mathbb{N}$ and $i \in \{0,1,\ldots,N-1\}$. The MA is only calculated during the photolithography process, e.g., during the exposure of a die. In this time span the error must be in the nanometer range. The short stroke performs repeated motions trajectories over the wafer. Fig. 11 shows the repeated motion trajectories of the short stroke and the window for the settling-time, the window in which the exposure of a die takes place and the window for which the calculated MA should be small, meaning that the MA is computed continuously, although its values only have importance in this window. By formulating the MJLS (8) from the reference to the error we are able to compute the expected value of the error. Because the MA filter is linear we are able to compute the expected moving average error, that is, $E[MA_k] = E[\sum_{i=0}^{N-1} w_i e_{k-i}] = \sum_{i=0}^{N-1} w_i E[e_{k-i}]$. The short stroke is modeled by a MIMO state-space system, which has 93 states and the controller has 82 states. Both have 6 inputs and 6 outputs. The linear controllers where designed based on loop-shaping techniques to meet the desired specifications. The frequency response of the open-loop and sensitivity transfer functions from the first input to the first output pertaining to the control of the $x$-axis are depicted in Figs. 12a and 12b, respectively. The requirements for the sensitivity frequency response are also depicted in Fig. 12b.

Together with the 6 states required to model data losses in the c-a channel, this brings a total of 181 states of the MJLS resulting model. The system, which computes the expected output (9), has the same number of states, while the model, which computes the variance of the output (11), has $181 \cdot 181 = 32761$ states. Some elements from the state matrix of the plant $A_p$ or the controller $A_c$ are very small. This caused numerical problems when computing $A$. As a result, we were not able to
compute the variance of the system. No numerical problems were observed when computing the expected output.

The time-domain simulation of the short stroke consists of two separate simulations: i) horizontal simulation in which only the \(x\), \(y\) and \(Rz\) axis have a setpoint and \(Rx\) and \(Ry\) are set to zero and ii) vertical simulation in which only the \(z\), \(Rx\) and \(Ry\) axis have a setpoint and \(x\), \(y\) and \(Rz\) are set to zero. The vertical simulation pertains to the case where the system has to compensate for small height differences of the wafer. The simulations are performed separately to assess the contributions to the overall error. This is necessary because the horizontal movements affect the vertical movements and vice versa. In the discussion below we will focus on the error caused by the horizontal displacement and only show the results of the \(x\)-axis for reasons of compactness.

Fig. 13a shows a simulation of the short stroke for the given trajectory along with the feedforward and the feedback controller but without any data losses. When comparing Figs. 13a and 13b, observe that data losses in the feedback and feedforward controller combined are far more severe than data losses from the feedback controller only. When we focus on the control system without the feedforward controller (Fig. 13b), we can notice that in the plot with 50\% data losses the mean from the simulations and likewise the moving average error coincide with the analytically calculated mean and the analytically calculated moving average. The same results were observed when we had 100\% data loss, i.e., when the system, without feedforward, lags one sample behind every period. We also investigated the behavior of the system when applying scenario 1, instead of scenario 2, in which case the system behaves very similarly for 50\% data losses. Even at 80\% data loss the system behaves similarly. However, at approximately 85\% data loss the system, exhibiting the behavior of scenario 1, becomes unstable.

From the results we conclude that the performance of the short stroke is highly affected by data losses when they occur...
in the feedforward path. This was also verified by performing simulations in which only the feedback controller was affected by data losses and the feedforward was not. In fact, for both scenario 1 and 2 with 50% data losses in the feedback controller the behavior is very similar to that of the system without any data losses. Hence, the responses are hardly influenced by up to 50% data loss in the feedback path and no data losses in feedforward path. This may also lead to an approach on how to cope with deadline misses that causes data losses. Assuming that the feedforward is computed before the feedback, it would be possible to send the new feedforward with the old feedback to the actuator. When the deadline of the control tasks, which compute the feedback control, are met the data will be overwritten by the new feedforward combined with the new feedback. If the deadline is missed, the IO board still has a control signal (using the pre-computed feedforward value), which gives better performance than using merely the old control signal. In addition, because data losses hardly affect the feedback controller, it may be beneficial for ASML to do research in multi-rate control in which the feedback controller has a lower sampling frequency as opposed to the feedforward controller. This reduces the number of computations, which have to be carried out by the real-time platform, which would lead to less deadline misses and a cost reduction since fewer processors are needed.

In this section we showed how our proposed methods apply to an industrial case-study and how valuable information could be obtained. For instance, we were able to show that data losses with respect to the feedforward controller are far more critical to obtain nanometer precision than data losses with respect to the feedback controller.

VI. CONCLUSION

In this paper we have presented an analysis and design framework for real-time control systems subject to data losses. The framework consists of i) two basic models, to capture data losses as a consequence of deadline misses in a real-time control system, and ii) analysis techniques, which are used to analytically compute the mean and the variance of responses in the time-domain of systems that are subject to data losses. We have demonstrated the usefulness of our methods on an experimental case-study in which we performed both simulations and experiments. Furthermore, we applied them to an industrial case-study in which we have determined that data losses in the feedback controller are more severe than in the feedback controller. In the industrial case-study we proposed two possible solutions to cope with deadline misses that are identified as highly favorable.

In the future we want to extend our methods to suit more general models. These include models for which Assumption 1 does not necessarily hold, models with delays (see, e.g., [31]–[33]), multi-rate sampling ([31], [34]), general nonlinear systems based on fuzzy dynamic models [35], and time-varying sampling periods ([36]).

REFERENCES


[26] W. Geelen was born in Weert, Netherlands in 1989. He received his Bachelor degree in the field of Mechatronics from Fontys University of Applied Sciences in Venlo (Netherlands) and his Master degree in the field of Systems & Control at the Eindhoven University of Technology in Eindhoven (Netherlands). Currently he is a mechatronics consultant at Nobleo Technology in Eindhoven and working at ASML in Veldhoven within the Waferstage control group. He is interested in real-time digital control systems, the combination of embedded systems and control theory.

[27] D. Antunes (M’13) was born in Viseu, Portugal, in 1982. He received the Licenciatura in Electrical and Computer Engineering from the Instituto Superior Técnico (IST), Lisbon, in 2005. He did his PhD from 2006 to 2011 in the research field of Automatic Control at the Institute for Systems and Robotics, IST, Lisbon. From 2011 to 2013 he held a postdoctoral position at the Eindhoven University of Technology (TU/e). He is currently an Assistant Professor at the Department of Mechanical Engineering of TU/e. His research interests include Networked Control Systems, Stochastic Control, Dynamic Programming, and Systems Biology.

[28] J.P.M. Voeten received his master’s degree in Mathematics and Computing Science and his Ph.D. in Electrical Engineering from the Eindhoven University of Technology, the Netherlands. He is a senior scientist at TNO and an associate professor in the Electronic Systems group at the faculty of Electrical Engineering. His research interests include system-level design, model-driven engineering and performance modeling for Cyber Physical Systems.
R. R. H. Schiffelers received the MSc and PhD degrees from Eindhoven University of Technology. His PhD project resulted in the hybrid process algebra Chi and accompanying tools. As a post-doctoral researcher, he dealt with modeling, analysis and synthesis of supervisory controllers for Philips MRI scanners and participated in European projects dealing with the design of the Compositional Interchange Format for hybrid systems (CIF). In 2010, he joined ASML, world’s leading provider of lithography systems for the semiconductor industry. As software innovation architect, he initiates, defines and supervises several (multi-disciplinary) research projects, mainly in the area of model-driven (software) engineering, executed by PhD, PDEng and MSc students. Since 2012 he also holds a position as assistant professor in de Model Driven Software Engineering group at the faculty of Mathematics and Computer Science at the Eindhoven University of Technology.

W. P. M. H. Heemels (SM’10) received the M.Sc. degree in mathematics and the Ph.D. degree in control theory (both summa cum laude) from the Eindhoven University of Technology (TU/e), Eindhoven, The Netherlands, in 1995 and 1999, respectively. After being an Assistant Professor at the EE dept at TU/e and a research fellow at the Embedded Systems Institute (ESI), he is currently a Full Professor in the Control Systems Technology Group at the ME department at TU/e. Maurice held visiting research positions at the Swiss Federal Institute of Technology (ETH), Zurich, Switzerland (2001), at Océ, Venlo, the Netherlands (2004) and at the University of California at Santa Barbara, USA (2008). Dr. Heemels is an Associate Editor for the journals Nonlinear Analysis: Hybrid Systems and Automatica. He was the recipient of a prestigious VICI grant of the Dutch Technology Foundation (STW) and the Netherlands Organisation for Scientific Research (NWO). In addition, he served as the general chair of the 4th IFAC Conference on Analysis and Design of Hybrid Systems (ADHS) 2012 in Eindhoven, The Netherlands, and was the IPC chair for the 4th IFAC Workshop on Distributed Estimation and Control in Networked Systems (NECSYS) 2013 in Koblenz, Germany. His current research interests include general system and control theory, hybrid and cyber-physical systems, networked and event-triggered control, and constrained systems including model predictive control.