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Design and Results of a New Interference Refractometer Based on a Commercially Available Laser Interferometer

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A new type of interference refractometers, based on a commercially available laser interferometer, has been developed. The design and behaviour of this refractometer is presented in this paper. A review of measurements on stability, absolute measuring accuracy and a comparison with calculated values of the refractive index of air will be given. The maximum uncertainty has been evaluated as 5 parts in \( 10^{-9} \).

This refractometer can be very useful for the accurate determination of the refractive index of air and other gases and also for the calibration of automatic compensators of commercially available laser interferometers.

1. INTRODUCTION.

Laser interferometry has been used for many years as a useful tool for the accurate measurement of length, angle and straightness. Today laser interferometers are the basic instruments for the calibration of coordinate measuring machines and other accurate length measuring instruments. There is also a growing need for the very accurate determination of errors in scales, straightness and squareness of coordinate measuring machines, because these data are now used for software error correction in these instruments.

Laser interferometers are also used as measuring systems in very accurate production- and measuring machines. When using interferometry the measured length \( L \) is generally calculated from

\[
L = \frac{n \lambda}{m}
\]

where \( n \) is the number of pulses counted, \( \lambda \) the vacuum wavelength of the laser source, \( m \) the refractive index of air and, \( p \) a numerical factor usually two or four, depending on the optical and electronic properties of the instrument.

The relative uncertainty of \( L \) can be calculated from Eq. (1):

\[
\frac{\Delta L}{L} = \frac{\Delta n}{n} + \frac{\Delta \lambda}{\lambda} + \frac{\Delta m}{m}
\]

Earlier in these Annals we have published information about the determination of the accuracy of \( n \) and \( \lambda \) [1,2]. It may be concluded from that information and Eq. (2) that the relative accuracy of \( L \) is limited by the accuracy \( \frac{\Delta n}{n} \). Today for the most accurate measurements \( \Delta \lambda \) \( 10^{-7} \) is demanded which means that at least the same accuracy for \( n \) is required. For commercially available laser interferometers \( \frac{\Delta n}{n} \) has to be calculated from the measured values of pressure, temperature and humidity using Edlens equation [3]. Somewhat modified in the air this equation can be written as:

\[
N - 1 = 0.006 \times 10^{-6} + 2 \times 10^{-10} \times T - 0.42963 \times 10^{-3} \times F
\]

where \( N \) is the number of counts due to the changing optical path length for the sample-chamber, \( T \) the air temperature in \( ^\circ C \), \( F \) the vapour pressure in Pa and, \( C \) the \( CO_2 \) content in ppm.

Commercially available laser interferometers with electronic correction for changes in \( N \), so called automatic compensation, use a constant value for \( C \), normally 300 ppm. From Eq. (3) the influence of errors can be calculated. For sake of completeness they are given in Eq. (4):

\[
\begin{align*}
\Delta N & = 2.67 \times 10^{-3} \text{ Pa}^{-1} \\
\Delta T & = -9.20 \times 10^{-7} \text{ K}^{-1} \\
\Delta F & = -4.21 \times 10^{-10} \text{ Pa}^{-1} \\
\Delta C & = 1.45 \times 10^{-10} \text{ ppm}^{-1}
\end{align*}
\]

Since the model-accuracy of Edlens equation has been claimed to be \( 5 \times 10^{-9} \) [3], it will be very difficult to reach the \( 10^{-7} \) level for \( \Delta \lambda \) due to errors in the determination of \( P \), \( T \), \( F \) and \( C \). To get a more accurate measurement of \( N \) interference refractometers have been built in recent years [4,5,6]. By these refractometers the refractive index including the contribution of all constituents in the air is measured. As can be expected this method gives better results than the Edlens-method. This has been confirmed by an international project on the comparison of interference refractometers. In this project, supported by BCR-ECC, Brussels, four refractometers developed in different countries are compared. The measured values of \( N \) are also compared with calculated values using Edlens equation. The complete results are published now [6].

The Dutch participants in this project have decided to redesign their refractometers and to build improved instruments based on the same concept: using commercially available laser interferometers. Two refractometers have been built based on the same principle but using different lasersources and counting systems [7] of a well known manufacturer. It should be noted that these refractometers can be used also with other lasersources and counting systems.

We have compared these refractometers and, separate, calculated \( N \) from Eq. (3). In this way we could also determine the differences between measured and calculated values of \( N \). Finally, the results of the calibration of automatic compensators of laser interferometers performed with this refractometer are given.

2. DESIGN OF THE INTERFERENCE REFRACTOMETER.

The refractometer has been based on a symmetric double-beam interferometer. One of the beams is passing through a sample-chamber which can be filled with the medium to be measured, normally air. The other beam is passing a vacuum chamber as a reference.

Vacuum and air chambers are drilled in an aluminium block, sizes 70 x 70 x 600 mm. The chambers are closed by optical windows. Connections for filling and pumping out the chambers are provided on the aluminium block. Two sensors for temperature measurement are mounted in the sample-chamber. The optics for beam-splitting, beam-bending and reflection are mounted separately on a common base together with the aluminium block and the laser source. These optics are not standard components of the laser interferometer used, but are available commercially.

The principle of the refractometer is shown schematically in Fig. 1. The quarter-wave plate is only necessary if a polarizing beamsplitting prism is used as is the case in our interferometers. It should be noted that the prisms for beamsplitting, beambending and also the laser source can be fine adjusted to optimise the interference signal for the counting system.

The method of measurement is very simple: first the chambers are evacuated to a sufficient low pressure, after which the medium - air - is admitted slowly into the sample-chamber through a filling station. The changing optical path has been measured by the interferometer during the filling period, normally a few minutes.

It can easily be proved that in the case of constant optical paths outside the aluminium block the refractive index can be calculated from:

\[
N - 1 = \frac{k \lambda c}{m}
\]

where \( k \) is the number of counts due to the changing optical path in the sample-chamber, \( p \) a numerical factor, and \( c \) the actual length of the sample-chamber.
FIG. 1: PRINCIPLES OF THE REFRACTOMETER.


By electronic extension provided with laser-source type A [7] a value $p = 400$ has been reached while for type B [7] a value of $p = 600$ has been used, using the build-in computer in connection with the straightness-measurement mode.

To ascertain that the air in the sample-chamber has the same humidity content as the air in an isolated volume, next called the sample-volume, the air has been circulated smoothly (1 l min$^{-1}$) from this volume through the sample-chamber. In the sample-volume we have measured also pressure, temperature and humidity. Daily we took several air samples for determination of the $\mathrm{CO}_2$ content and other constituents by gaschromatographic techniques. For the pressure measurement a Portin-type mercury barometer and a meteobarometer have been used. Temperature measurement in the sample-chamber, on the aluminium block and in the sample-volume are carried out by resistance thermometers. The thermometers, the Pt-100 type, are coupled to a measuring set-up according to Dauphinee [6]. In this set-up the resistance of the thermometers has been compared with a standard using a Diekelhorst-compensator with null-detection. Most of the humidity measurements were carried out by measuring the dewpoint temperature $T_d$ and from these results the vapour pressure was calculated from Eq. (6):

$$F = 611 \times \exp \left(72.5 \times 10^{-3}T_d - 237.3 \times 10^{-6}T_d^2 + 0.79 \times 10^{-9}T_d^3 \right)$$

where $T_d$ is the dewpoint temperature in $^\circ\mathrm{C}$, and $F$ the vapour pressure in Pa.

A wet and dry bulb psychrometer has been used also for comparison.

The actual length $L_0$ of the sample-chamber can be calculated from $L_0 = \frac{L_1}{(1 + \alpha(T_0 - T))}$. Here, $\alpha$ is the linear coefficient of expansion of aluminium, $L_1$ the length of the chamber at $T_0$ and $T$ the temperature of the aluminium block. The resolution of the type A refractometer has been calculated to be 4 parts in $10^9$ and for type B 2 parts in $10^9$. The refractometers are connected to filling and pumping stations coupled by valves. Connections were made by thick-walled flexible PVC tubes. Vacuum measurement was carried out by a Pirani-gauge.

The refractometers and optics are situated in a Polystyrene-cabinet in order to avoid temperature gradients in the refractometers. Fig. 2 shows a diagram of the complete refractometer set-up for the comparison of the measured and calculated values of $N$.

3. MEASUREMENTS AND RESULTS.


Before the refractive index measurements have been started the stability of the refractometers was studied. For this measurement both chambers have been evacuated and after equilibrium the change in optical path has been measured by the interferometer over periods of several hours. Both refractometers have shown nearly the same behaviour: a drift in $N$ of a few parts in $10^8$. Fig. 3 shows a sample graph of the drift.
After evacuation a single measurement of \( N \) takes about 5 minutes so in that case the drift is negligible. Continuous measurement of \( N \), without intermediate evacuation of the sample cell, over longer periods, needs small correction for the most accurate measurements.

3.2. Comparison of values measured by the refractometer, with calculated values of \( N \).

In this set-up both refractometers were connected to the sample-volume. From this volume air was admitted to both sample-chambers by separate filling stations. During the measurements the air was circulated through both sample-chambers. Temperature was measured in the sample-chambers and in the sample-volume to correct the measured values of \( N \) for temperature difference between these places.

In the sample-volume also pressure, humidity and \( \text{CO}_2 \)-content have been measured. From these results values of \( N \) have been calculated. Fig. 4 shows graphically some results for both refractometers. Several measurements have shown a slight tendency for the measurements of \( N \) to be higher than the calculated values as we have found also in the international comparison mentioned earlier. To confirm this, it will be necessary to improve our measurements of \( P, T \) and \( F \).

3.3. Direct comparison of the refractometers.

For these measurements both refractometers have been connected to one filling and pumping system. In this way the vacuum and air conditions were the same for both instruments. After evacuation air from the sample-volume has been admitted into both sample-chambers. Also a slight circulation of air through both chambers was accomplished. Air temperature in both sample-chambers has been measured to correct for temperature differences. Fig. 5 shows the complete set-up for the comparison of the refractometers. In this case the insulated cabinets around the refractometers are removed.

3.4. Role of \( \text{CO}_2 \)-content and other constituents.

For the most accurate measurements with laserinterferometers one has to measure the \( \text{CO}_2 \)-content of the air and generally to correct for it [6]. To get a good idea about the situation in our laboratory the air has been analysed over longer periods by gaschromatography. Every day showed the same tendency: a starting value around 350 ppm and thereafter an increasing \( \text{CO}_2 \)-content reaching a level between 700 and 950 ppm at the end of the day depending on the number of people in the 400 m\(^3\) volume of the laboratory.
The interference refractometers described can be used also for the determination of the refractive index of other gases at atmospheric pressure. After correction for the temperature-difference between measured values and sample-chamber the measured values of N have been compared. The relative difference is below 3 parts in $10^{-7}$ mainly due to measurement errors of the sensors of the automatic compensators. The relative differences are below 3 parts in $10^{-7}$ mainly due to measurement errors of the sensors of the automatic compensators.

It may be concluded that in the car manufacturing plant situation only the carbon dioxide concentration has a significant influence on the measuring accuracy.

4. ADDITIONAL APPLICATIONS.

The interference refractometers described can be used also for the determination of the refractive index of other gases at atmospheric pressure. After correction for the temperature-difference between measured values and sample-chamber the measured values of N have been compared. The relative difference is below 3 parts in $10^{-7}$ mainly due to measurement errors of the sensors of the automatic compensators. The relative differences are below 3 parts in $10^{-7}$ mainly due to measurement errors of the sensors of the automatic compensators. The manufacturer claims a maximum uncertainty of 5 parts in $10^{-7}$.

5. DISCUSSION.

The interference refractometers described here have shown a stability better than 5 parts in $10^{-7}$ over several hours. At least a part of this drift can be explained from small temperature-effects on the mechanical structure for the adjustment of the optics. Direct comparison showed also relative differences less than 5 parts in $10^{-7}$. Part of these differences are due to small errors in the temperature-measurement in the sample-chambers. The relative difference in this measurement was less than 0.02 K which causes maximum relative errors of $N = 2.10^{-8}$. Also small effect have been measured from local expansion of the optical windows arising from the vacuum-air change in the sample-chamber. These effects are evaluated now.

Comparison between measured and calculated values of N, as was shown in Fig. 4, indicating relative differences up to 8 part in $10^{-7}$. Part of these differences can be explained from the uncertainty in the calculated value of N. The uncertainty of the maximum uncertainty has been determined to be at least 15 Pa and the uncertainty in the dewpoint measurement will be 0.3 K. The carbon dioxide content has been calculated from interpolation between measured values. The maximum uncertainty will be less than 50 ppm. From these values and the model uncertainty of ± 5 parts in $10^{-7}$ the total uncertainty in the calculated values of N will be ± 7 parts in $10^{-7}$. The results showed in Fig. 4 are within this range.

6. CONCLUSIONS.

It may be stated that the interference refractometers developed are very useful instruments for the accurate determination of the refractive index of air and for the calibration of automatic compensators in laser interferometers. Relative uncertainty will be less than 5 parts in $10^{-7}$ even when...
the instruments are used continuously for periods of several hours. The instruments can be build relatively easy because they are based on commercially available laserinterferometers. For some types it is even possible to use the refractometer parallel to the interferometer using the same laser source [9].

It has been proved that the CO₂-content plays an important role in accurate interferometric measurements and generally it is not allowed to use the standard value of 300 ppm for calculating W values. Especially in industrial environments the CO₂-content can be very high but also the butane and octane content can be important [5].

We have measured a relation between the number of people and the CO₂-content in our laboratory. The air in this laboratory is conditioned by closed circuit. Generally it can be stated that for interferometric length measurements with relative uncertainty less than 1 part in 10^7 the refractive index has to be measured by an air-refractometer. 7. ACKNOWLEDGMENTS

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[7] Two laserinterferometers manufactured by Hewlett-Packard have been used:
Refractometer A: laser 5500C + 5505A display + resolution extender 59995A
Refractometer B: laser 5518A + 5508A display. The automatic compensators calibrated are also manufactured by H-P both belonging to the A-type laserinterferometer.

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