Nanomechanical control of optical field and quality factor in photonic crystal structures

Citation for published version (APA):

DOI:
10.1103/PhysRevB.97.115304

Document status and date:
Published: 08/03/2018

Document Version:
Accepted manuscript including changes made at the peer-review stage

Please check the document version of this publication:
• A submitted manuscript is the version of the article upon submission and before peer-review. There can be important differences between the submitted version and the official published version of record. People interested in the research are advised to contact the author for the final version of the publication, or visit the DOI to the publisher’s website.
• The final author version and the galley proof are versions of the publication after peer review.
• The final published version features the final layout of the paper including the volume, issue and page numbers.

Link to publication

General rights
Copyright and moral rights for the publications made accessible in the public portal are retained by the authors and/or other copyright owners and it is a condition of accessing publications that users recognise and abide by the legal requirements associated with these rights.

• Users may download and print one copy of any publication from the public portal for the purpose of private study or research.
• You may not further distribute the material or use it for any profit-making activity or commercial gain
• You may freely distribute the URL identifying the publication in the public portal.

If the publication is distributed under the terms of Article 25fa of the Dutch Copyright Act, indicated by the “Taverne” license above, please follow below link for the End User Agreement:
www.tue.nl/taverne

Take down policy
If you believe that this document breaches copyright please contact us at:
openaccess@tue.nl
providing details and we will investigate your claim.
Nanomechanical control of the optical field and the quality factor in photonic crystal structures

Michele Cotrufo,1,* Leonardo Midolo,1,2 Žarko Zobenica,1 Maurangelo Petruzzella,1 Frank W. M. van Otten,1 and Andrea Fiore1

1Department of Applied Physics, Eindhoven University of Technology, P.O. Box 513, 5600MB Eindhoven, The Netherlands.
2Niels Bohr Institute, University of Copenhagen, Blegdamsvej 17, DK-2100 Copenhagen, Denmark.

(Dated: February 20, 2018)

Abstract

Actively controlling the properties of localized optical modes is crucial for cavity quantum electrodynamics experiments. While several methods to tune the optical frequency have been demonstrated, the possibility of controlling the shape of the modes has been scarcely investigated. Yet, an active manipulation of the mode pattern would allow a direct control of the mode volume and the quality factor, and therefore of the radiative processes. In this work, we propose and demonstrate a nano-opto-electro-mechanical device in which a mechanical displacement affects the spatial pattern of the electromagnetic field. The device is based on a double-membrane photonic crystal waveguide which, upon bending, creates a spatial modulation of the effective refractive index, resulting in an effective potential well or anti-well for the optical modes. The change of the field pattern drastically affects the optical losses: large modulations of the quality factors and dissipative coupling rates larger than 1 GHz/nm are predicted by calculations and confirmed by experiments. This concept opens new avenues in solid-state cavity quantum-electrodynamics where the field, instead of the frequency, is coupled to the mechanical motion.
I. INTRODUCTION

The active manipulation of localized optical modes lies at the heart of many groundbreaking experiments in cavity quantum-electrodynamics and studies of light-matter interaction, in particular because it allows an on-demand control of the atom-photon interaction. So far, most of the efforts have been devoted to the tuning of the optical frequency, in order to change the spectral overlap between the mode and a quantum emitter.\textsuperscript{1,2} Several tuning methods, mainly based on changing the refractive index of the material surrounding the cavity,\textsuperscript{3–8} have been proposed. Additionally, frequency tuning can be obtained by a mechanical perturbation of the cavity structure itself, realized by, \textit{e.g.}, approaching and perturbing the optical near field by an external object, such as a tip,\textsuperscript{9,10} or changing the distance between different parts of the cavity. In this regard, micro- and nano-opto-electro-mechanical systems (NOEMS) have often been used as a reliable solution to implement spectral control on devices such as vertical cavity surface emitting lasers\textsuperscript{11} and photonic crystal (PhC) cavities.\textsuperscript{12–18}

In all the approaches mentioned above the perturbation leads to a change of the optical frequency, while the spatial distribution of the field is only weakly altered. The opposite effect, \textit{i.e.}, the possibility of altering the spatial pattern of a cavity mode, has been recently considered in a few studies,\textsuperscript{19–22} including the demonstration of on-demand PhC cavity creation,\textsuperscript{23} and is quite attractive in various contexts. Indeed, the amplitude of the mode field at an emitter’s position directly determines the emitter-field coupling rate, and affects radiative processes such as spontaneous emission, Rabi oscillations and optical gain. Moreover, modifications of the field profile can lead to a change of the optical mode volume and the quality (Q) factor, which also determine the strength of the light-matter interaction. If the perturbation is implemented mechanically, the resulting mechanical control of the optical losses can have important applications in the context of Q-switched lasers\textsuperscript{24} and dissipative optomechanics.\textsuperscript{25} In the latter, the change of the optical loss rate ($\kappa$) is usually quantified through the dissipative coupling rate $g_\kappa \equiv \partial \kappa / \partial x$, where $x$ parametrizes the mechanical displacement. Previous approaches for the mechanical control of the optical loss have mainly relied on altering the external losses by controlling the distance between the cavity and an external reservoir,\textsuperscript{26–29} and/or altering the internal losses by displacing small parts of the cavity.\textsuperscript{27,29–33} In electromechanical implementations, modest variations of the Q
factors (∆Q/Q < 1), corresponding to |gκ|/2π = 20 – 200 MHz/nm, have been obtained so far.26,31

In this work, we propose and experimentally demonstrate a new concept to control the spatial pattern of a localized optical mode by a mechanical perturbation. The device is composed of two coupled PhC waveguides (PhCWG) embedded in GaAs slabs (fig. 1a) and separated by a small air gap. A bending of the membranes (fig. 1d) creates a local modulation of the effective refractive index, which in turn controls the mode localization. In particular, an effective potential well or anti-well can be realized in our system, according to the symmetries of the modes considered. As a consequence, the optical fields get strongly localized either at the center or at the edges of the structure. The changes of the field profiles are very pronounced: for the case of the anti-well potential a mechanical displacement smaller than 10 nm is sufficient to completely reshape the pattern of the fundamental mode, so that the center of the waveguide evolves from being a point of maximum to a point of minimum of the field. Importantly, varying the field profile alters the coupling to leaky modes at the PhCWG edges significantly, resulting in a modulation of the optical losses. Our numerical calculations predict variations of the optical losses of more than two orders of magnitude, and dissipative coupling rates in the range |gκ|/2π = 1 – 5 GHz/nm. Experimentally, we are able to measure dissipative coupling rates comparable or even larger than the calculated ones, and to modulate the loss rate by more than a factor of five, only limited by the maximum Q factors and bending achievable in our current implementations. Besides, this work demonstrates for the first time how the spatial shape of localized optical fields can be controlled by displacing an integrated on-chip mechanical object. The concept is not limited to the proposed implementation, and it can be readily extended to any optical device in which the effective refractive index depends on a mechanical displacement. While here we mainly investigate the consequences on the optical losses, this novel effect is more general, and it paves the way to a large class of new phenomena in which the emitter-cavity coupling is controlled by the field amplitude rather than a spectral detuning, allowing new applications such as gain-modulated lasers and emitter-phonon coherent coupling.22
FIG. 1. **Field and quality factor control in double-membrane NOEMS.** (a) Schematic of the double membrane structure, with a sketch of the symmetric (blue line) and antisymmetric (red line) field profiles. (b) Dispersion curves of the fundamental guided modes of a single-membrane PhCWG (green line) and of a double-membrane PhCWG, for the symmetric (blue line) and the antisymmetric (red line) mode. (c) In-plane field profiles (y-component of the electric field) of the first three localized modes in a single-membrane PhCWG. (d) Sketch of the working principle of the device: when the membranes are bent towards each other, the S modes (only the first one is shown here) localize at the center of the waveguide. (e-f) SEM micrographs of a fabricated device. (g) Calculated downward displacement of the top membrane of the device shown in panel (e) under a voltage of 4 V applied between the membranes. The green dashed line indicates the position and the orientation of the PhC waveguide. (h) Distance between the two membranes along the waveguide direction for the maximum bending achievable in the real device (green curve, cut from panel g along the green dashed line) and for the case in which the edges are clamped (blue line), as in panel d.

**RESULTS**

**Device concept**

The device is schematically depicted in fig. 1a. It is composed of two parallel GaAs membranes containing two identical PhCWGs. The membrane thicknesses are 170 nm, the gap between the membranes is \( z_0 = 200 \) nm, the lattice constant of the PhC is \( a = 370 \) nm and the filling factor of the holes is 0.35. The hybridization of the fundamental guided modes
of the two isolated PhCWGs leads to the formation of two coupled guided modes, with a symmetric (S) and an antisymmetric (AS) vertical distribution of the y-component of the electric field (fig. 1a, blue and red line respectively). The dispersion curves of the S and AS guided modes (blue and red line, respectively, in fig. 1b) are spectrally shifted with respect to the dispersion curve of the fundamental guided mode of the single PhCWG (fig. 1b, green line). The propagation of guided modes in coupled waveguides can be described in terms of effective refractive indices (ERIs) \( \tilde{n}_i \) \( (i = S, AS) \) that depend on the materials, the membrane thicknesses and the intermembrane gap.\(^{35,36} \) In our structure, when the gap decreases \( \tilde{n}_S \) increases, while \( \tilde{n}_{AS} \) decreases [see Supplemental Material (SM)\(^{37} \)]. We now consider the double-membrane PhCWG to be abruptly terminated: if the membranes are parallel (fig. 1a), \( \tilde{n}_i \) is uniform along the waveguide and the structure can be described as a Fabry-Perot cavity with weakly reflecting mirrors at the waveguide ends, caused by the large group-index mismatch. This gives rise, for both the S and the AS guided modes, to a discrete set of localized modes in the slow-light region (\( i.e., \, ka/2\pi \approx 0.5 \), see fig. 1b). The in-plane electric fields of the localized modes stem from the Bloch mode of the infinite waveguide, modulated by slowly-varying envelopes (fig. 1c). We now consider the situation in which the membranes are bent in such a way that the intermembrane gap changes along the waveguide direction (\( e.g., \) fig. 1d). If the maximum bending is much smaller than the membrane’s length, we can describe the structure as a waveguide with a gentle spatial modulation of the ERIs. In particular, for a bending small with respect to the initial distance, the ERI depends exponentially on the local value of the air gap,\(^{38} \) and can be described by the formula

\[
\tilde{n}_i(x, \Delta z) = \tilde{n}_\infty + (\tilde{n}_{i,z_0} - \tilde{n}_\infty) \exp \left[ \gamma \Delta z (x) \right],
\]

where \( \tilde{n}_\infty \) and \( \tilde{n}_{i,z_0} \) \( (i = S, AS) \) are the ERI of the single slab waveguide and the ones of a double slab waveguide with constant gap \( z_0 \), respectively, \( \gamma \equiv (\omega/c) \sqrt{\tilde{n}_\infty^2 - 1} \) is the spatial decay rate of the single-slab electric field along the z-direction, \( \omega \) is the angular optical frequency and \( c \) is the speed of light in vacuum. \( \Delta z \) denotes the maximum variation of the gap (see fig. 1d) and the function \( \xi(x) \), normalized such that \( \max(\xi)=1 \), describes the bending of the membranes along the x-direction.\(^{37} \) The distance between the two slabs in each point is then given by \( z_0 - \Delta z \xi(x) \). For the structure considered here, the ERI of the S modes is larger than the one of the single-slab mode (\( \tilde{n}_{S,z_0} > \tilde{n}_\infty \)), as shown in fig. S4 of the SM.\(^{37} \) Therefore, when the deformation function \( \xi(x) \) has a local maximum (\( i.e., \) where the
two slabs are closer), the ERI of the S modes becomes higher in that region compared to its surroundings, promoting the localization of light. Conversely, $\tilde{n}_{AS,z_0} < \tilde{n}_\infty$, and therefore the ERI of the AS modes is lowered in the local maxima of $\xi(x)$, resulting in an anti-well which "pushes away" the AS modes. Thus, for a quasi-parabolic bending profile, as the one shown in fig. 1d (obtainable by applying an uniform force between the two clamped membranes), a strong localization of the S modes at the center of the waveguide is expected, while the AS modes will be pushed towards the waveguide’s edges. Moreover, as the optical losses of these modes are mainly due to the in-plane leakages at the waveguide-bulk interfaces, such variations of the field intensity at the waveguide edges is expected to strongly increase (decrease) the Q factor of the S (AS) modes.

More useful insights into the behaviour of the optical modes of this device can be obtained within the effective refractive index approximation and by utilizing a 1D envelope-function model. The device is here described as a 2D PhCWG made of air holes embedded in a material with a refractive index given by eq. 1. The effect of the mechanical deformation can therefore be described by a perturbation of the periodic dielectric function, $\epsilon(r)$, such that $\tilde{\epsilon}(r) = \Delta_i(x)\epsilon(r)$ is the new dielectric function and $\Delta_i(x) \equiv \tilde{n}_i^2(x, \Delta z)/\tilde{n}_i^{2,z_0} (i=S,AS)$, where the explicit dependence of $\Delta_i$ on $\Delta z$ has been omitted for brevity. Moreover, in the following we omit the subscript $i$ from all the quantities, since all formulas apply separately to the S and AS modes. It can be shown that, for a generic slowly-varying perturbation $\Delta(x)$, the electric field of an unperturbed band-edge guided mode $E_{k_X}(r) = e^{ik_X x}u_{k_X}(r)$ is modified into $E_\alpha(r) = \Gamma_\alpha(x)e^{ik_X x}u_{k_X}(r)$, where $u_{k_X}(r)$ is the periodic part of the Bloch function at $k_X = \pi/a$, $\alpha$ is the frequency of the perturbed mode, and we have introduced an adimensional function $\Gamma_\alpha(x)$. This latter function describes the modulations of the electric field envelope due to the perturbation, and it satisfies the equation

$$\left[ -\frac{c^2}{2m^*} \frac{d^2}{dx^2} + \omega^2(k_X) \right] \Gamma_\alpha(x) = \alpha^2 \Delta(x) \Gamma_\alpha(x), \tag{2}$$

where $c$ is the speed of light, $\omega(k_X)$ is the band-edge frequency of the unperturbed guided mode, and we introduced the adimensional effective mass $(m^*)^{-1} \equiv \frac{1}{c^2} \frac{d^2\omega^2(k)}{dk^2} \bigg|_{k=k_X}$. The derivation of eq. 2, and the approximations involved, are discussed in the SM. Equation 2 is a generalized eigenvalue equation whose set of solutions provides the frequencies $\alpha$ and the field profiles $\Gamma_\alpha(x)$ of the modes created by the perturbation $\Delta(x)$. As shown in the SM, for our device the function $\Delta(x)$ has a quadratic behaviour near the center of the waveguide.
(x \approx 0). We can therefore expand \( \Delta(x) \approx \Delta_0 + \Delta_2 x^2 \). By substituting this expression in eq. 2 we obtain
\[
\left[ -\frac{c^2}{2\mu} \frac{d^2}{dx^2} + (\alpha^2 \Delta_2) x^2 \right] \Gamma_\alpha(x) = (\alpha^2 \Delta_0 - \omega^2(k_X)) \Gamma_\alpha(x).
\] (3)

which, depending on the sign of \( \Delta_2 \), is mathematically equivalent to the Schrödinger equation of a generalized (i.e., the potential energy \( V(x) = -\alpha^2 \Delta_2 x^2 \) depends on the ‘eigenenergy’ \( \alpha^2 \)) quantum harmonic or reversed oscillator. For the S modes, \( \Delta_2 \) is negative and it decreases with increasing membrane bending (see fig. S4b in Ref. [37]). Equation 3 describes therefore a generalized quantum harmonic oscillator,\(^{41,42}\) with an attractive potential energy at the center of waveguide that increases with bending. For the AS modes the term \( \Delta_2 \) is positive and it increases with increasing membrane bending. Equation 3 describes in this case a generalized quantum reversed oscillator, in which the modes feel a repulsive potential at the origin \( x = 0 \), and are therefore pushed towards larger values of \( |x| \).

**Numerical analysis**

While the analytical model discussed above provides a semi-quantitative description of the control of the optical fields in our device, its accuracy in predicting the field and loss modulations is hindered by the approximations involved, as discussed in details in the SM.\(^{37}\) We have therefore utilized full 3D finite-element-method (FEM) simulations\(^{43}\) to verify the magnitudes of the predicted effects. Figures 2(a-b) show the calculated (FEM) in-plane profiles of the electric field (y-component) of the first two S modes, for a PhCWG length of \( L_{WG} = 28a \approx 10.5 \mu m \) and a quasi-parabolic bending of the membranes (fig. 1d). The bending profile is calculated analytically by solving the Euler-Bernoulli beam equation for a doubly-clamped beam under uniform applied force.\(^{37}\) The bending is parametrized by the decrease \( \Delta z \) of the gap in the center of the waveguide. As expected from the previous discussion, the S modes get strongly localized at the waveguide’s center for increasing bending (figs. 2(a-b), from left to right), as a result of the local increase of the ERI (the field patterns for different displacements and for the other modes are shown in the SM\(^{37}\)). Figures 2(c-d) show, respectively, the frequencies and the loss rates of the first four S modes versus \( \Delta z \). The frequencies of all modes decrease (fig. 2c), due to the overall increase of the ERI. Moreover, the frequency spacings, initially strongly uneven, become uniform for large
FIG. 2. Numerical analysis of the field localization in bent double-membrane waveguides. $\Delta z$ denotes the variation of the distance between the centers of the two membranes. (a-b) In-plane field profiles (y-component) of the first two S modes for no bending (parallel membranes, $\Delta z = 0$ nm) and a moderate bending ($\Delta z = 30$ nm), as indicated on top of each sub-panel. The color scales of all plots are the same as in fig. 1c. (c) Frequencies of the first four S modes versus $\Delta z$. (d) Optical loss rates of the first four S modes versus $\Delta z$. Color legend is the same as in panel c. The vertical axis on the right shows the corresponding values of the Q factor, calculated for an average normalized frequency of 0.277. (e-h) Same as in panels (a-d), for the AS modes. The Q factor scale in panel h is calculated for an average normalized frequency of 0.2897. (i) Mode volume (V) (solid lines) and Q/V ratio (dashed lines) of the S modes for increasing bending. (j) Modulus square of the Fourier transform of the in-plane profile of the electric field (y-component) of the first S mode for $\Delta z = 0$ nm and $\Delta z = 60$ nm. The red circle denotes the light cone. (k) Modulus square of the Fourier transform of the in-plane electric field (sum of the $x$ and $y$ components) of the first S mode integrated over the light cone versus the displacement $\Delta z$. 

bending, as expected for the eigenmodes of a potential well, which can be approximated
locally by a harmonic oscillator. Importantly, the loss rates of all the S modes (fig. 2d) decrease very strongly (by more than two order of magnitudes for the first two modes), as a consequence of the reduced leakages at the waveguide edges. For $\Delta z > 30 \text{ nm}$ the losses of the first two modes saturate and start to increase. We attribute this behaviour to the fact that the strong spatial localization promotes the coupling to optical states inside the light cone, and therefore increases the out-of-plane losses. It is well known that the impact of the out-of-plane losses in PhC structures can be assessed from the intensity of the Fourier transform of the in-plane electric field within the light cone. Figure 2j shows the Fourier transform of the electric field ($y$-component) of the first S mode for two different displacements of the structure. The intensity of the Fourier transform inside the light cone increases sensitively for a large bending ($\Delta z = 60 \text{ nm}$, right panel) with respect to the unbent case ($\Delta z = 0$, left panel). In fig. 2k we plot the intensity of the total Fourier transform ($|E_x(k_x, k_y)|^2 + |E_y(k_x, k_y)|^2$) integrated inside the light cone as a function of the displacement $\Delta z$. A monotonic increase of the intensity, as the structure is progressively bent, is clearly evident, which confirms our hypothesis on the role of the out-of-plane losses in limiting the increase of the Q-factor.

Remarkably, we note that a moderate bending can provide localized modes with extremely high optical Q factors ($Q > 10^7$), comparable with the ones obtainable in PhC cavities where the position and/or radius of each hole is carefully optimized to maximize the Q. Moreover, the field localization of the S modes leads to a two-fold reduction of the mode volume $V$ (fig. 2i, left axis), which further increases the ratio $Q/V$, a typical figure of merit for cavity QED experiments and in particular for Purcell enhancement. As shown in fig. 2i (right axis), our structure can attain values of $Q/V$ up to $10^7(\lambda^3/n^3)^{-1}$, that are comparable to those theoretically predicted in properly optimized PhC cavities or hybrid plasmonic-PhC designs. We notice that, while a bending of $\Delta z \geq 30 \text{ nm}$ is required to obtain the lowest absolute values of the losses, the dissipative coupling rates are already large for small displacements around the mechanical equilibrium. The dissipative coupling rates of the first four S modes, calculated at $\Delta z = 0$, are $\{g^{(1)}_\kappa, g^{(2)}_\kappa, g^{(3)}_\kappa, g^{(4)}_\kappa\}/2\pi = \{-0.82, 3.19, 4.31, 3.71\}$ GHz/nm, which are among the largest dissipative coupling rates predicted so far for optical modes in the visible and infrared range.

In figs. 2(e-h) we show the same calculations of figs. 2(a-d) but for the AS modes. When the structure is bent, the field profiles of the first two AS modes are pushed towards the
FIG. 3. Control of the optical losses in photonic crystal waveguides. Positive voltages correspond to attractive electrostatic force. (a) Spectrum of the S modes for increasing applied voltages. The plots are vertically shifted for clarity. (b-c) Frequencies (b) and optical loss rates (c) of the four S modes versus the applied voltage, extracted from panel a. The top horizontal axis shows the calibrated displacement of membrane’s center, obtained by comparing the measured frequency tuning of the first mode with the calculated data. (d-f) Same as in panels a-c, but for the AS modes of a different device.

edges of the waveguide and, apart for an opposite phase of the two lobes, the field patterns become identical. Similar behaviour occurs for the third and fourth AS modes, as shown in the SM. Accordingly, the frequencies of the first two AS modes become quasi-degenerate with increasing bending (see fig. 2g and its inset, red and black lines), and the same happens for the third and fourth mode (green and blue lines). Such a degeneracy is a consequence of the anti-well potential. Importantly, due to the localization of the fields at the waveguide edges, the losses of all the AS modes strongly increase for large deformations (solid lines in fig. 2h). Large dissipative coupling rates, $\left\{ g_1^{(1)}, g_2^{(2)} \right\}/2\pi = \{0.76,1.46\}$ GHz/nm, are therefore predicted also for the AS modes at $\Delta z = 0$. 
Experimental results

The double-membrane GaAs PhCWGs samples have been fabricated through several steps of optical and electron beam lithography, similarly to the process used for parallel double-membrane PhC cavities, and described in details in the SM. A layer of high-density InAs quantum dots is grown in the middle of the top membrane and used as an internal source to excite the modes. The bending of the structure is achieved electromechanically, by applying a voltage between the adjacent faces of the two membranes. The maximum decrease of the intermembrane gap obtainable with this actuation scheme, known as the pull-in limit, is \( \Delta z_{\text{max}} = 1/3 z_0 \approx 67 \text{ nm} \) in our geometry. In the fabricated device, only the top PhCWG is mechanically-compliant and it is embedded in a four-arm bridge, while the bottom PhCWG is embedded in a fixed membrane (figs. 1(e-f)). This design allows us to strongly reduce the post-fabrication vertical buckling by etching small rectangular trenches close to the points where the four arms are connected to the substrate, as suggested in a recent work. However, compared to the ideal double-bridge design (fig. 1d), this design features two main differences. First, only the top membrane will bend under an applied inter-membrane force. Nevertheless, as long as the vertical displacement is small compared to the length of the bridge, we expect no fundamental difference with respect to the case in which both membranes move towards each other (as assumed in the calculations in fig. 2). Second, the edges of the top waveguide are not clamped. Therefore, even if a quasi-parabolic bending along the waveguide direction is obtained for large applied voltages (fig. 1g), the difference between the bending of the center and the one of the edges of the membrane is strongly reduced with respect to the ideal case in which the edges do not move (compare green and blue curves in fig. 1h). In particular, close to the pull-in condition, the bending difference is approximately 10 nm for the real structure, as compared to 67 nm for the ideal one. As we discuss below and in the SM, this sub-optimal bending profile represents one of the main practical limitations in the present implementation.

In fig. 3a we show the photoluminescence spectra of the S modes in a device with lattice constant \( a = 385 \text{ nm} \), for different applied voltages. Three peaks are visible in the spectrum when no electrostatic force is applied (\( V_B = 0 \text{ V} \), dark-blue shaded spectrum in fig. 3a). The highest-wavelength peak actually consists of two almost-overlapping modes, which appears more evident for larger applied voltages (\( V_B > 3 \text{ V} \)) when the two modes split apart. For
each applied voltage we extracted the frequency and linewidth of the optical modes by performing a multi-peak lorentzian fit. The frequency spacing between the four modes is initially strongly uneven (see fig. 3b at $V_B = 0$ V). As the voltage is progressively increased, the whole set of modes redshift, and the mode spacings become almost uniform for large applied voltages, as expected for the energy levels of a harmonic-like potential. Moreover, as shown in fig. 3c, the optical loss rates of all four modes decrease for large applied voltages. For the first mode ($\kappa_1$, black squares in fig. 3c), a modulation of the loss rate of a factor of almost 2 is obtained, while for the second mode ($\kappa_2$, red circles in fig. 3c) the loss rate is modulated by a factor larger than 3 (calculated from the lowest to the highest point). A decrease of the loss rate of a factor of 2 is also observed for the third and fourth mode. The initial increase of the loss rates of the first two modes is likely due to the structural disorder and to the frequency degeneracy of the two modes which, up to a voltage of 3 V, makes the estimation of the linewidths difficult. By comparing the measured spectral tuning of the first mode (fig. 3b, black line) with the simulated one, we can infer the vertical displacement of the center of the waveguide for each applied voltage, as indicated in the top axis of figs. 3(b-c). This allows us to estimate the maximum dissipative coupling rates. In particular, by performing a fit of the data shown in fig. 3c for large applied voltages (specifically, for $V_B > 3$ V for the first mode and for $V_B > 3.4$ V for other modes) we obtain the values \{\frac{g_1}{2\pi} = \{2.4 \pm 0.7, 6.2 \pm 1.0, 2.0 \pm 0.1, 2.3 \pm 0.1\} \text{ GHz/nm}, which are in the same range as those calculated for the ideal structure in fig. 2.

In figs. 3(d-f) we show the results of the electrostatic tuning of the AS modes of a different device, which is nominally identical to the first one (apart for the lattice constant that is $a = 380$ nm), but fabricated in a different run. Two modes are clearly visible and well-separated in the spectrum when no electrostatic force is applied (bottom plot of fig. 3d). When the structure is bent (fig. 3d) the two modes blue-shift and their spectral spacing quickly decreases until, at about 2.6 V, the modes completely overlap. Moreover, the optical losses of both modes strongly increase, resulting in a loss modulation of more than a factor of three for the first mode and more than a factor of five for the second mode (fig. 3f). For voltages higher than 2.95 V, the mode intensity becomes too low and the linewidth cannot be estimated accurately. Both the spectral merging of the two modes and the loss increase match the expected behaviour shown in fig. 2g (red and black line). Similarly as for the S modes, we estimate the membrane displacement (top axis of figs. 3(e-f)) by comparing
the experimental frequency tuning of the first mode with the simulated one. From this calibrated displacement, we calculate the maximum dissipative coupling rates of the two AS modes, \( \{ g_1, g_2 \} / 2\pi = \{ 3.3 \pm 1.7, 7.9 \pm 3.1 \} \) GHz/nm.

**DISCUSSION**

While the observed trends match the theoretical results, the measured optical loss rates deviate considerably from the theoretical values, both in terms of their initial values (i.e., when the structure is not bent) and in terms of the total loss modulation, which is expected to be more than two orders of magnitude for the first two S and AS modes. A primary cause of this deviation is constituted by the structural disorder in the PhC pattern and by the residual surface roughness due to the fabrication. Both these imperfections introduce additional loss channels, which can become the dominant loss mechanism and therefore hinder the expected loss modulation. Moreover, in the fabricated devices the obtainable bending profile is far from the ideal one (compare blue and green lines in fig. 1h), because the edges of waveguides are also displaced downward. This reduces the contrast between the ERI of the center and the one of the edges of the waveguide, and therefore limits the field modulation. We quantitatively investigated the effect of the structural disorder and the non-optimized bending separately by performing a set of numerical simulations. The structural disorder can be modeled by introducing in the FEM simulations random fluctuations of the positions and radii of the holes. Our calculations (fig. S14 of the SM) show that an amount of structural disorder comparable to the one observed in the fabricated devices can limit the maximum Q factor achievable in a bent waveguide to values of \( 10^4 - 10^5 \), thus reducing the loss modulations calculated for a non-disordered PhC (in particular for the first two S/AS modes). To estimate the impact of the sub-optimal bending profile, we performed FEM simulations in which the intermembrane spacing is varied according to the bending profile of the real device (such as the one in fig. 1g), calculated for different applied voltages. The results (fig. S13 of the SM) indicate that a realistic bending profile can substantially reduce the loss modulations, in particular for the S modes, for which the maximum Q factor enhancements shown in fig. 2d are reduced by a factor of about 10. Finally, we performed simulations in which both the structural disorder and the sub-optimal bending profile are taken into account (fig. 4). The calculations show that, while a clear decrease
of the optical losses is still obtained for large values of $\Delta z$, the loss modulations are less than one order of magnitude (fig. 4b, averaged over four realizations of the disorder), in a good agreement with the experimental data. We note that the dependence of the loss rate on the bending becomes non-monotonic for some modes in the presence of imperfections, a feature also observed in the experiments (fig. 3c). The frequency spacings (fig. 4a) become even for the first three modes for large displacements, while the spacing between the third and fourth mode remains larger, similar to what observed in the experimental data (fig. 3b). The field patterns of the first two S modes (for a particular realization) are quite affected by the structural disorder for $\Delta z = 0$ (fig. 4(c-d), first row). Nonetheless, for large mechanical deformations a reshaping and a localization of the field profiles is clearly visible. We emphasize that, despite these strong limitations in the current implementation of the device, the measured modulation of the optical losses is much larger than the one obtained in other electromechanical systems, demonstrating the potential of our method for the mechanical control of the Q factor in PhC structures.

Importantly, while the total modulation of the loss rate is reduced by the effects described above, we do not expect the dissipative coupling rate to be affected. Indeed, the variation of the loss rate is not altered by the presence of other loss channels. Moreover, large dissipative coupling rates are expected in the ideal device already for small displacements $\Delta z$ around the configuration in which the membranes are parallel to each other (see figs. 2(d,h)). Such moderate bending profiles can be reached in the real devices for large applied voltages (e.g., fig. 1h, green line). Indeed, the order of magnitude of the experimental values of the dissipative coupling rates at large voltages ($|g_\kappa|/2\pi = 1 - 10 \text{ GHz/nm}$), agrees well with the dissipative coupling rates calculated for the ideal device and for small displacement around $\Delta z = 0$.

Finally, we note that the displacement pattern induced by the applied voltage is rather similar to the one of the fundamental flexural mechanical mode of the top membrane. Therefore, the values obtained for the dissipative coupling rates $g_\kappa$ allow us to estimate the vacuum dissipative coupling rates (i.e., the loss rate modulation due to the presence of one phonon) achievable in our structure. The vacuum dissipative coupling rate is defined by $g_{0,\kappa} \equiv g_\kappa x_{\text{zpfs}}$, where $x_{\text{zpfs}} = \sqrt{\hbar/2M_{\text{eff}}\Omega}$ is the zero-point motion amplitude, and $M_{\text{eff}}$ and $\Omega$ are the effective mass and the resonant frequency of the mechanical mode, respectively. By calculating numerically $M_{\text{eff}}$ and $\Omega$, we obtain a value of $x_{\text{zpfs}} = 9.6 \text{ fm}$, which leads to vacuum dissipative
FIG. 4. **Behaviour of the S modes in a double-membrane PhCWG with a disordered PhC pattern and a realistic bending of the top bridge.** (a) Frequencies and (b) losses of the first four S modes versus the displacement $\Delta z$, obtained by averaging four realizations of the disordered structure. (c-d) Field patterns of the (c) first and (d) second S mode for a particular realization of the disorder and for different deformations of the structure. The displacement $\Delta z$ is indicated on the right side of each row.

coupling rates in the range $|g_{0,\kappa}|/2\pi = 10\text{-}100$ kHz.

**CONCLUSIONS**

We have proposed, theoretically discussed and experimentally demonstrated a photonic-crystal-based NOEMS in which the mechanical bending of a membrane induces large variations of the spatial pattern of the optical fields. This is achieved by locally modulating the effective refractive index in a double photonic crystal waveguide, which results in the creation of a potential well or anti-well for the optical field. As a consequence of moving the optical field far away or close to the waveguide’s edges, large modulations of the optical losses are predicted by our calculations. Experimentally, we were able to measure modulations of the optical losses up to a factor larger than five, much larger than the ones obtained with different electromechanical approaches,$^{26,31,32}$ and dissipative coupling rates in the 1 - 10 GHz/nm range. We have shown that the performance of our devices are currently limited...
by the structural disorder of the PhC and by the sub-optimal bending profile. The latter is
due to the particular four-arm bridge design that we used to eliminate the post-fabrication
vertical buckling. Thus, the bending profile can be improved by either further optimizing the
geometrical parameters of the four-arm bridge design, or by working with shorter doubly-
clamped bridge designs (fig. 1d) that are not affected by vertical buckling (fig. S11); since
shorter bridges are also stiffer, the latter option will require fabricating p-n junctions with
larger breakdown voltages, or implementing different bending mechanisms.

Importantly, this work demonstrates how the field pattern in a nanophotonic cavity can
be controlled mechanically, and opens the way to new regimes of opto-electro-mechanical
coupling where the field, instead of the frequency, is coupled to the mechanical motion. We
note that, while in the present structure the mechanical motion produces a variation of
mode frequency, field distribution, and loss rate, it is possible to design structures where
only the field is modulated upon an anti-symmetric perturbation.\textsuperscript{20–22} In perspective, this
coupling can lead to several applications such as novel platforms for controlling the sponta-
neous emission based on altering the field amplitude at the emitter position rather than
introducing a frequency detuning,\textsuperscript{19} establishing an efficient emitter-phonon coupling,\textsuperscript{21} and
the mechanical control of the far-field emission and lasing.

\textbf{ACKNOWLEDGMENTS}

We acknowledge fruitful discussions with R. W. van der Heijden, E. Verhagen, P. M.
Koenraad and M. E. Flatté. The work of M.C. is part of the research programme 'Nanoscale
quantum optics' of the Foundation for Fundamental Research on Matter (FOM), which
is financially supported by the Netherlands Organisation for Scientific Research (NWO).
This research is also supported by the Dutch Technology Foundation STW, applied science
division of NWO, and the Technology Program of the Ministry of Economic Affairs under
projects No. 10380 and No. 12662. L.M. acknowledges financial support by the Danish
Council for Independent Research (Technology and Production Sciences).

* michele.cotrufo@utexas.edu


The quoted values of the dissipative coupling rates have been inferred by the authors from fig. 3b of ref. 31 and fig. 3b of ref. 26.


See Supplemental Material at [URL will be inserted by publisher] for additional details on: pull-in limit, analytical and numerical simulations, sample fabrication, influence of buckling, experimental setup, and limitations of the real devices.


